

GALEX TELESCOPE VIBRATION RESPONSE REDUCTION

**Michelle Coleman
June 25, 2002**



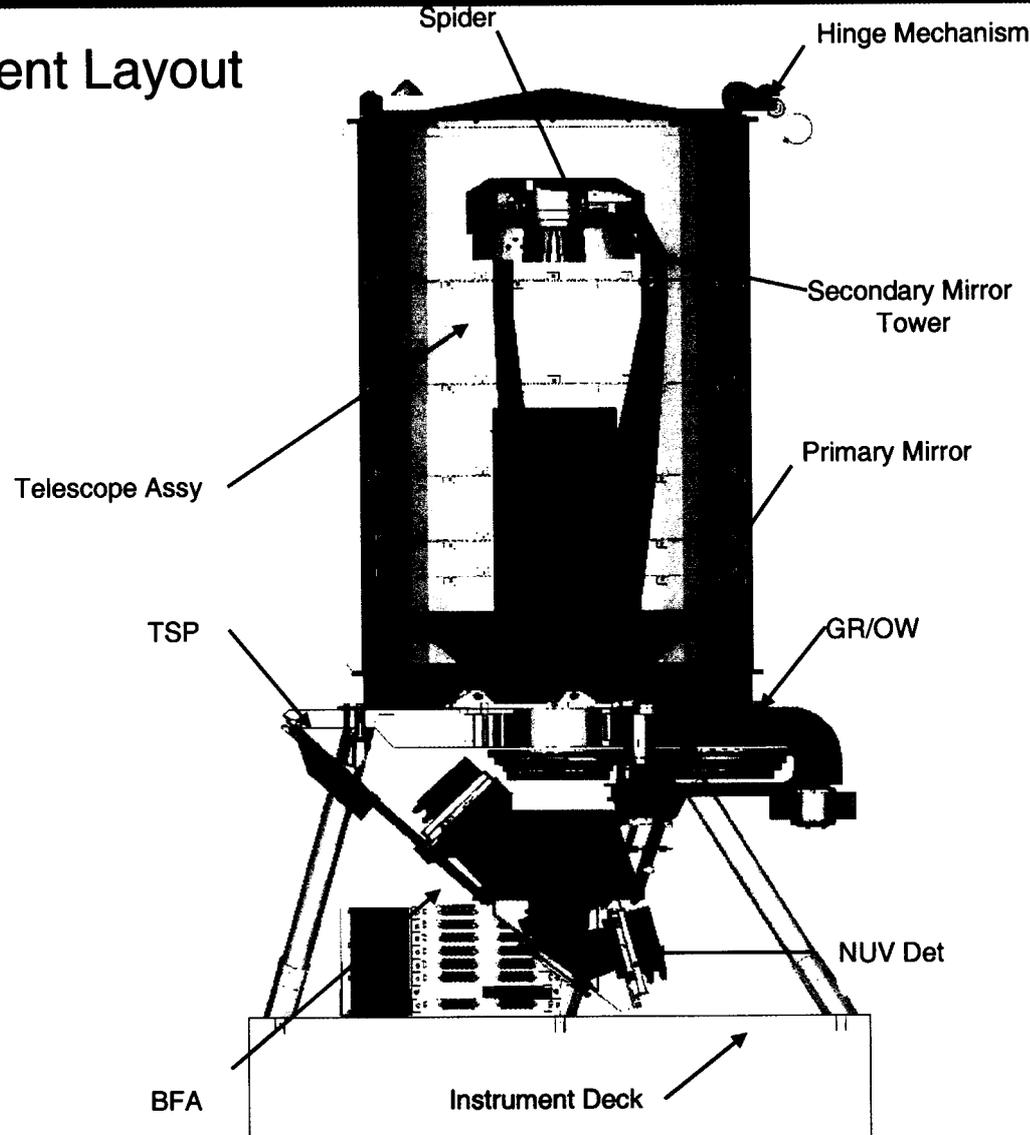
GALEX Telescope Vibration Response Reduction



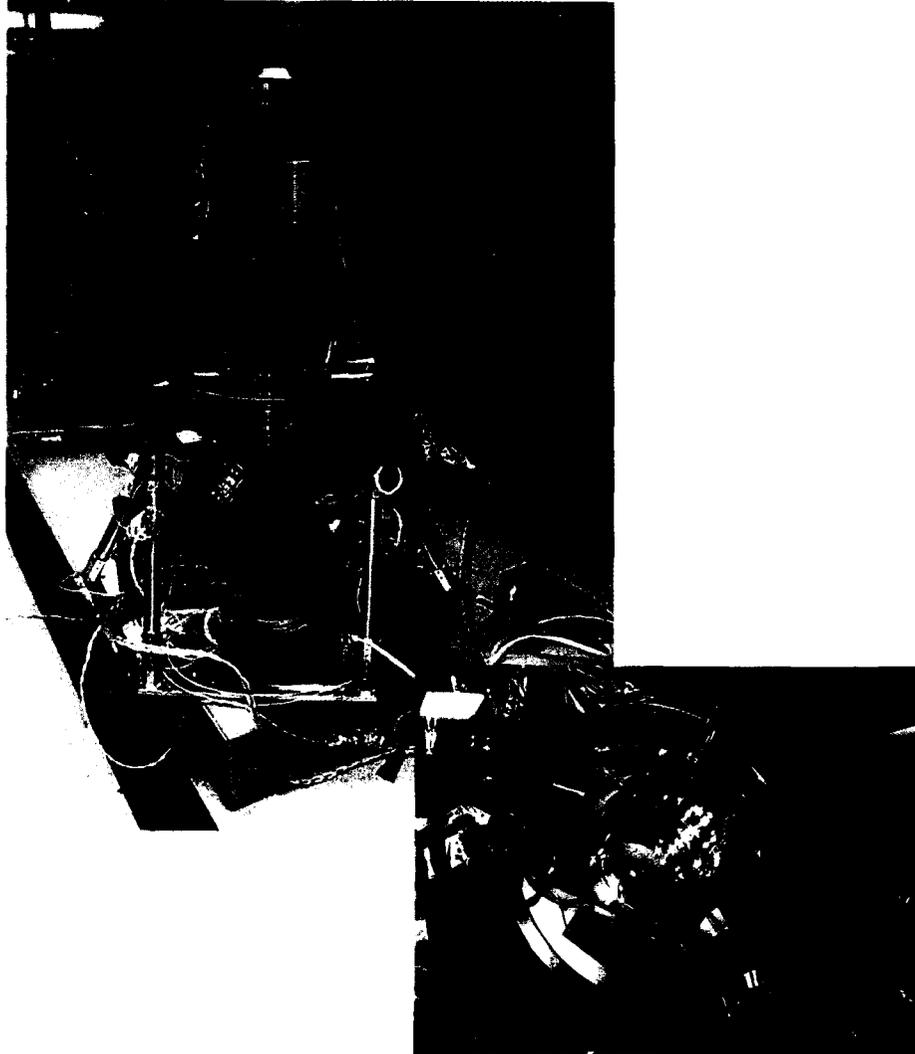
- Overview
 - *Telescope Response Problem*
 - *Telescope Response Solution*
 - *Instrument Bipod Design Approach*
 - ◆ Stiffness Reduction
 - ◆ Damping
 - *Instrument Vibration Test Results*
 - *Spacecraft Vibration Test Results*

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- Instrument Layout



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- Telescope Response Problem
 - *During Instrument lateral vibration testing (10/00), the input was manually notched -20 dB from 45 to 55 Hz in addition to force limiting due to the TA secondary mirror assembly response above the misalignment g level (22 g) determined by static testing (8/00).*
 - ◆ Response at the Telescope secondary mirror showed a Q of 80+

| | | | |
|-----------|-------------------------|-----------|-------------------------|
| 20-30 | +9 dB/Oct | 20-75 | +9 dB/Oct |
| 30-60 | 0.1 g ² /Hz | 75-120 | 0.1 g ² /Hz |
| 60-80 | -10 dB/Oct | 120-160 | -10 dB/Oct |
| 80-1000 | 0.04 g ² /Hz | 160-1000 | 0.04 g ² /Hz |
| 1000-2000 | -12 dB/Oct | 1000-2000 | -12 dB/Oct |
| Overall | 7.3 grms | Overall | 7.4 grms |
| duration | 75 sec | duration | 75 sec |

- *As a result, the Instrument was not qualified in the lateral axes.*



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- Telescope Response Solution
 - *Several Paths were investigated*
 - ◆ KSC re-analyzed Spacecraft vibration levels based on previous Pegasus flight data
 - *Analysis indicated that a -2 dB reduction in the X axis input acceleration from 0.16 g²/Hz to 0.10 g²/Hz was possible*
 - ◆ Design modifications to reduce the Telescope Secondary response levels
 - *Options investigated by analysis were*
 - tuned mass damper on Baffle cover
 - dampened spring system between Telescope and Baffle structures
 - Instrument Bipod stiffness reduction with constrained layer damping
 - Instrument vibration isolation system (CSA Engineering)
 - Spacecraft vibration isolation system (CSA Engineering)
 - *Instrument Bipod stiffness reduction was optimal choice (based on schedule and cost) by reducing the TA response to acceptable levels without effecting optical hardware and resulted in 2 benefits*
 - favorable modal combination
 - increased damping



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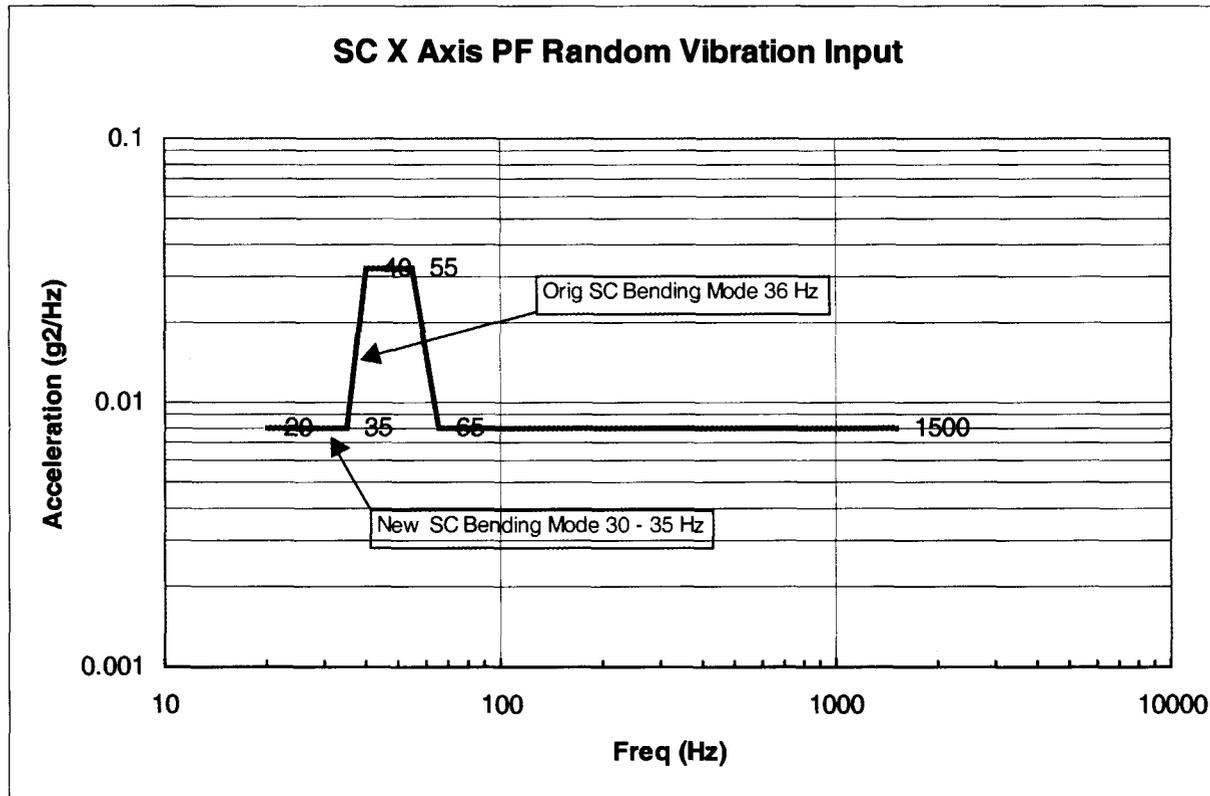


- Instrument Bipod Design Approach - Stiffness Reduction
 - *Favorable modal combinations*
 - ◆ *200 lb Instrument on a 200 lb Spacecraft bus*
 - ◆ *Critical local Telescope mode not susceptible to force limiting due to low effective mass*
 - *Vibration Analysis Assumptions*
 - ◆ *Spacecraft FEM with 1.5% modal damping for all modes*
 - ◆ *Stiffness of the bipods were varied from current 262,000 lb/in to 46,500 lb/in min*
 - *Method relies on changing the Instrument modal character*
 - ◆ *Instrument bending mode combines with the Telescope bending mode and drives the overall Spacecraft bending mode from 36 Hz to 30 Hz.*
 - ◆ *Reduced SC bending mode occurs at a frequency which is at the lower acceleration input level than previous SC bending frequency*
 - *Force limiting at the base further reduces input acceleration*
 - ◆ *Telescope secondary response decreased from 11.1 grms to 5.6 grms without force limiting and 8.5 grms to 4.2 grms with force limiting*

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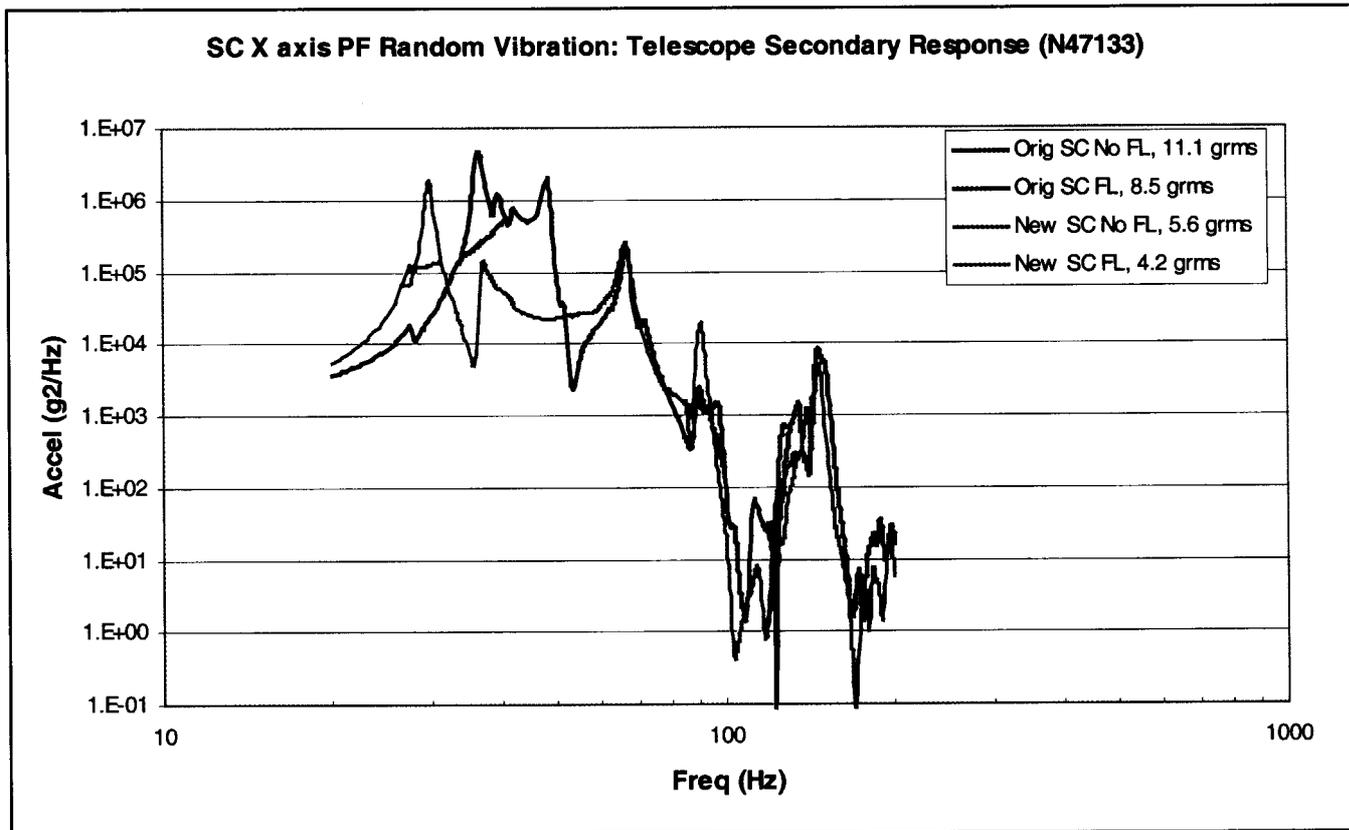
- Instrument Bipod Design Approach - Stiffness Reduction



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- Instrument Bipod Design Approach - Stiffness Reduction





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Vibration Response Reduction

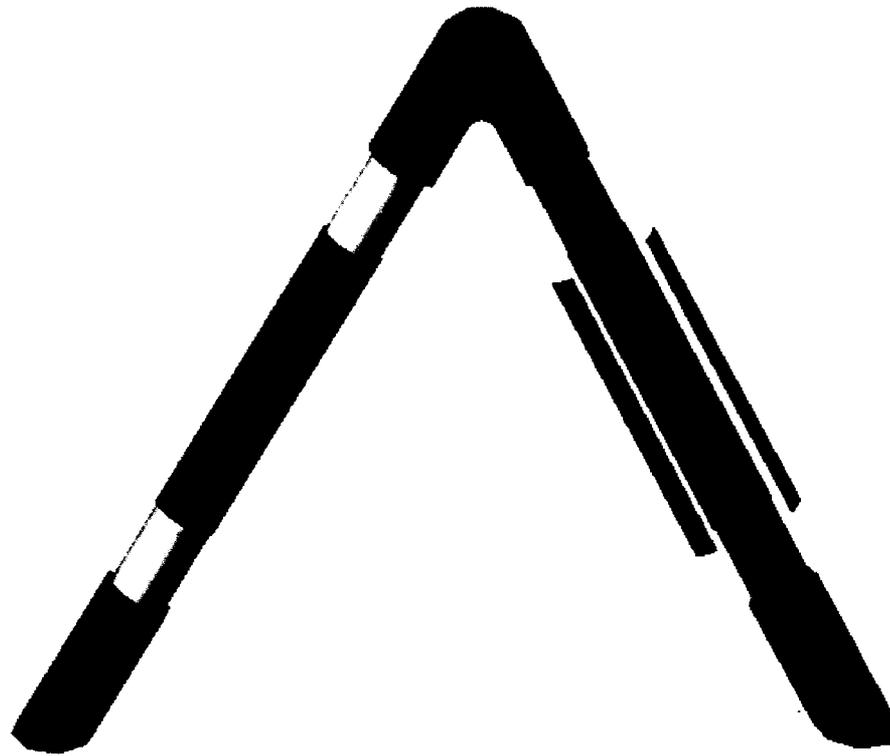


- Instrument Bipod Design Approach - Stiffness Reduction
 - *Based upon acceptable TA secondary response from random vibration analysis, bipod stiffness variations were determined*
 - ◆ 46500 lb/in minimum
 - ◆ 66400 lb/in maximum
 - *Bipod material and wall thickness were determined using 46500 lb/in*
 - ◆ 1.5" OD drove the tube material to Fiberglass for acceptable wall thickness of 0.050" for handling and positive buckling margins
 - *Composite codes showed that Astroquartz II with ± 45 layup produced an acceptable Young's Modulus*
 - coupon plate test results (± 45 & 0, 90, ± 45 layups) showed Young's Modulus lower than composite code predictions
 - Tube (t=0.040" & 0.060") test for Young's Modulus (less than predicted) and tensile failure
 - Tube thickness was increased to 0.070", tested for Young's modulus and sent to CSA Engineering
 - ◆ Bipod fittings were changed from AL 7075 to Ti 6Al 4V for thermal compatibility with new fiberglass tubes and 8 mil bond line of 9394 epoxy
 - *Structural Integrity maintained*

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- Instrument Bipod Design Approach - Damping
 - *In order to achieve 1.5% modal damping, CSA Engineering designed a constrained layer damping treatment*
 - ◆ Eight Alum 0.050" thick staves, 0.010" thick 3M9473 2" at both ends of strut



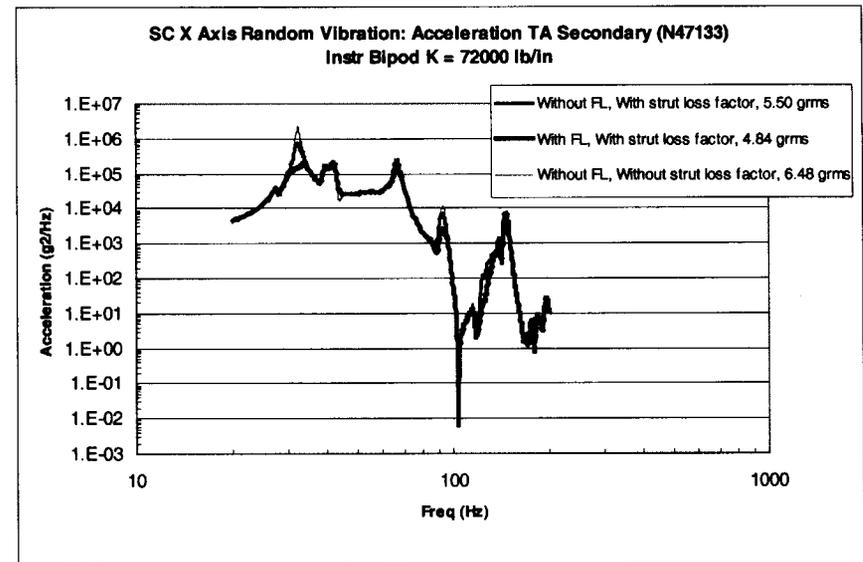
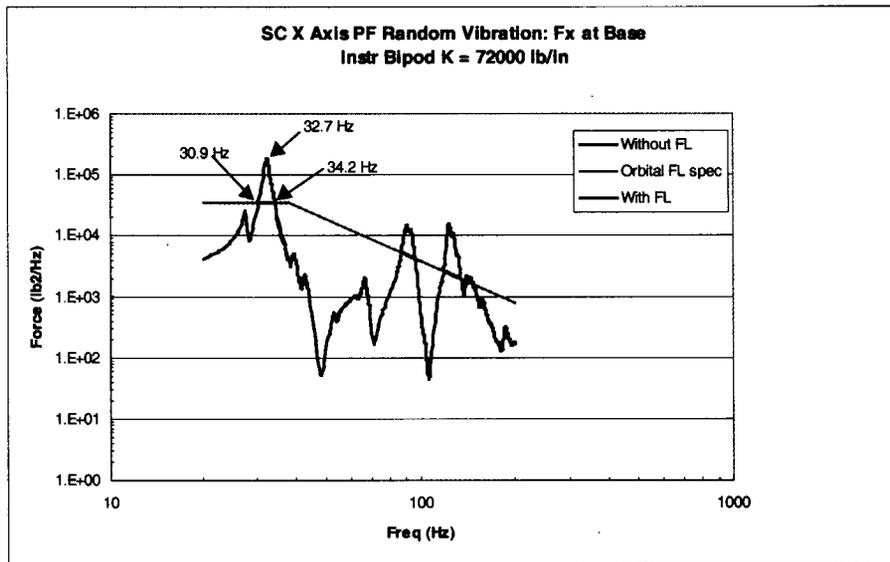
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- Instrument Bipod Design Approach - Damping
 - *CSA test tube results (1.35" ID, 14 plies Astroquartz II \pm 45 layup)*
 - ◆ undamped - tube stiffness 59400 lb/in, loss factor of 0.45%
 - ◆ damped - VEM (t=0.010") is temperature and frequency dependent
 - @70F and 30Hz
 - tube stiffness 64000 lb/in, loss factor 9.6%
 - @74.5F and 30 Hz
 - tube stiffness 62700 lb/in, loss factor 8.7%
 - *A tube stiffness of 72000 lb/in was used in the analysis to account for colder temperature and additional margin*

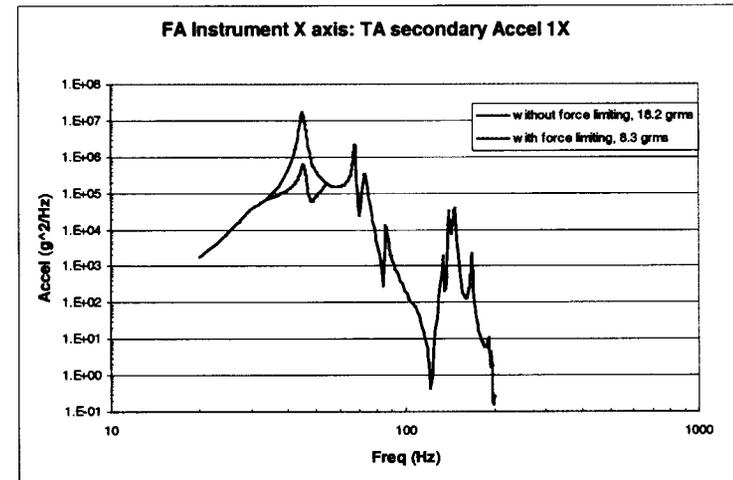
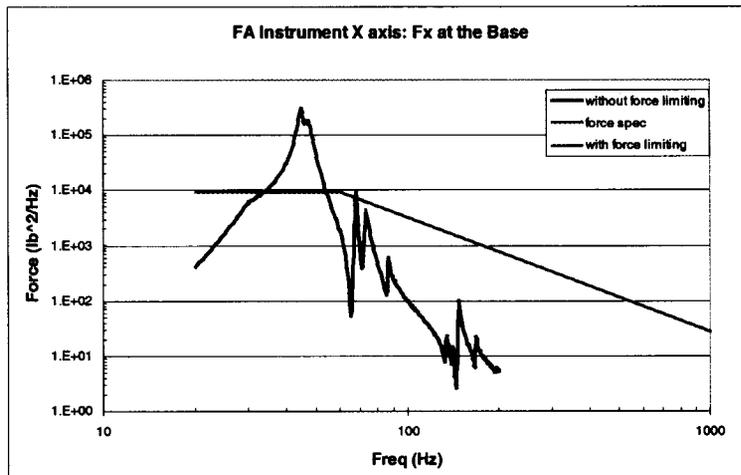
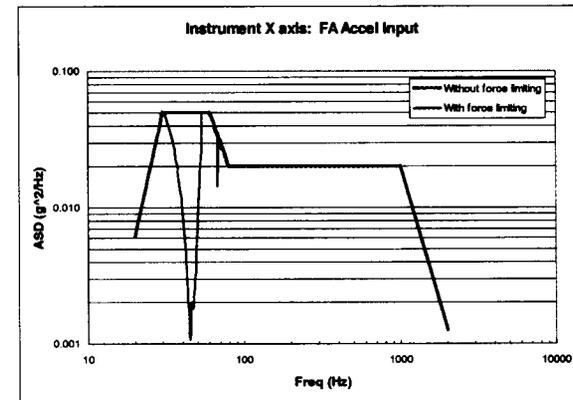
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- Instrument Bipod Design Approach - Damping
 - *SC vibration analysis for 72000 lb/in strut with a loss factor of 0.11 resulted in a SC bending mode of 32.7 Hz and TA secondary response of 5.5 grms without force limiting and 4.8 grms with force limiting*



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- Instrument Random Vibration Test, June 2001 - Predictions
 - *Analysis predicted a single mode at 45 Hz with enough effective mass for force limiting to reduce input and Telescope response*

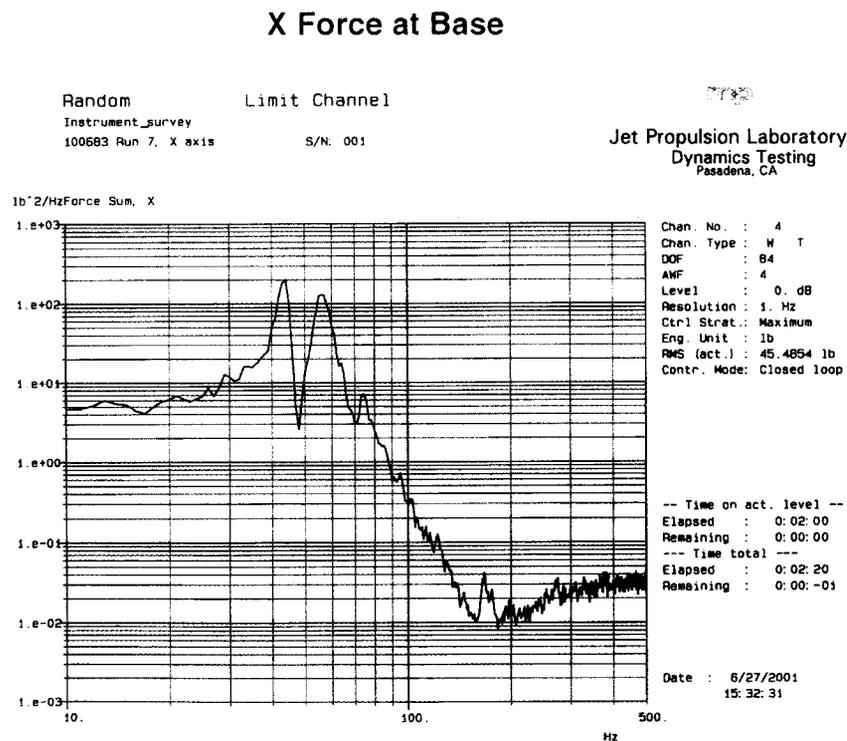
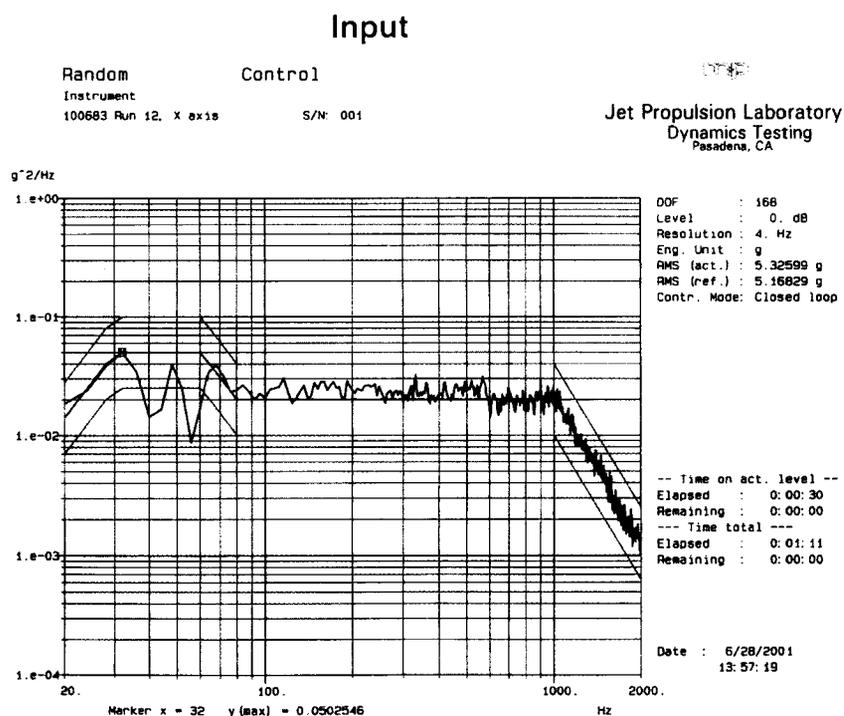




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- Instrument Random Vibration Test, June 2001 - Results
 - Two modes at 45 and 55 Hz with large effective mass for force limiting to reduce input by 6 dB.





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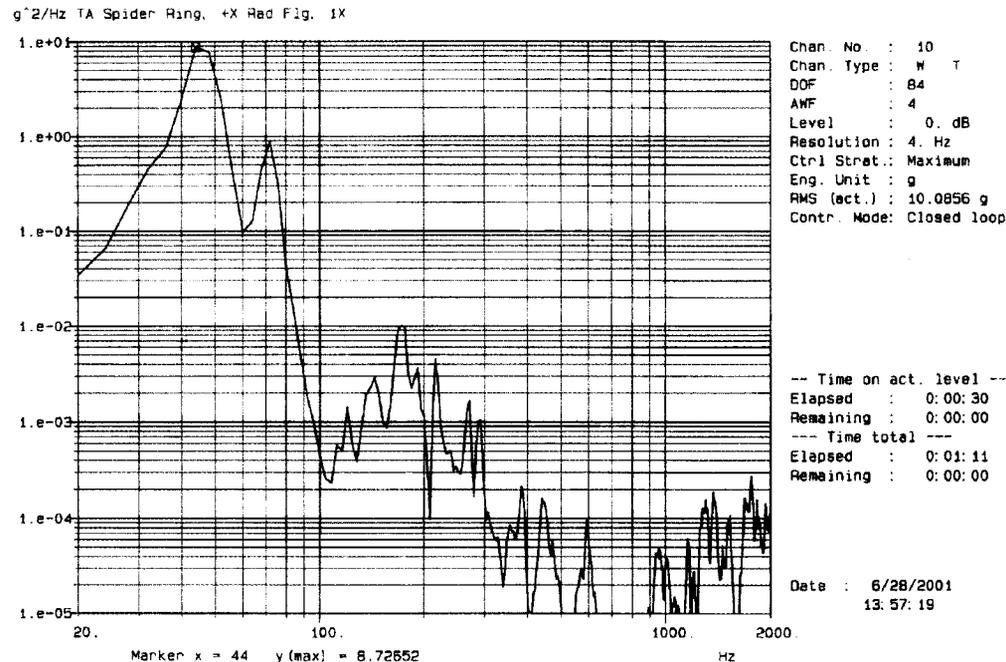


- Instrument Random Vibration Test, June 2001 - Results
 - Time histories: 29.1 g peak X axis, 21.4 g peak Y axis
 - Post-test misalignment showed acceptable

Telescope Response Random Instrument Limit Channel S/N: 001

100683 Run 12, X axis

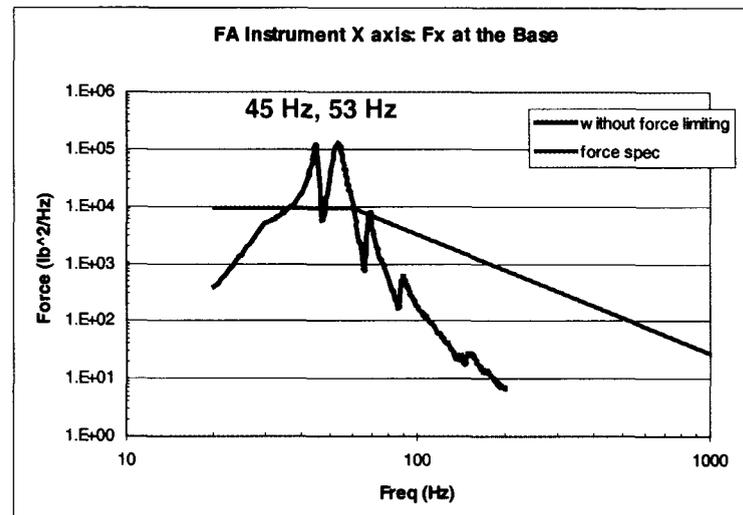
Jet Propulsion Laboratory
Dynamics Testing
Pasadena, CA



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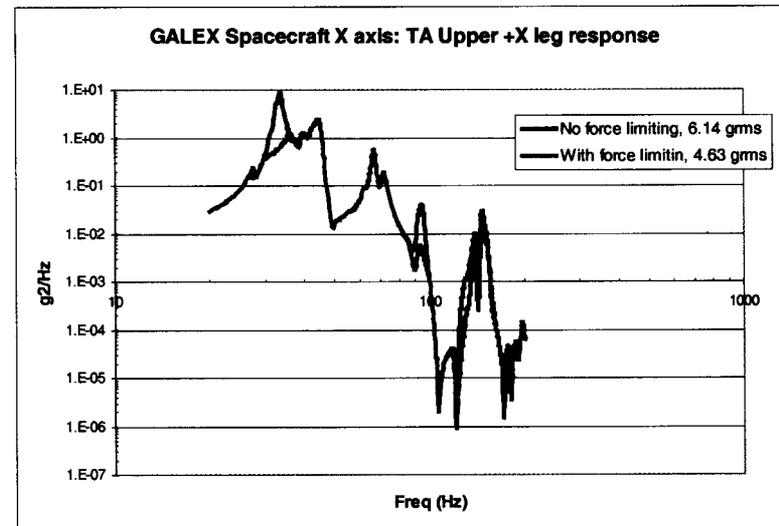
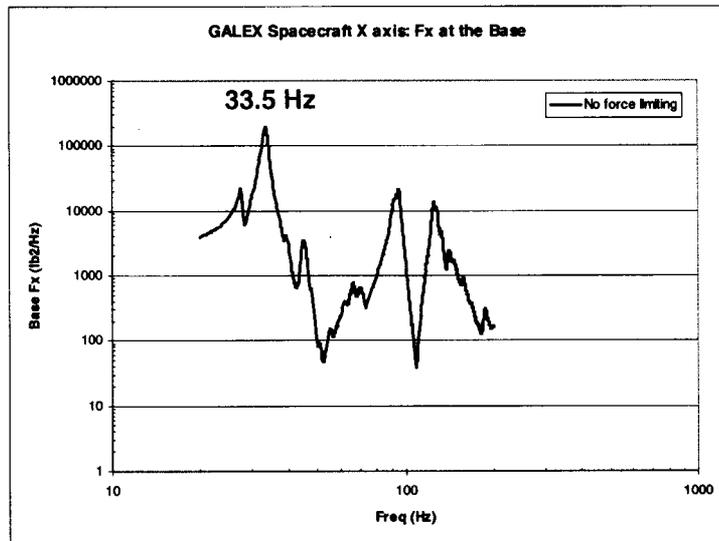


- Instrument Random Vibration Test, June 2001 - Results
 - *Correlation of vibe test results with Instrument finite element model*
 - ◆ calculated effective mass from test
 - ◆ single mode to two modes
 - *Adjusted bipod properties to obtain results similar to test*



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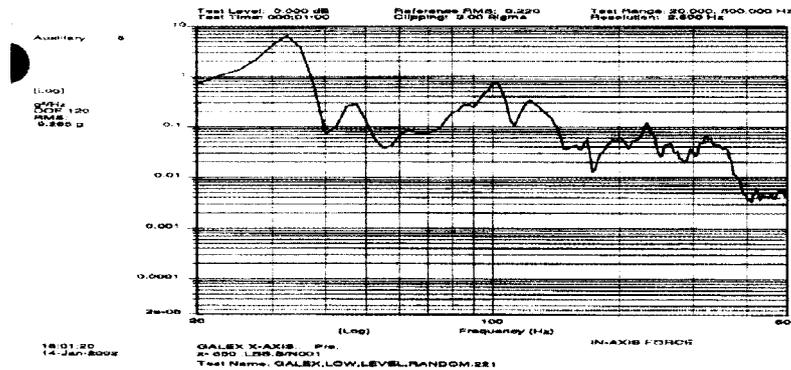
- Spacecraft Random Vibration Test, January 2002 - Predictions
 - *Re-analyzed Spacecraft random analysis with updated Instrument FEM*



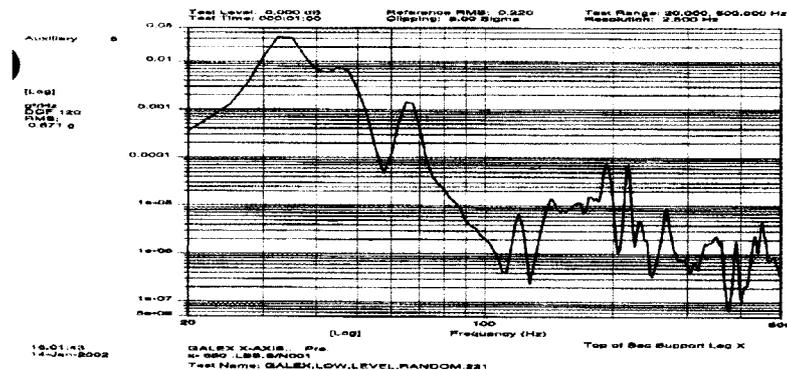
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- **Spacecraft Random Vibration Test, January 2002 - Results**
 - *Frequency and Telescope response predictions correct*
 - ◆ Spacecraft / Instrument/ Telescope mode at ~33 Hz
 - ◆ Telescope response rms prediction
 - *Spacecraft provided additional damping*

Low level run: X Force at Base



Low level run: Telescope Response



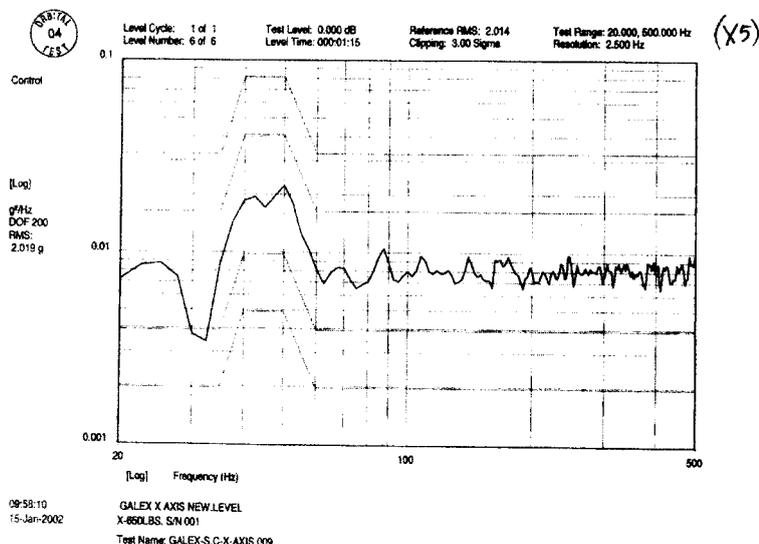


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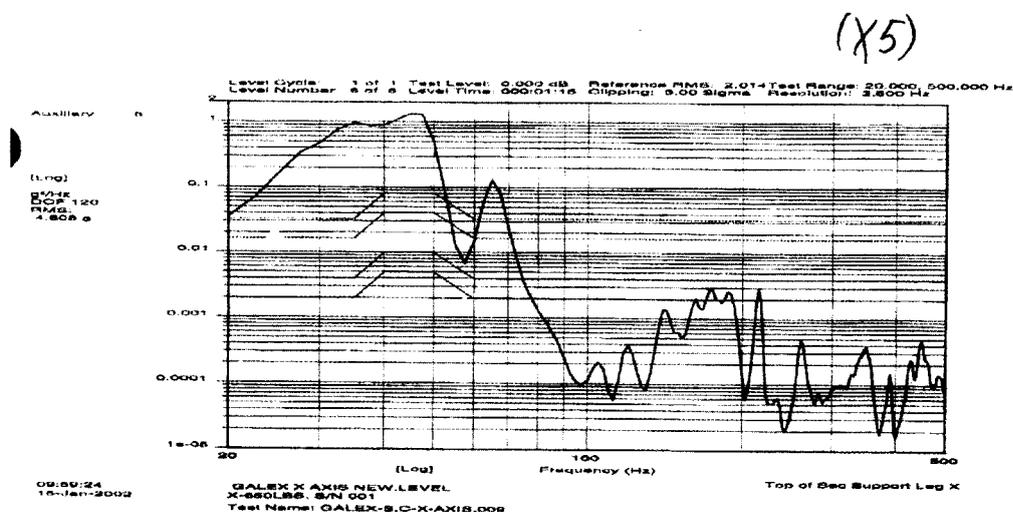


- Spacecraft Random Vibration Test, January 2002 - Results
 - Time Histories: 17.4 g on leg extrapolated to 19.6 g peak at spider in X axis

Full level run: X Force at Base



Full level run: Telescope Secondary leg Response



- Spacecraft successfully completed random vibration testing with minimal force limiting