



**Jet Propulsion Laboratory**  
California Institute of Technology

# Splashdown on Titan: Modelling Peak Loads, Plunge Depth, and Resurge Time for a Capsule Impact in a Methane Sea

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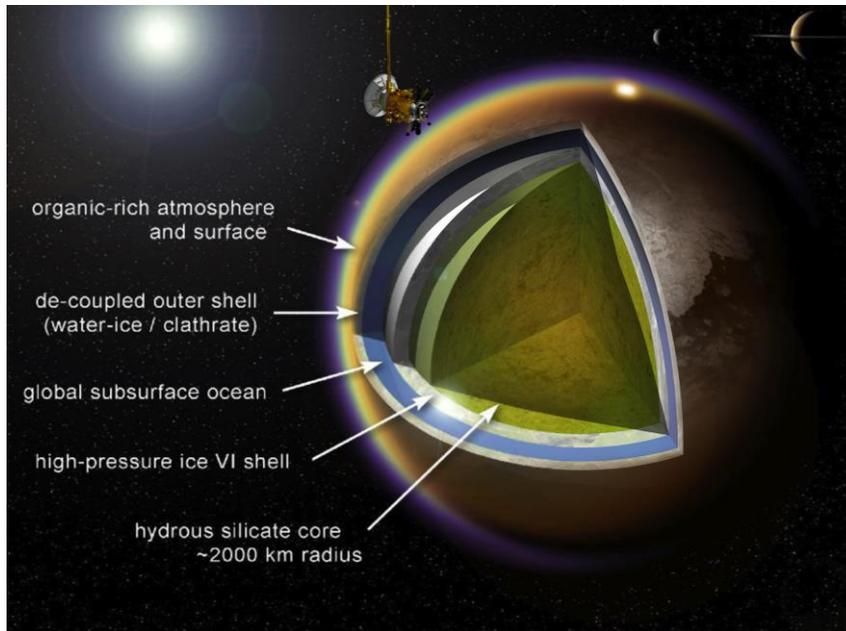
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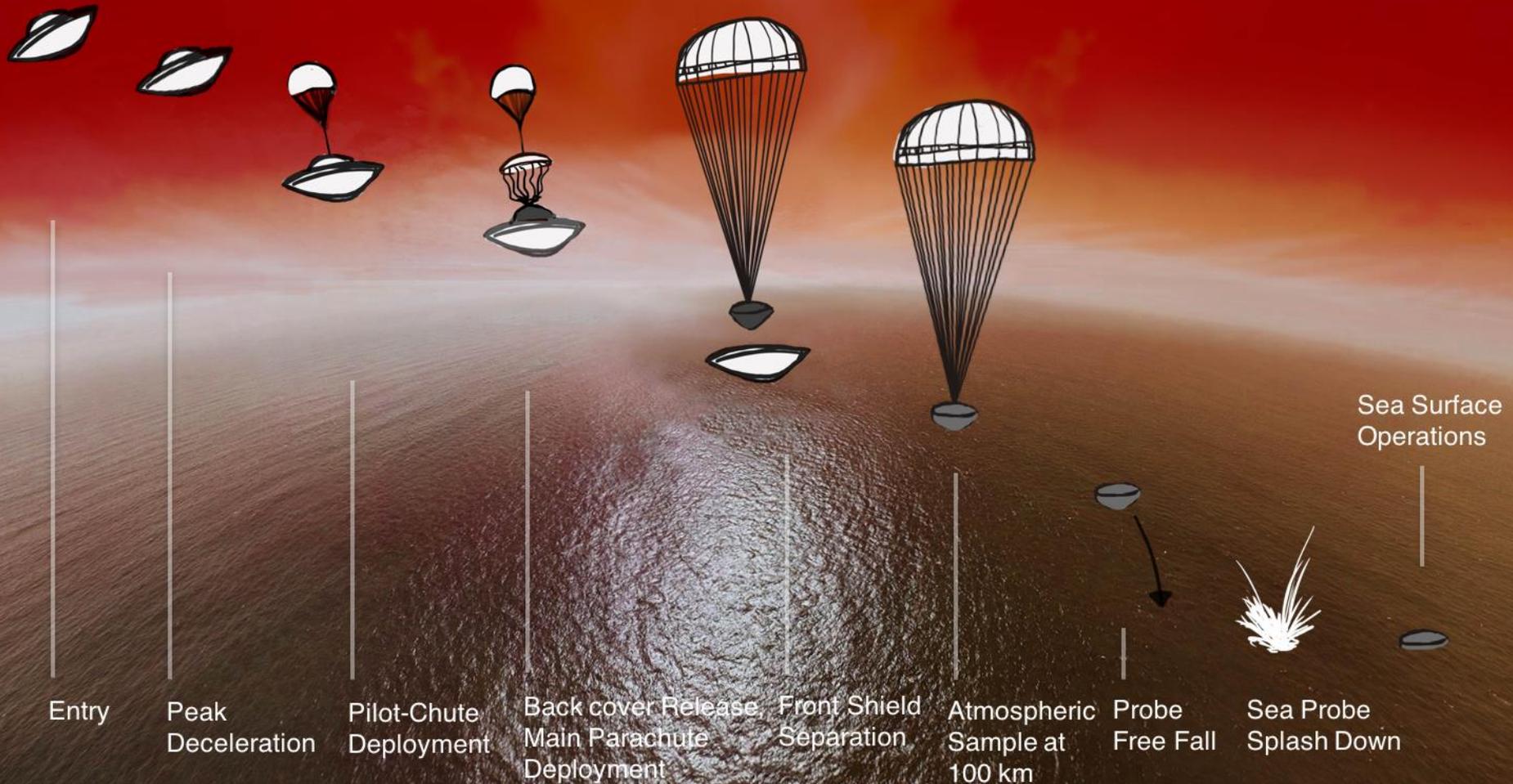
# Motivation



- Titan is only body besides Earth to support standing bodies of liquid
- Hydrocarbon seas of astrobiological and oceanographic interest
- A probe structure and instruments would need to survive splashdown event
  - Need to predict impact loads
- Knowledge of plunge depth vital for probe design (liquid resistance) and operations timing
  - Ensure doesn't hit bottom
  - Informs ability to take sample at depth
- Analytical solutions limited to simple axisymmetric shapes and ideal vertical entry

# Probe EDL Concept of Operations

Freefall segment would reduce landing dispersions due to winds

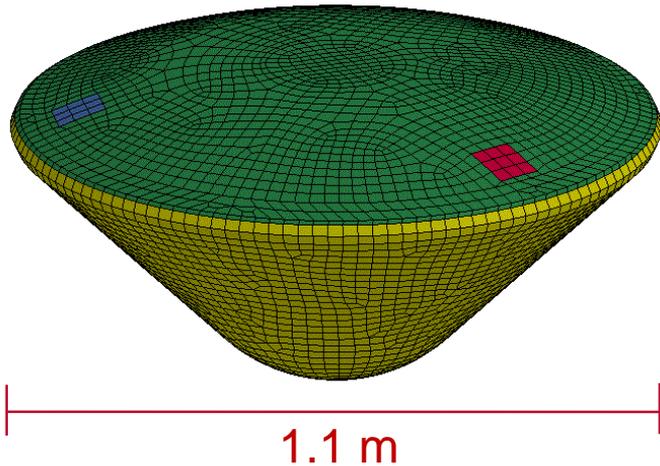


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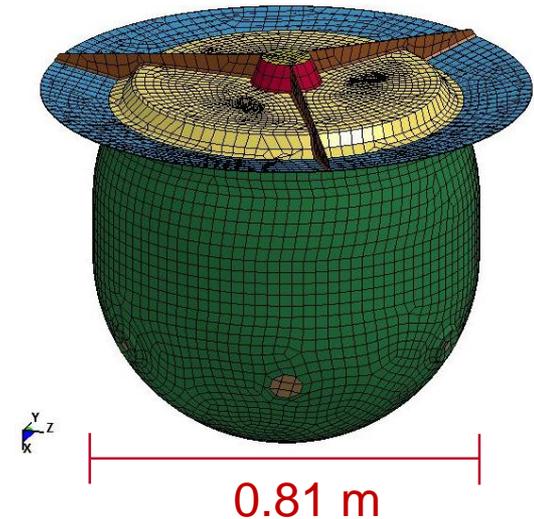
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# Candidate Probe Designs



- **45° Spherecone Probe**
  - Provides subsonic aero stability in freefall
  - Provides tapered shape for low-G impact
  - Provides high drag for low velocity impact and low-G load on splashdown



- **Cylinder with Spherical Nose Probe**
  - Drag plate reduces velocity and provides stability in freefall
  - Flexible packaging

# Analytical Methodology

## Impact G-Loads

- Impact velocity is terminal descent velocity

- $V_0 = \sqrt{\frac{2Mg}{\rho_{atm}SC_D}}$

- Method 1: Closed form solution for spherical noses [Hirano and Miura]

- Froude number,  $F = V_0(gR_N)^{-1/2}$

- Mass ratio,  $\mu = \frac{3M}{4\pi\rho R_N^3}$

- Max deceleration,  $A_{max} = 0.491F^2\mu^{-2/3}g$

- Method 2: Solve numerically over time [McGehee, et al],[Lorenz, et al]:

- For general axisymmetric shape, radius R is a function of height:  $R = f(h)$

- $A = \frac{V^2\pi k\rho R^2 dR}{(M + \frac{2}{3}k\pi\rho R^3)dh}$

- For spherical nose,  $V = \frac{MgV_0}{Mg + \left(\frac{3}{4}\right)\frac{2\pi}{3}\rho gR^3 \left[\sin^3 \cos^{-1}\left(1 - \frac{h}{R}\right)\right]}$

- $A = \frac{\Delta V}{\Delta t}$

# Analytical Methodology

## Plunge Depth

- Method 1: 1-D differential equation solved numerically
  - Buoyancy ( $B$ ), drag ( $D$ ), and weight ( $W$ ) forces act on probe
  - $Ma = B - \text{sign}(V)D - W$
- Method 2: Conservation of momentum and energy
  - Use conservation of momentum to calculate residual velocity after impact
  - $Work_{Buoyancy} = KE$
  - Ignore drag, potential energy

# LS-DYNA

- Explicit, transient dynamic finite element code
- Fluid modeled with Arbitrary Lagrangian-Eulerian approach
  - Takes into account movement of fluid mass and compressibility
  - Not full Navier-Stokes
- Probe is rigid body
- Maximum expected sea density used for impact loads:  $500 \text{ kg/m}^3$
- Minimum expected sea density used of plunge depth:  $630 \text{ kg/m}^3$

# Test Suite for 45° Spherecone Candidate Probe

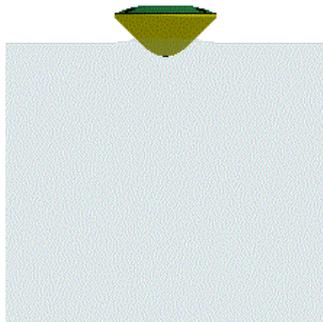
## Case 1: 0° Vertical High Load

$V_v = 8.8 \text{ m/s}$

$V_h = 0.0 \text{ m/s}$

Angle = 0°

Liquid Density =  $630 \text{ kg/m}^3$



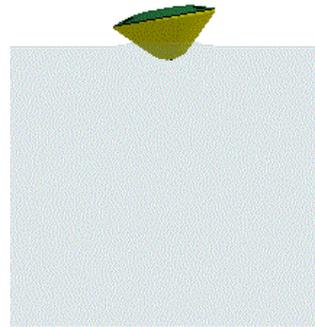
## Case 2: 10° Vertical High Load

$V_v = 8.8 \text{ m/s}$

$V_h = 0.0 \text{ m/s}$

Angle = 10°

Liquid Density =  $630 \text{ kg/m}^3$



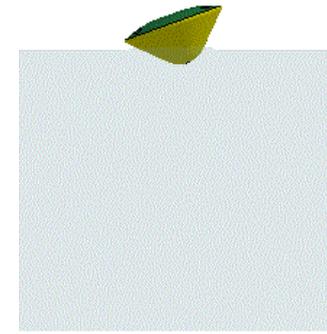
## Case 3: 20° Vertical High Load

$V_v = 8.8 \text{ m/s}$

$V_h = 0.0 \text{ m/s}$

Angle = 20°

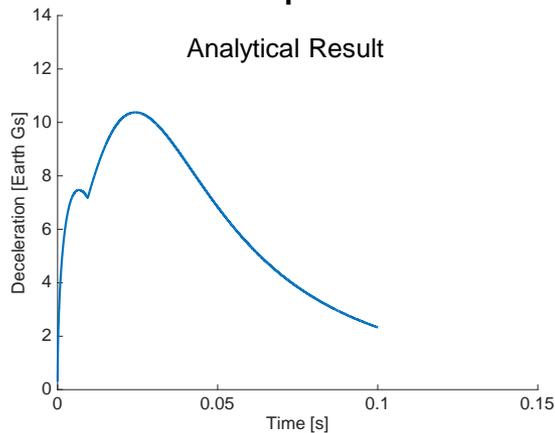
Liquid Density =  $630 \text{ kg/m}^3$



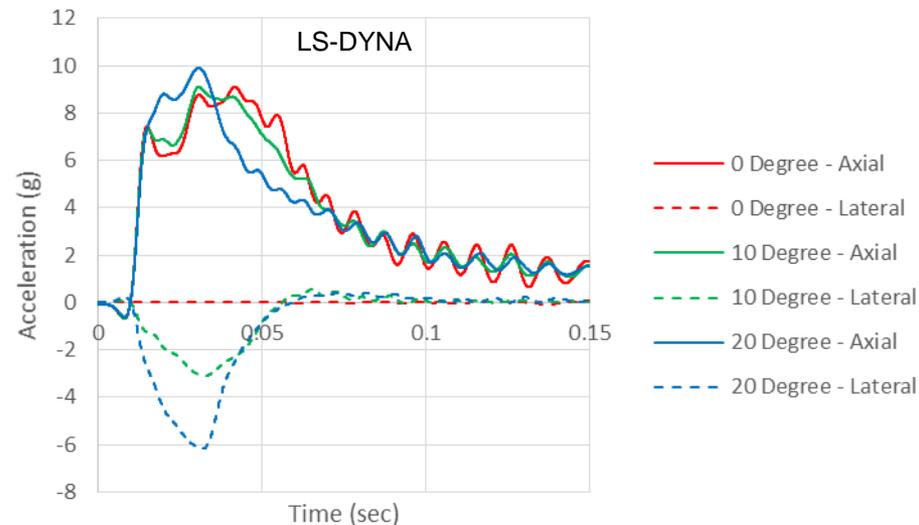
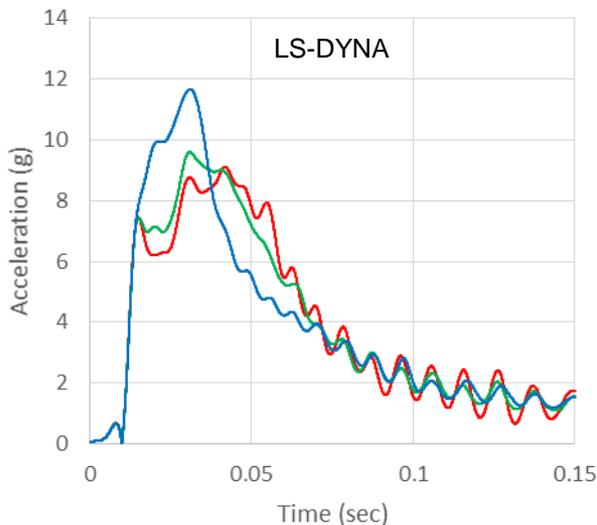
# Results: G-Loads

45° spherecone LS-DYNA compared to analytical

- Note two peaks seen in both LS-DYNA and numerical integration
  - 1<sup>st</sup> peak corresponds to  $\max dR/dh$  of spherical nose
  - 2<sup>nd</sup> peak occurs on cone

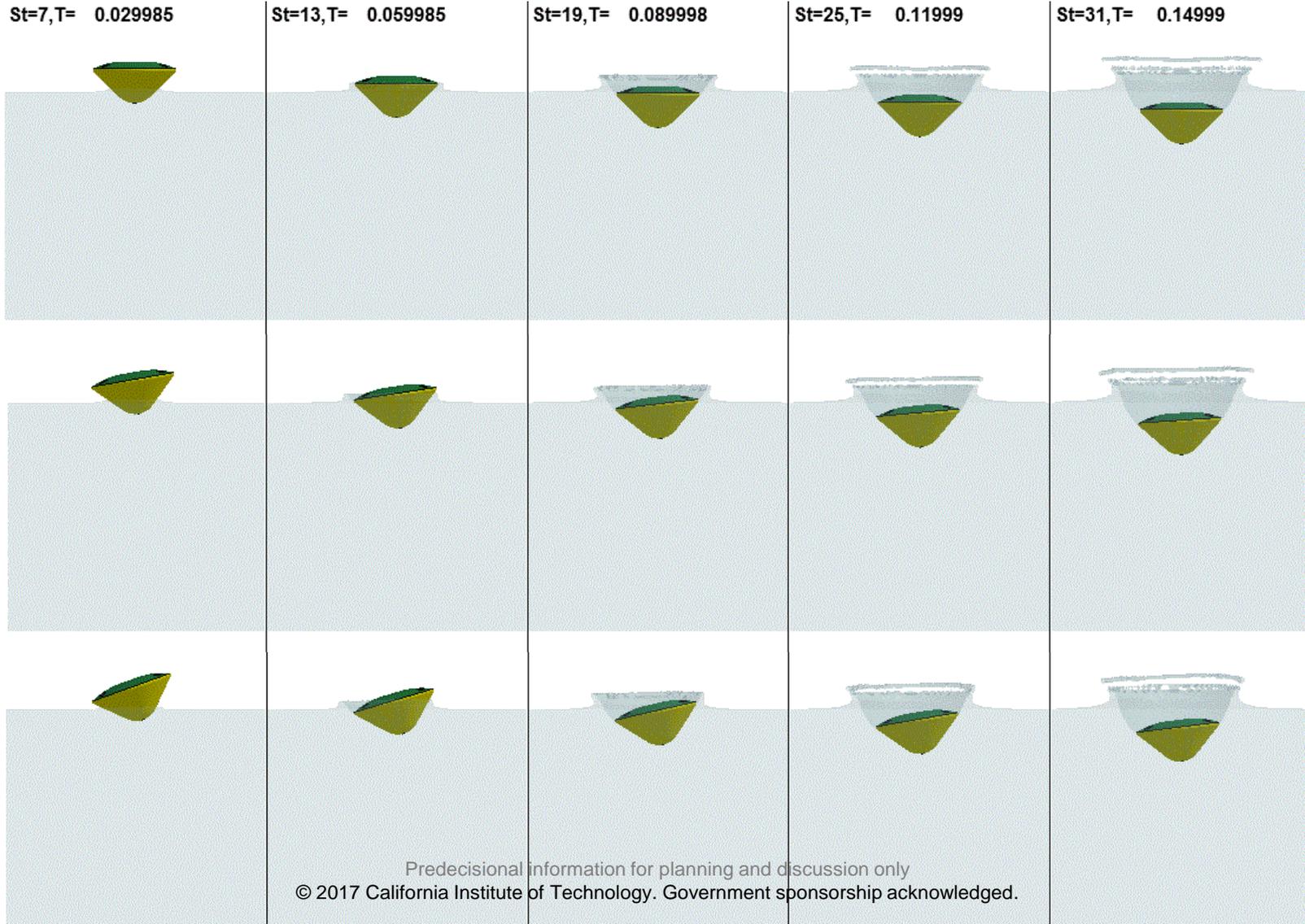


Method	Peak Acceleration [Earth G's]
Closed Form Spherical	9.4
Numerical Integration	10.4
LS-DYNA	9.0



# Results: G-Loads Motion Sequence

45 degree spherecone LS-DYNA, all cases



# Test Suite for Candidate Drag Plate Probe

## Case 1: Maximum Plunge Depth

$V_v = 12.5 \text{ m/s}$   
 $V_h = 0.0 \text{ m/s}$   
Angle = 0.0 degrees  
Liquid Density = 500 kg/m<sup>3</sup>



## Case 2: 0° Vertical High Load

$V_v = 12.5 \text{ m/s}$   
 $V_h = 0.0 \text{ m/s}$   
Angle = 0.0 degrees  
Liquid Density = 630 kg/m<sup>3</sup>



## Case 3: 30° Vertical High Load

$V_v = 12.5 \text{ m/s}$   
 $V_h = 0.0 \text{ m/s}$   
Angle = 30.0 degrees  
Liquid Density = 630 kg/m<sup>3</sup>



## Case 4: 0° Resultant High Load

$V_v = 12.5 \text{ m/s}$   
 $V_h = 3.4 \text{ m/s}$   
Angle = 0.0 degrees  
Liquid Density = 630 kg/m<sup>3</sup>



## Case 5: 15° Resultant High Load

$V_v = 12.5 \text{ m/s}$   
 $V_h = 3.4 \text{ m/s}$   
Angle = 15.0 degrees  
Liquid Density = 630 kg/m<sup>3</sup>



## Case 6: -30° Resultant High Load

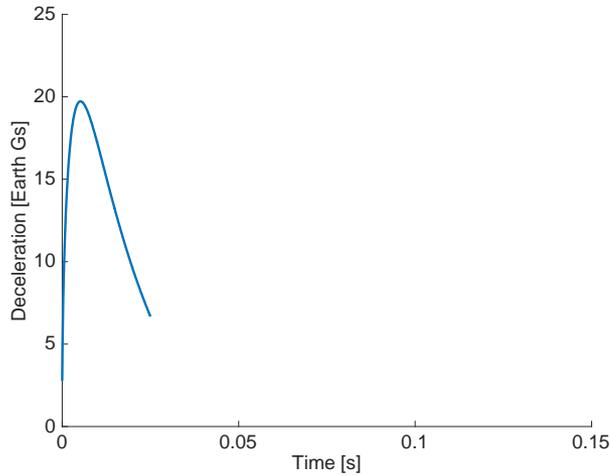
$V_v = 12.5 \text{ m/s}$   
 $V_h = 3.4 \text{ m/s}$   
Angle = -30.0 degrees  
Liquid Density = 630 kg/m<sup>3</sup>



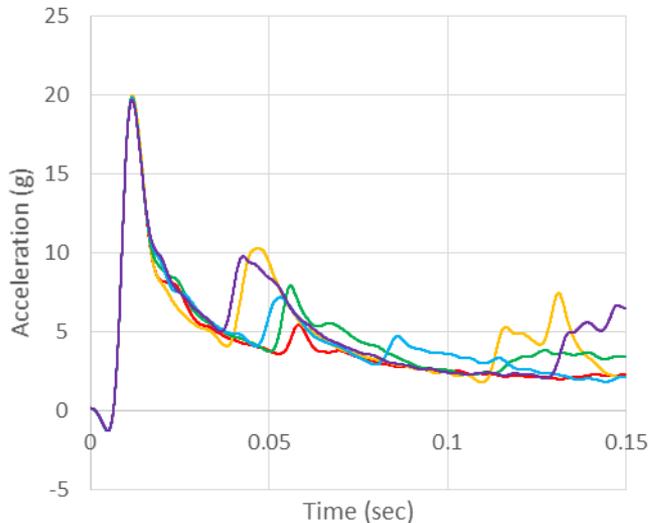
# Results: G-Loads

Drag Plate Case 2 (vertical only) LS-DYNA compared to analytical

- Drag plate not modeled analytically
- LS-DYNA sees second peak due to drag plate



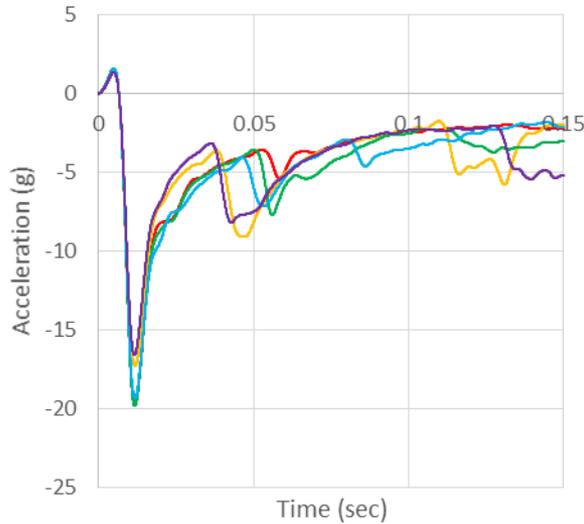
Method	Peak Acceleration [Earth G's]
Closed Form Spherical	21.9
Numerical Integration	19.7
LS-DYNA	20.0



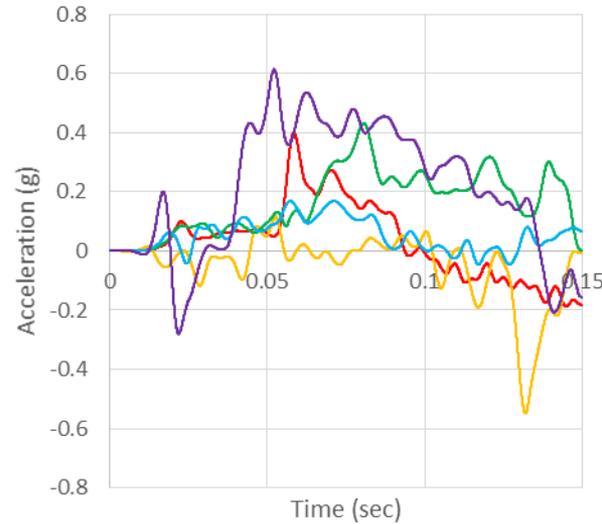
- Case 2 Resultant Acceleration
- Case 3 Resultant Acceleration
- Case 4 Resultant Acceleration
- Case 5 Resultant Acceleration
- Case 6 Resultant Acceleration

# Results: G-Loads

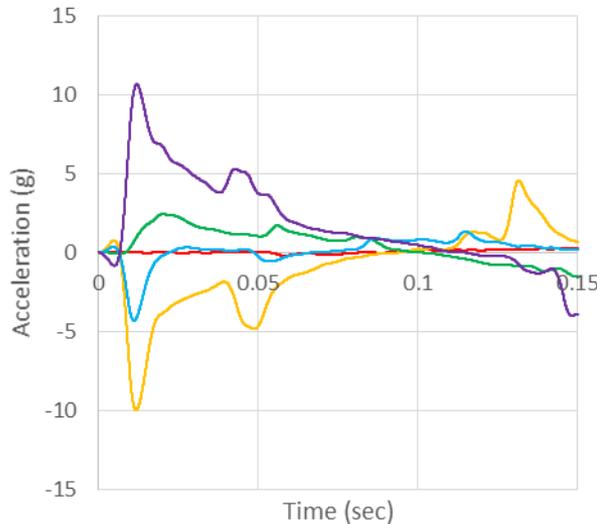
Drag Plate, LS-DYNA for all cases. X-axis is out the nose of vehicle



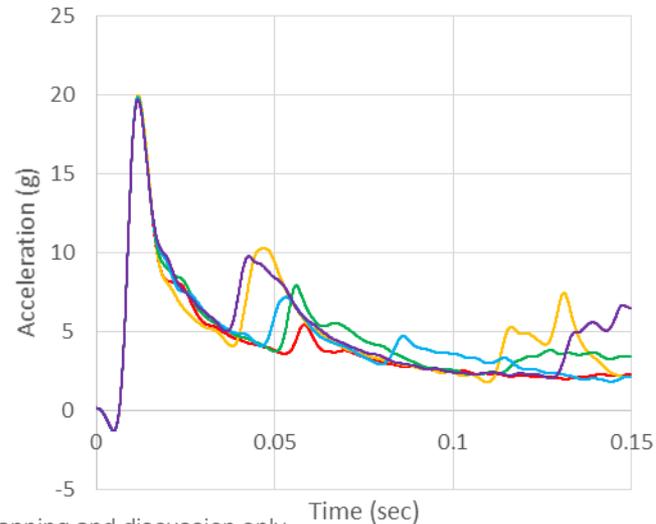
- Case 2 - X-Acceleration
- Case 3 - X-Acceleration
- Case 4 - X-Acceleration
- Case 5 - X-Acceleration
- Case 6 - X-Acceleration



- Case 2 Y-Acceleration
- Case 3 Y-Acceleration
- Case 4 Y-Acceleration
- Case 5 Y-Acceleration
- Case 6 Y-Acceleration



- Case 2 Z-Acceleration
- Case 3 Z-Acceleration
- Case 4 Z-Acceleration
- Case 5 Z-Acceleration
- Case 6 Z-Acceleration

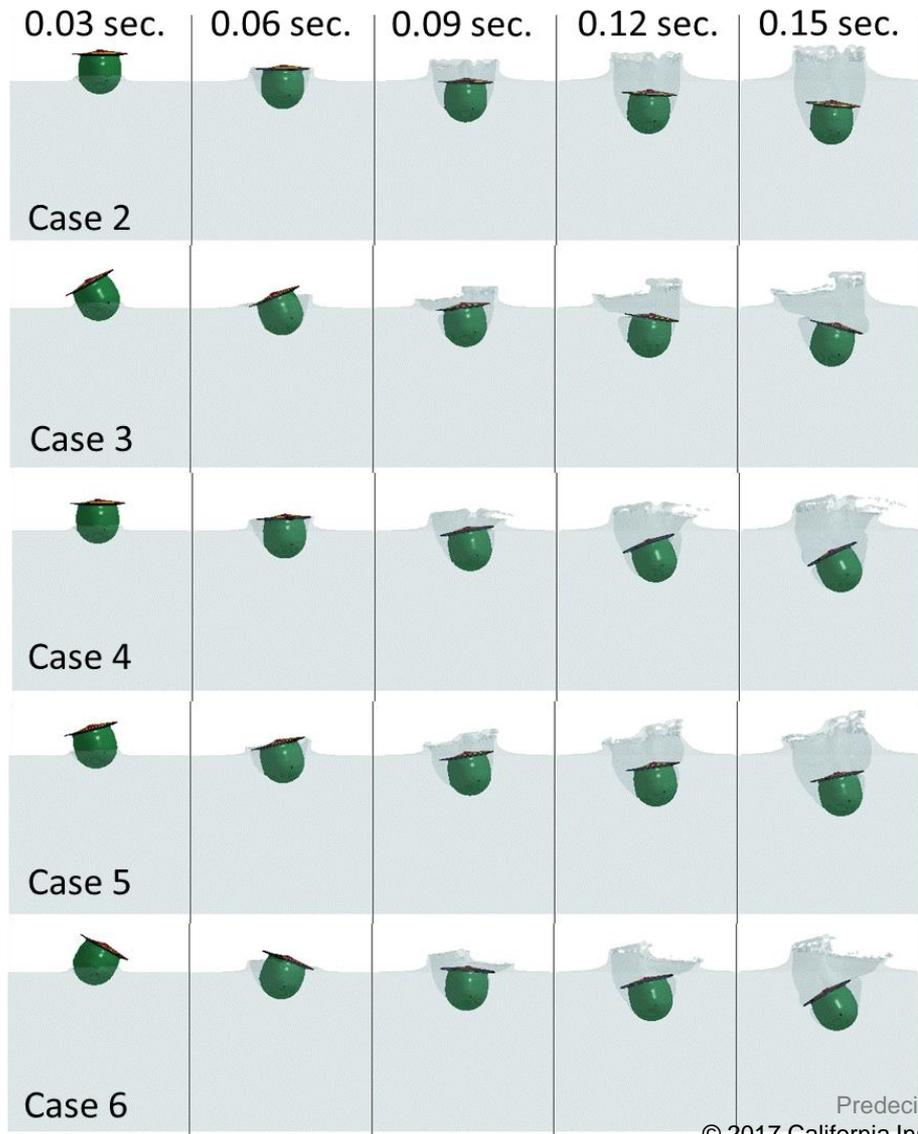


- Case 2 Resultant Acceleration
- Case 3 Resultant Acceleration
- Case 4 Resultant Acceleration
- Case 5 Resultant Acceleration
- Case 6 Resultant Acceleration

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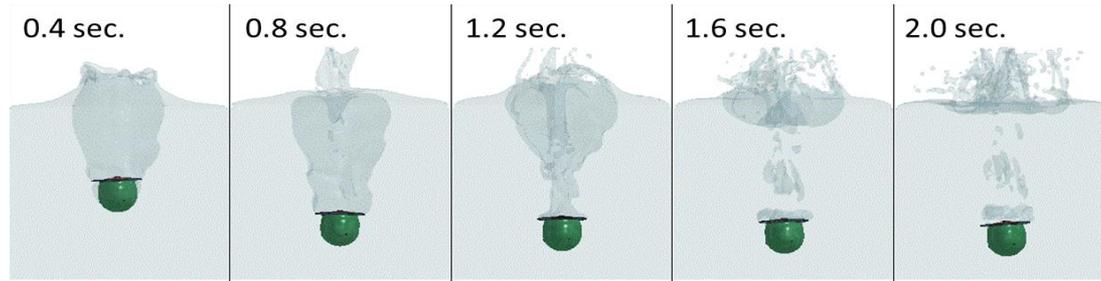
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# Results: G-loads Response Sequence

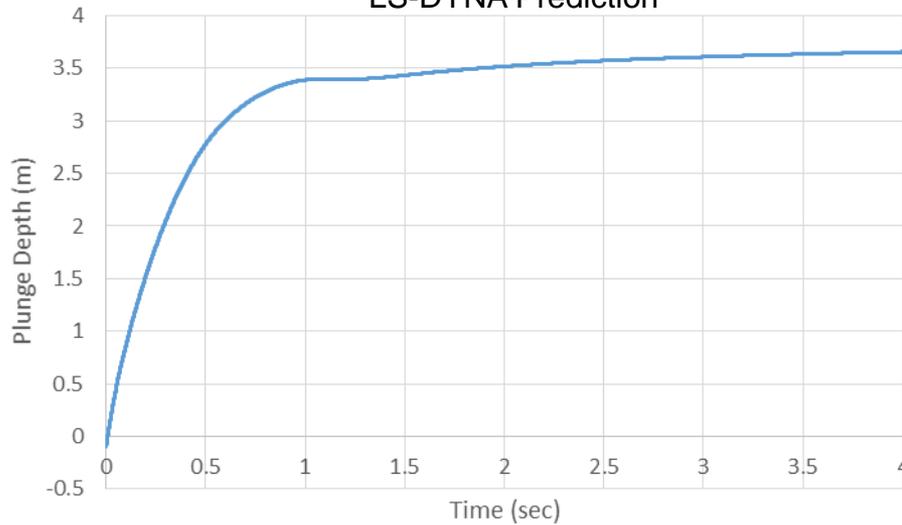


- Fluid impact phenomena predicted well compared to other experiments
- Note void above the plunging body

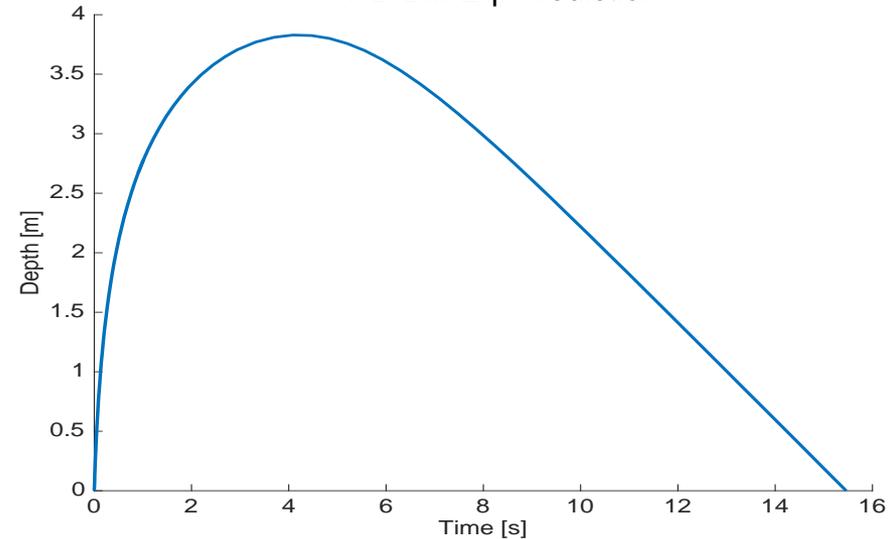
# Results: Plunge Depth



LS-DYNA Prediction



1-D Diff Eq. Prediction



Method	Plunge Depth [m]	Resurge Time [s]
Conservation Equations	4.2	10
Numerical Integration	3.8	15
LS-DYNA	3.7	-

# Conclusions

- Analytic expressions, LS-DYNA, and experiments (on other test articles) yield results within 20% of each other for normal impacts
  - Analytics useful for rapid initial scoping/screening of designs
- LS-DYNA accurately predicts impact loads and impact flow phenomena
  - Useful for determining lateral loads of off-vertical impacts
  - Valuable in calculating margin for instrument accelerations for off-nominal sea entries
    - Includes pitch angles and horizontal winds
- Resurge difficult to predict due to complex flow
  - Behavior of cavity is important
  - Solution also degrades over time
  - Run time becomes computationally expensive
  - Scale model tests and correlations may be useful
  - CFD may be more effective
- Simple models suggest plunge depth of ~4m and resurge time of ~10 s for baseline Titan probe design in this study
  - May permit measurement of conditions at depth
  - Tests and/or CFD needed to better understand vehicle depth and entrainment of liquid adjacent to probe surface





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# Back-up

# Related Work

- Von Karman: derived momentum approach for wedges entering water
  - To find max impact load for seaplane floats
- McGehee, et al: Theoretical and experimental water impact accelerations results for Mercury program
- Stubbs, et al: Experimental results for Apollo program
- Hirano and Miura: Closed form solution for peak load of spherical and conical shapes related to experimental results
- Lorenz, et al and Seiff, et al: Conducted experimental impact tests into water and kerosene for Titan probes Huygens and TiME

Test Results:



7/26/16

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