



An Innovative Very Low Thermal Power Waste Heat Recovery System for Thermal Control of Deep Space Missions

- A Thermal Flask in Space

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Agenda

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Problem Statement

- Typical deep space missions like Juno (to Jupiter at ~5 A.U.) and the currently envisioned Europa Clipper Mission (to Europa, a moon of Jupiter) would rely on solar photovoltaic power
 - Need extremely large & heavy solar arrays because solar intensity is so low at those locations
- Also would require as much as 200-300 W of electrical power for thermal control due to their size
- Hence any power that would be needed for thermal control is extremely limited
- This is prohibitively large and leads to needing very large and heavy solar arrays (on the order of ~20-30 m²) *just for thermal reasons*
- Hence there is a need to come up with a thermal architecture and design that would not need such prohibitively large thermal power levels
- Power needs for thermal control are related to keeping typical spacecraft components within their allowable temperature limits
 - Propulsion System: +15°C → +50°C; Electronics: -40°C → +50°C; Battery: -20°C → +30°C



Typical Environments Encountered

- **Near Earth Cruise**
 - *Warm* (benign); 1 A.U.
- **Possible Venus Gravity Assist (e.g., Venus)**
 - *Very Hot* (Worst Case Hot) Case; ~0.7 A.U.
 - 2x Sun flux from Sun (Direct)
 - 1.5x Sun Flux from Venus (Albedo)
- **Cruise to Outer Planets**
 - *Very Cold* (Worst Case Cold) Case; as far as ~10 A.U.
 - 90-130 K sink temperature at outer planet



Description of Proposed Architecture

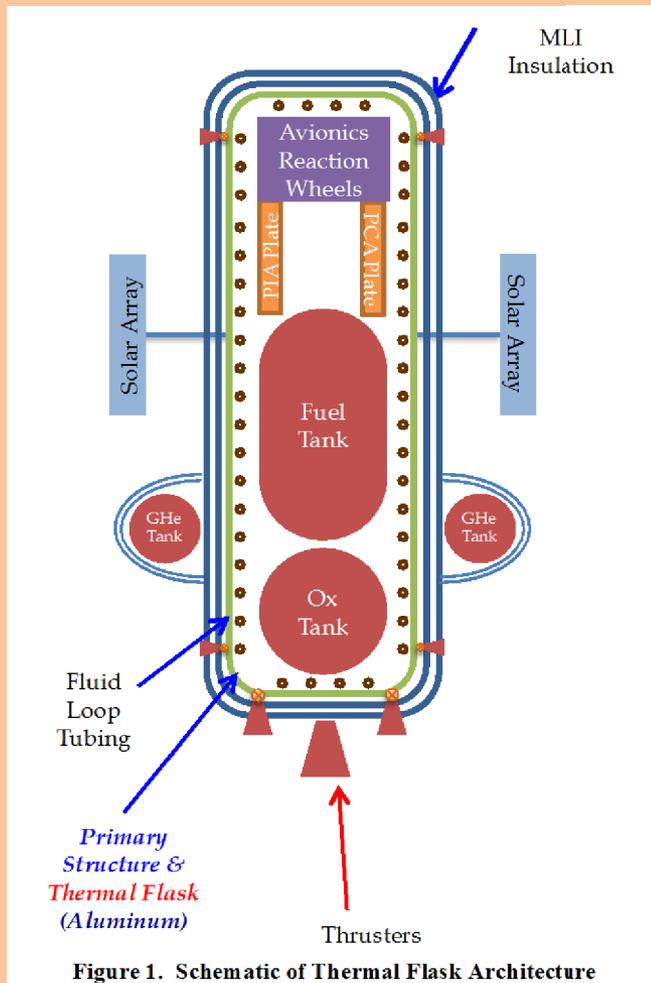
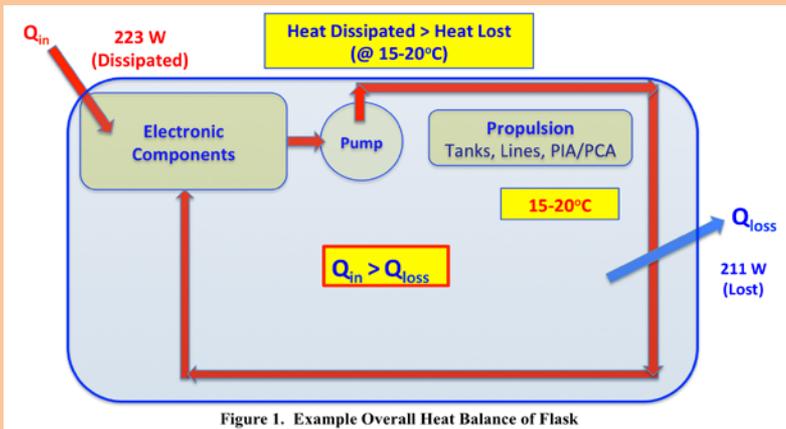


Figure 1. Schematic of Thermal Flask Architecture

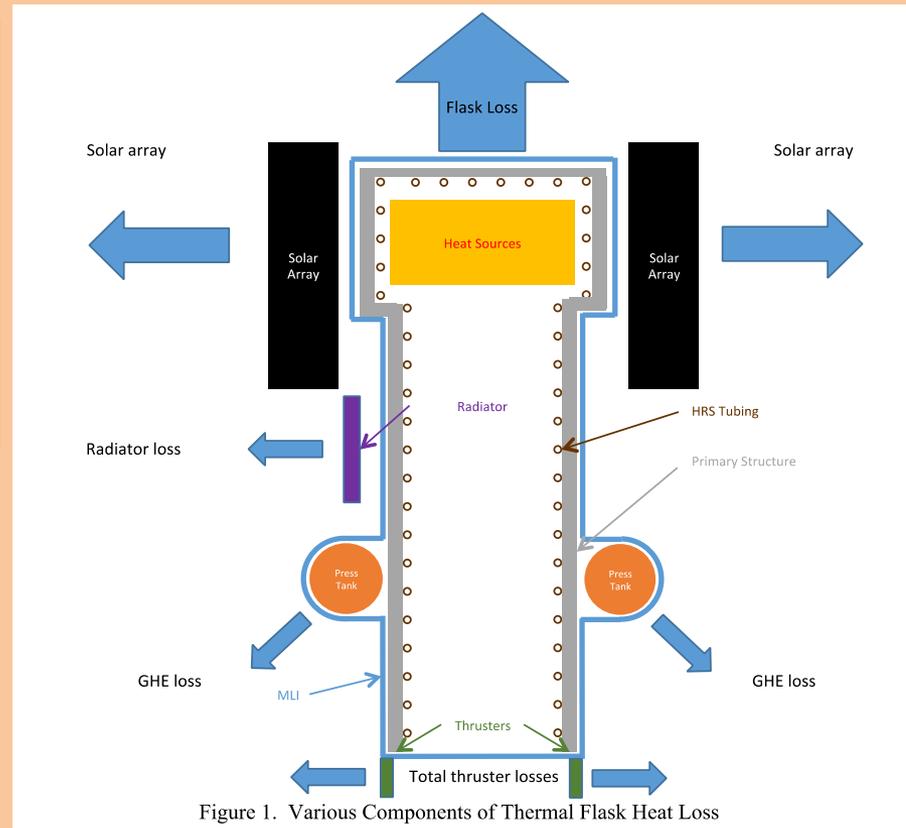
- **Harvest waste heat from heat dissipating components**
 - Avionics, Instruments, Telecom, ACS, etc.
 - Dissipate ~200 W for reasonable spacecraft functionality
- **Waste heat comparable to that required for components that need survival heat**
 - Propulsion system, etc.
 - Need ~ 200 W for thermal control
- **Pick up waste heat by single phase fluid loop tubing & supply to components that need it via tubing attached to it**
 - Mechanical pump is prime mover of fluid
- **Hence create a thermal flask that has fluid loop tubing attached to it**
 - All key s/c components reside in flask
 - Except for solar array, antennae, thrusters, instrument apertures, etc.
 - Entire flask is covered with MLI blankets



Example Heat Balance

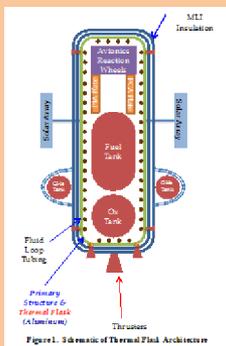


- Almost isotherm flask (due to fluid loop)
- Maintains flask's temperature around 15-20 C
- Minimal use of heater power to augment waste heat harvested





Novelty of Architecture

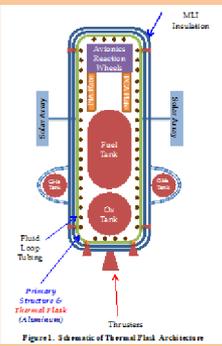


- *This is a novel concept that could enable missions because it could almost eliminate the need for thermal control power for a large size spacecraft that is designed for deep space*
- Without this concept, missions could potentially be prohibitively heavy & expensive to provide large amount of power for thermal control in extremely cold environments that such missions would encounter
- This concept is completely automatic
 - Requiring no on-board or ground directed control of its function
- It is also quite simple in its implementation because all the spacecraft components would be placed inside an aluminum shell with standard MLI insulation covering it
 - *Thermal Flask shell has dual function of s/c structure & thermal control*
- This work is radically different from previous missions that utilized solar arrays for power where electrical heaters (~200 W) were utilized just to thermally control the spacecraft components
- Missions that had Multi-Mission Radioisotope Generator (MMRTG) nuclear power sources (e.g., Cassini) did not encounter this problem because of ample waste heat available from MMRTGs
- Solar missions do not have that luxury, hence the need to come up with novel schemes like the one proposed here to enable them



Heritage & Technology Assumptions

- **The fluid loops utilized to make this architecture work have a long and extremely successful heritage from JPL's Mars missions**
 - Starting from Mars Pathfinder (MPF)
 - Followed by the two Mars Exploration Rovers (MERs, Opportunity and Spirit)
 - And the recent Mars Science Laboratory (MSL) Curiosity Rover mission
- **In particular, the Curiosity Rover utilized waste heat from the MMRTG to thermally control the rover on Mars**
- **HRS (fluid loop) technology is well established (TRL-9) for last ~20 years for application in extremely successful spaceflight projects**
- **Number of pumps inside an assembly can be further increased for long life missions to increase reliability**
 - MSL Cruise HRS pump assembly has 3 pumps, 2 redundant, only one on at any time
 - This would lead to an insignificant mass increase with no change in power
- **MLI blanket properties have been well characterized for several decades on several flight projects**
 - For large and small size blankets



Other Options Investigated

- **Due to severe power constraints, only options that harvested waste heat from components to service other components (like propulsion) were considered:**
 - Options that relied on significant use of electrical heat were deemed unattractive
 - Due to reasons cited before
 - Fluid loop (HRS) based thermal bus was the most logical option for thermal control
 - For cold and hot conditions
 - Heat pipes or loop heat pipes were not deemed to be as attractive
 - From testing, integration, ATLO, and modularity reasons as well as a multi component serving autonomous thermal bus
- **Within the HRS approach, an earlier option considered was to employ local HRS plate clamshells to surround propulsion system to maintain their temperatures:**
 - Smaller surface area/mass of plates
 - Would need thermal isolation of these components from the cold structure
 - Which would be difficult to satisfy simultaneous thermal and structural needs
 - Heat losses via conduction & MLI around clamshells would be comparable to an all enclosing thermal flask
- **Thermal flask approach that encloses the entire spacecraft except solar arrays, Helium tanks, thrusters and some small components was found to be the most attractive**
 - Integrated structure and thermal flask system
 - ~3 mm or 1/8" thick aluminum shell with local stiffening features
 - Reasonable total mass
 - All components inside flask are thermally and mechanically coupled to integrated structure/flask
 - No need for thermal isolation based complexity

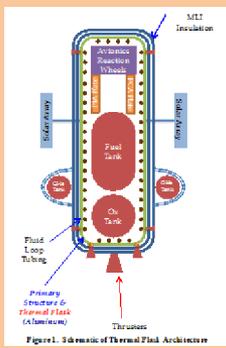


Rules of Thumb for Sizing & Performance

- The heat loss from the flask should be proportional to the external surface area of the flask for a given controlled temperature as shown below:

$$Q = \sigma \epsilon A (T_{flask}^4 - T_{sink}^4)$$

- The total heat loss would then be simply the harvested heat plus any heat dissipation in the locations where the heat is supplied
 - e.g. propulsion module

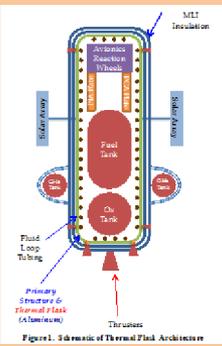


Applicability & Limitations

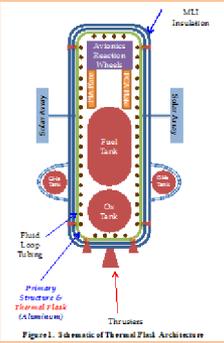
- **Obviously this architecture is most well suited for missions that are very power-starved and which could encounter very cold environments**
 - Like the ones that go to outer planets
- **Key assumption is that significant amount of dissipation is present from which waste heat could be harvested**
- **This architecture relies on enclosing all (or most) thermally controlled components within the flask**
- **If the configurational constraints present a challenge to this assumption then a single flask concept may not work as well**
 - And it would have to be broken into mini-flask-regions
 - Which would make the configuration more complicated to implement
- **There will inevitably be some components that will have to protrude out of the flask**
 - e.g., solar array and supporting structure, thrustors, apertures of star scanner, sun sensor, instruments, radiators, etc.
- **There would be some thermal-mechanical design challenges to minimize these parasitics to minimize the waste heat recovery required to overcome all the heat losses**



Possible Improvements



- **Reduction of MLI blanket emissivity would directly benefit the thermal design's efficiency**
 - Since the primary heat loss from the flask and correspondingly the required harvested heat is directly proportional to the MLI blanket effective emissivity
- **The large blanket surfaces that would cocoon the flask would be amenable to substantial improvements because the edge seam losses can be minimized**
 - The edge seam losses are the largest contributors of MLI emissivity increase due to local compaction of the blanket layers
- **Additionally, two mechanically separated blankets, which are not in contact with each other, could greatly reduce the heat loss**
- **Maximization of packing of components within the flask envelope would also minimize heat loss**
 - Because the external surface area of the flask is what determines the total loss
 - So anything that could fit inside would already have its heat loss accounted for by loss from flask external area
- **Minimizations of protrusions out of the flask would also be beneficial**
 - Since those external components would tend to run cold and would increase the parasitics losses from the controlled warm surfaces of the flask



Conclusions

- **The thermal flask architecture presented in this paper describes an attractive, practical, simple and power efficient approach for the thermal design of future deep space solar power based missions**
 - That are extremely power starved due to the very small solar flux available at large distances from the Sun
- **It relies on harvesting waste heat from heat dissipating components via mechanically pumped fluid loop tubing**
 - And then, via the same tubing, directing it to a “thermal flask” that contains all the essential thermally controlled spacecraft components within it
- **The thermal flask serves as the spacecraft structure as well as a thermal cocoon to create a warm environment that the spacecraft components are slaved to**
- ***The simplicity, robustness and low thermal power needs of this approach, along with the ease in its implementation and testing makes it a very enabling architecture for future deep space missions***



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