

Deployment of the MARSIS Radar Antennas

On-board Mars Express

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A GO for deployment was reached only in 2005. Risk analyses recommended safing measures to minimize potential impact on vital spacecraft elements and to verify its health and configuration after the deployment of each boom, which vastly increased the operational complexity. A simulations campaign in April 2005 prepared the mission team for these critical operations, while a flight pre-deployment test campaign was executed in the gaps not used by the science mission.

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Meanwhile, no one worried about the approximately one minute of the actual deployment transient. Each 20 m boom had mass of 1-kg. The structure was so large and light, there was no real way to test it in Earth gravity and atmosphere. Astro Aerospace developed a simulation program to model the deployment transient. The result appeared sufficiently benign that no one actually questioned the validity of the model. In April 2004, while working with a deployment simulation of the antenna for the SHARAD instrument (SHALLOW RADAR, an instrument on NASA's Mars Reconnaissance Orbiter), an error in the way damping was modeled in the software was discovered. When corrections were made to the MARSIS deployment model, the results were highly chaotic and so different from the previous results that proceeding with MARSIS deployment at that time would have been irresponsible. The Mars Express-NASA Project Manager notified ESA of the need to postpone the scheduled deployment. As it happened, this realization and notification took place a mere 12 hours before ESA was to load the deployment sequence aboard the spacecraft.

The expected science value was such the deployment was very desirable. JPL spent the next four weeks attempting to identify and solve the problems. At a review with ESTEC on May 14, 2004, it became apparent that too little was actually known about the real deployment expectations and the mechanical properties to proceed. JPL then put together what amounted to a retroactive qualification effort, considering the flight article was already at Mars and only the Engineering Model was available to test. This effort will be described later.

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Impact on the SC attitude control during and after the deployment; resulting attitude controllers for the whole deployment phase.

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Basic requirements for characterization of the deployment

E. Operations and Commissioning Constraints

Alan M.?

(also include the trade-off on the deployment target date as early / as late as possible: science demo phase for the optical instruments just after Mars arrival, concerns of the other PIs, maximum eclipse duration...)

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B. The Point of View of the Marsis Principal Investigator

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C. Boom Deployment Studies

One of the key issues with a lightweight, large motion, and highly dynamic deployment such as MARSIS is that friction, gravity, and aerodynamic resistance forces will dominate any attempts at ground based testing. The boom is extremely light weight and its properties are also temperature dependent. As a result of the influence of these forces it impossible to test the full system behavior prior to flight and we must rely on analysis to predict the deployment dynamics. Due to the infeasibility of a full system test, a computational study was used to determine the critical controlling parameters of the deployment which resulted in narrowing the planned component testing to three major parameters: the hinge buckling strength, the hinge torque profile, and the stowed compressive energy.

The hinge buckling strength was measured using sections of the flight spare boom in a four-point bending fixture. Results from this test indicated that the in-situ hinge strength of the flight booms was lower than previous measurements had suggested and that buckling could occur both in the hinge section and in the material immediately adjacent to the hinges. Additionally, the hinge deployment torque was measured in an environmental chamber at its on-orbit temperature of -70 C to better characterize its contribution to the deployment energy as well as the hysteresis energy dissipation associated with any hinge buckling events. Finally, the stowed energy due to the compression of the tube diameter in the cradle was measured in a vacuum chamber at -70 C for all three booms.

The boom deployments were simulated using a highly specialized ADAMS model. The model was constructed with 13 straight segments connected by spline hinge joints that reproduced the measured hinge torque profile and buckling strengths. Each of the 13 straight segments was composed of two beam elements that employed an automated algorithm to update the structural (stiffness proportional Rayleigh) damping parameter based on the local straight section beam length and end conditions. Finally, the accordion style stowed state was modeled with gap springs connecting adjacent boom segments in order to capture the stowed compressive energy.

A total of 1000 cases of the ADAMS model were run in a Monte Carlo study of the deployment dynamics. One of the key results from the Monte Carlo analysis was the discovery that a number of scenarios were possible that could result in the boom re-contacting the spacecraft during the deployment. Due to the high compressive energy the dipole boom reaches its full 20 m length in about 2.5 seconds, after which, it typically experiences a "whip" type behavior and tends to fold back towards the spacecraft in two or more sections. The margin against boom re-contact was quantified based on the closest buckled hinge after the full length of the boom was reached and it was exhibiting recoiling motion.

Results from the Monte Carlo study indicated that there was a significant probability that the MARSIS booms could contact the spacecraft or solar arrays during the deployment. Based on this result, a failure modes analysis was done at ESA using the energies and incidence angles obtained from the Monte Carlo runs. The conclusion of this analysis was that, while significant damage to the spacecraft was possible, the likelihood of it occurring was very low. Hence, the decision was made to proceed with the deployment.

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(usage of MCR, shifts, organization)

B. The First Boom: An Excellent Spacecraft Behavior

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C. The First Boom : an Unexpected Behavior

Having spent a year working the technical issues involved in deployment, the ESA/NASA JPL/EADS Astrium team approached the scheduled May 4, 2005 deployment with enthusiasm and confidence. At first impression of the event, deployment appeared successful. There was a significant tip off motion of the spacecraft, followed by jerky motions of the dynamics, concluding with a damped sinusoidal behavior. Champagne time at ESOC!

However, detailed analysis of the flight telemetry showed a total of three clearly observable frequencies at 0.043 Hz and 0.146 Hz about one axis and the third at 0.076 Hz about the other axis instead of the expected pair of frequencies near 0.10 Hz. These measured frequencies were completely unexpected. The moments of inertia data for the spacecraft also were not consistent with a single segment boom. The anomalous inertia cross-product values and the smaller than expected principal axis values suggested a partial deployment with a "bent" end. Both the frequency and inertial data were consistent with the 10th hinge from the spacecraft being stalled at a 40° angle. An "even" numbered hinge would have been colder than an "odd" numbered hinge and would have been pre-bent away from the sun direction.

Test data taken months before on the hinge torque versus angle characteristic at very cold temperature showed a small region of negative torque at about 40°. If the boom deployment energy had reached zero with the boom segment bent greater than 40° deg at hinge-10, the segment could easily remain "stuck". Thus a 40° partially deployed hinge-10 was the likely condition. As it happened, the sun angle at that hinge was such that it gave the least possible warming, thus adding strength to the theory.

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E. How to Unbend The First Boom

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Appendix

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B. The Point of View of the Marsis Principal Investigator

Enrico??

C. Boom Deployment Studies

One of the key issues with a lightweight, large motion, and highly dynamic deployment such as MARSIS is that friction, gravity, and aerodynamic resistance forces will dominate any attempts at ground based testing. The boom is extremely light weight and its properties are also temperature dependent. As a result of the influence of these forces it is impossible to test the full system behavior prior to flight and we must rely on analysis to predict the deployment dynamics. Due to the infeasibility of a full system test, a computational study was used to determine the critical controlling parameters of the deployment which resulted in narrowing the planned component testing to three major parameters: the hinge buckling strength, the hinge torque profile, and the stowed compressive energy.

The hinge buckling strength was measured using sections of the flight spare boom in a four-point bending fixture. Results from this test indicated that the in-situ hinge strength of the flight booms was lower than previous measurements had suggested and that buckling could occur both in the hinge section and in the material immediately adjacent to the hinges. Additionally, the hinge deployment torque was measured in an environmental chamber at its on-orbit temperature of -70 C to better characterize its contribution to the deployment energy as well as the hysteresis energy dissipation associated with any hinge buckling events. Finally, the stowed energy due to the compression of the tube diameter in the cradle was measured in a vacuum chamber at -70 C for all three booms.

The boom deployments were simulated using a highly specialized ADAMS model. The model was constructed with 13 straight segments connected by spline hinge joints that reproduced the measured hinge torque profile and buckling strengths. Each of the 13 straight segments was composed of two beam elements that employed an automated algorithm to update the structural (stiffness proportional Rayleigh) damping parameter based on the local straight section beam length and end conditions. Finally, the accordion style stowed state was modeled with gap springs connecting adjacent boom segments in order to capture the stowed compressive energy.

A total of 1000 cases of the ADAMS model were run in a Monte Carlo study of the deployment dynamics. One of the key results from the Monte Carlo analysis was the discovery that a number of scenarios were possible that could result in the boom re-contacting the spacecraft during the deployment. Due to the high compressive energy the dipole boom reaches its full 20 m length in about 2.5 seconds, after which, it typically experiences a "whip" type behavior and tends to fold back towards the spacecraft in two or more sections. The margin against boom re-contact was quantified based on the closest buckled hinge after the full length of the boom was reached and it was exhibiting recoiling motion.

Results from the Monte Carlo study indicated that there was a significant probability that the MARSIS booms could contact the spacecraft or solar arrays during the deployment. Based on this result, a failure modes analysis was done at ESA using the energies and incidence angles obtained from the Monte Carlo runs. The conclusion of this analysis was that, while significant damage to the spacecraft was possible, the likelihood of it occurring was very low. Hence, the decision was made to proceed with the deployment.

D. Spacecraft Protection Strategy

Eric?

E. Operations Coordination and In-flight Tests

Alan M.?

F. Operational Timeline Preparation

Zeina?

G. Preparation and Verification of Attitude Control Products

Jay, Joerg??

IV. The Deployment and Its Surprises (May-June 2005)

A. Overall Execution Conditions

Michel / Alan M.
(usage of MCR, shifts, organization)

B. The First Boom: An Excellent Spacecraft Behavior

Eric

C. The First Boom : an Unexpected Behavior

Having spent a year working the technical issues involved in deployment, the ESA/NASA JPL/EADS Astrium team approached the scheduled May 4, 2005 deployment with enthusiasm and confidence. At first impression of the event, deployment appeared successful. There was a significant tip off motion of the spacecraft, followed by jerky motions of the dynamics, concluding with a damped sinusoidal behavior. Champagne time at ESOC!

However, detailed analysis of the flight telemetry showed a total of three clearly observable frequencies at 0.043 Hz and 0.146 Hz about one axis and the third at 0.076 Hz about the other axis instead of the expected pair of frequencies near 0.10 Hz. These measured frequencies were completely unexpected. The moments of inertia data for the spacecraft also were not consistent with a single segment boom. The anomalous inertia cross-product values and the smaller than expected principal axis values suggested a partial deployment with a "bent" end. Both the frequency and inertial data were consistent with the 10th hinge from the spacecraft being stalled at a 40° angle. An "even" numbered hinge would have been colder than an "odd" numbered hinge and would have been pre-bent away from the sun direction.

Test data taken months before on the hinge torque versus angle characteristic at very cold temperature showed a small region of negative torque at about 40°! If the boom deployment energy had reached zero with the boom segment bent greater than 40° deg at hinge-10, the segment could easily remain "stuck". Thus a 40° partially deployed hinge-10 was the likely condition. As it happened, the sun angle at that hinge was such that it gave the least possible warming, thus adding strength to the theory.

D. Stop or Go?

Alan S.

E. How to Unbend The First Boom

Mike.

F. A Minor Anomaly and its Drastic Consequences

AOCS Acquisition Control Board (ACM-B) Telemetry wraparound.
Alan M..

G. The Second Boom Deployment

Michel

H. The Monopole

Joerg.

V. Conclusion

Michel and others

Appendix

<needed ?>.

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References

Periodicals
<any? >

Books
<any? >

Proceedings
<any? >

Reports, Theses, and Individual Papers
<any? >

Electronic Publications
<any? >

Computer Software
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