



GaAs based Terahertz Sources for Space Applications: Challenges and Prospects

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Outline

- Introduction
- Requirements and current capability
- Technology development Road map
- Status of power sources in $f < 1000$ GHz range
- Status of power sources in $f > 1000$ GHz range
- Challenges
- Conclusion



Introduction

- Traditional space borne submillimeter-wave sources
 - Gunn diode + whisker contacted Schottky diode multipliers
- Limitations
 - Instantaneous bandwidth of Gunn diodes is very limited
 - Power combining is difficult
 - Whisker contacted diodes are extremely difficult to assemble
 - commercial availability of both Gunn diodes and whisker contacted high frequency diodes is limited
 - multiple diode configurations are not readily possible



Prospective source to 2400 GHz

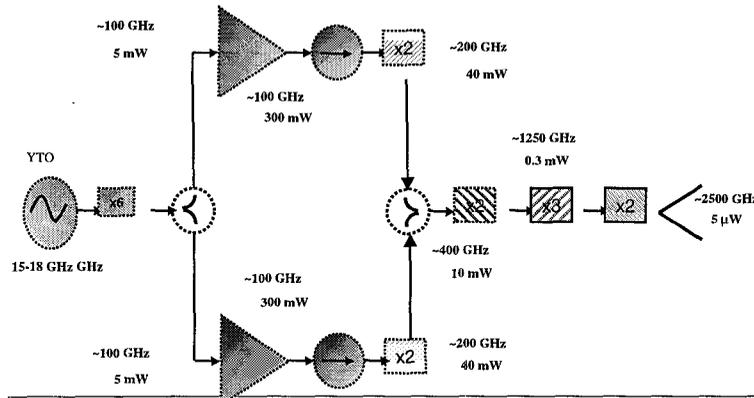


Figure 1. Schematic of the all-solid-state source to 2500 GHz. Dashed outlined components are either commercially available or have already been demonstrated in our laboratory. Solid outlined components are to be developed under this proposal.

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Technology Development Roadmap

- Increase available power at 100 GHz
- Use balanced multiple diode arrays in the earlier stages
- Use planar technology
- Waveguide based circuits
- Enhance performance by radiative cooling

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Increase available power at 100 GHz

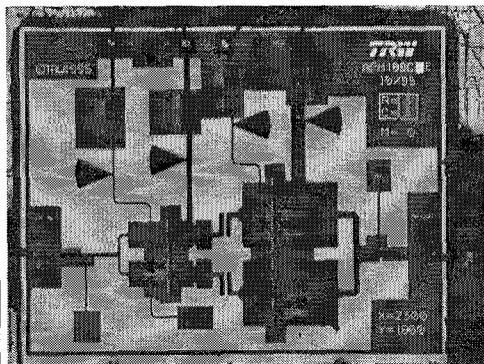
- Current status: Gunn diodes limited to about 100mW at 100 GHz
- Solution: Power Amplifier technology
 - Utilize power combining
 - Issues
 - technology
 - efficiency
 - noise

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TRW MMIC PA Chip



- 0.1 μm PHEMT process
- 50 μm thick substrate
- $f_t = 200$ GHz
- 64 finger device cell (output)
- on-chip bias network
- 50 ohm matching in/out
- 2.3 mm x 1.8 mm

Ref: R. Lai et. al, "A high efficiency 0.15 μm 2-mil thick InGaAs/AlGaAs/GaAs V-band power HEMT MMIC," IEEE GaAs IC Symposium Digest, Nov. 1996.

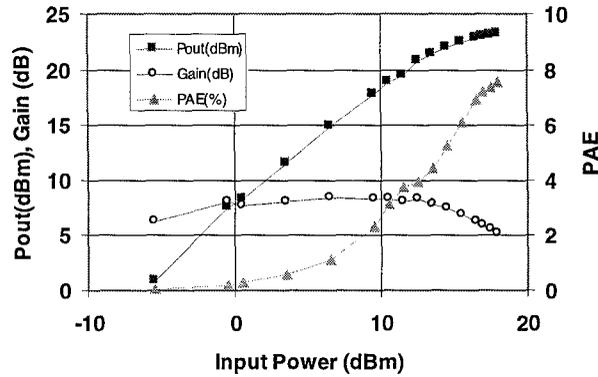
M. D. Biedenbender et al, "A 0.1 μm W-band HEMT production process for high yield and high performance low noise and power MMIC's," 16th GaAs IC Symposium, 1994.

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Performance of prototype single chip module

Measured output power in Block B
(@91 GHz) Flange-to-flange



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Power combined amplifier module

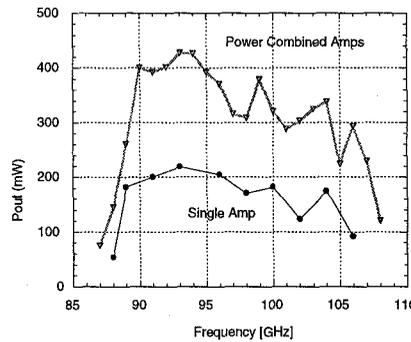
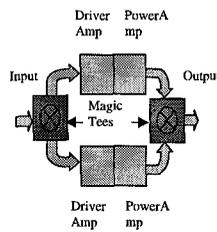


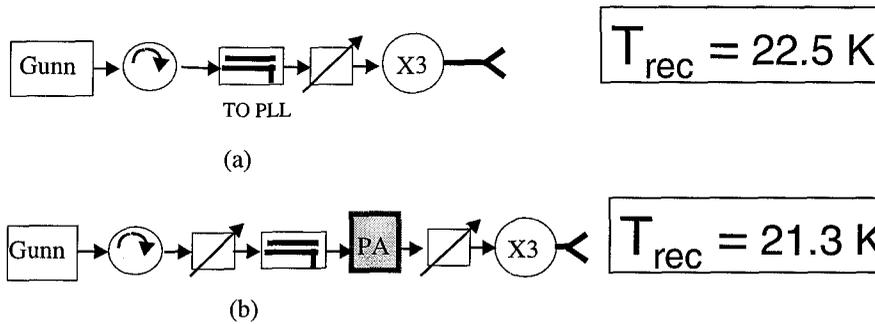
Figure 2. Power output from single and dual power combined packaged TRW MMIC amplifiers at W-band.

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Noise considerations for power amplifiers

Test with a SIS 278 GHz receiver
at CSO on Mauna Kea, Hawaii



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Current status of planar Technology for initial stages $f < 1 \text{ THz}$

- Discrete chips
- Substrateless technology
- thermal issues
- cooling effects

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First stage multipliers

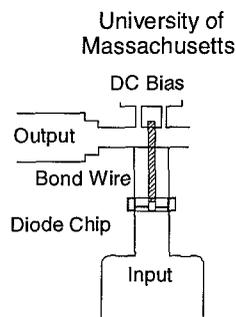
- Current status: whiskered devices
- Solution: Planar multiplier devices
 - Multiple diode configuration
 - Higher power handling
 - Balanced approach
 - Simplify design, circuit construction
 - Issues
 - Technology
 - Device yield
 - Thermal management

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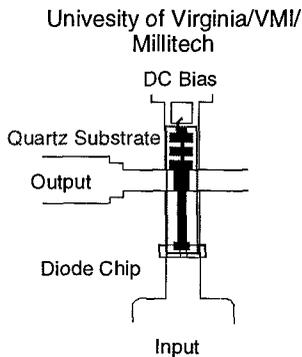
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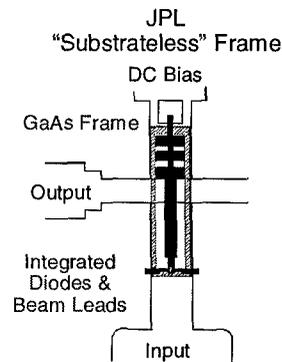
Planar Balanced Doubler Technologies Based on Neal Erickson Split-Block Concept



- ! Chip soldered to block
- ! Bondwire connects chip to DC Bias Cap



- ! Chip soldered to block or Quartz
- ! Bondwires connect quartz to Bias Cap and to block (for chip on quartz version)



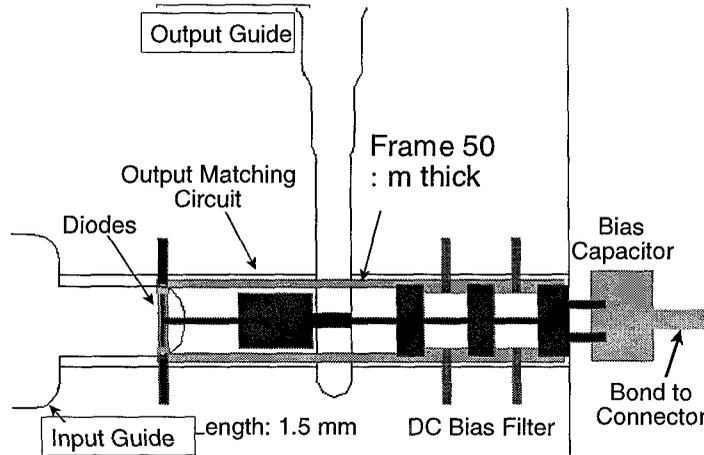
- ! All chip connections to block made with beam leads
- ! Diodes integrated into circuit
- ! GaAs under metal removed for low loss

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400 GHz Substrateless Circuit in Block

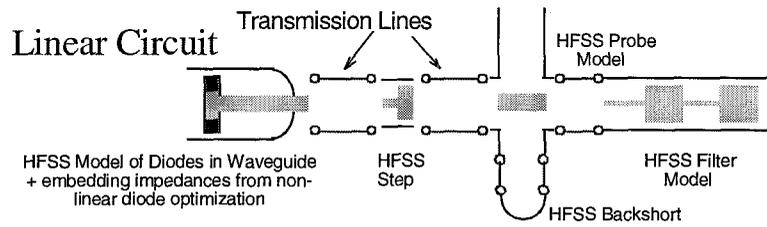


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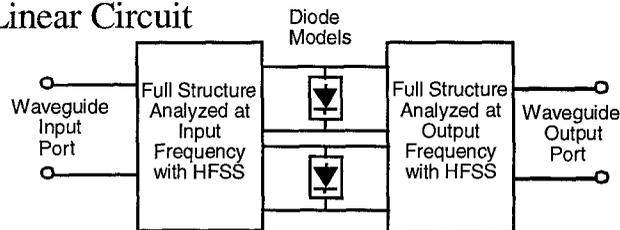
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Doubler Design Strategy



Non-Linear Circuit

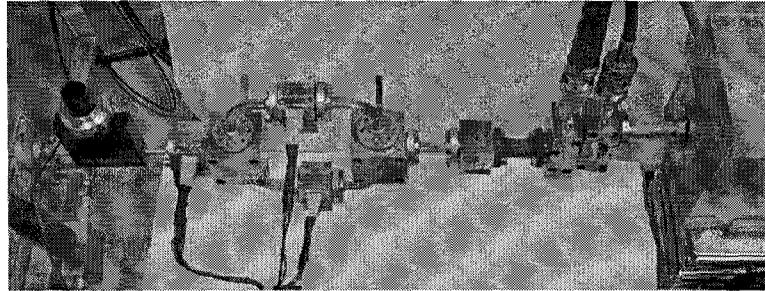
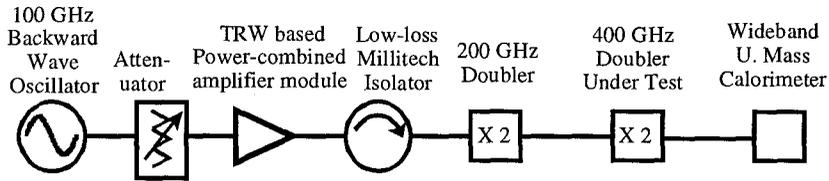


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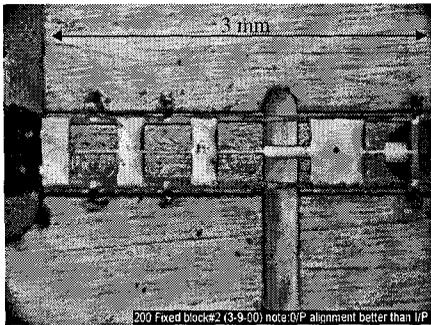
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400 GHz Doubler Test Set



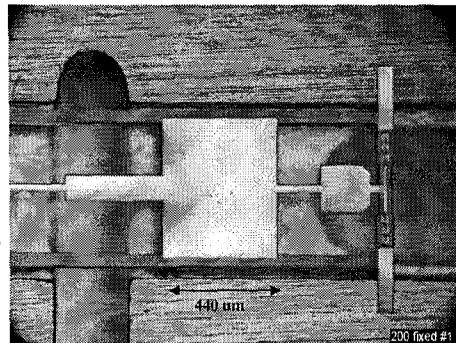
Substrateless Technology for 200 GHz MMCs



Full view of structure mounted in a waveguide block

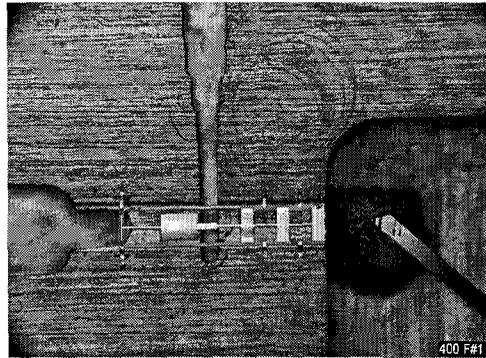
Close-up of the anodes

Gives 8% efficiency, despite design flaw



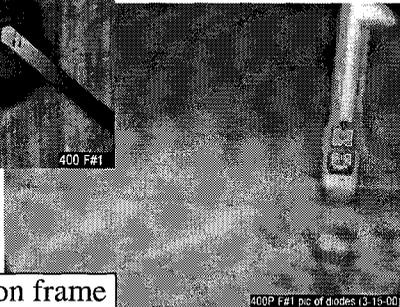


Substrateless Technology for 400 GHz MMCs



Doubler mounted in block

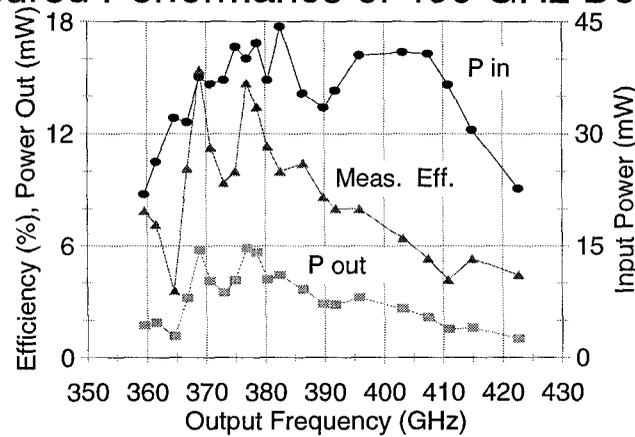
30 μ m



Closeup of diode on frame



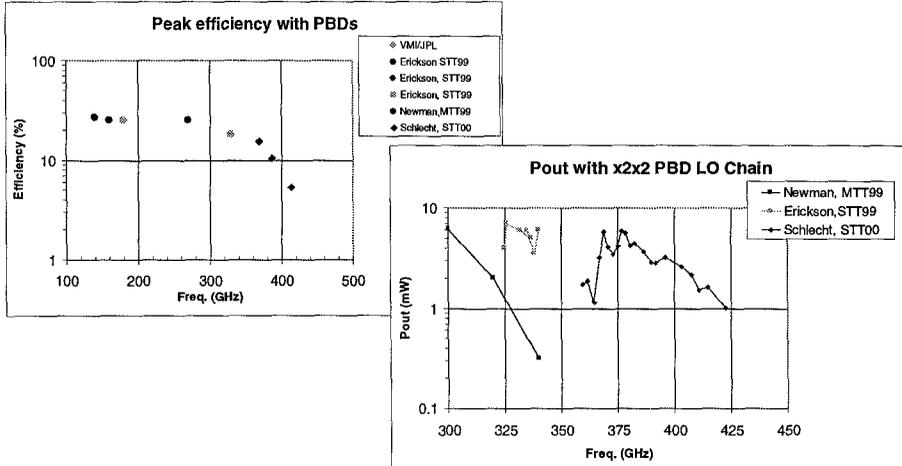
Measured Performance of 400 GHz Doubler



- Calculated performance 35 % efficiency
- Expected performance 25 % including circuit loss



Fix tuned Multiplier State-of-the-art performance, (Apr 2000)



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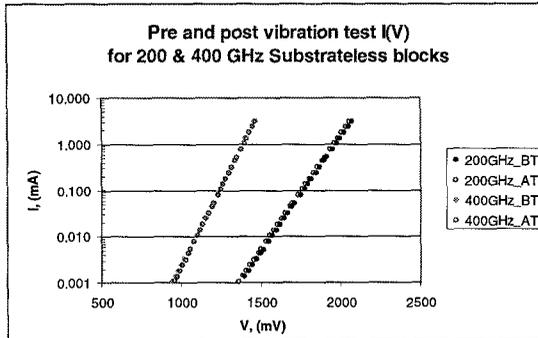


Vibration Test on the Substrateless MMCs

- 200 and 400 GHz blocks, block length parallel to x-axis, 1st order random test

Test I specifications
 20 Hz--0.001 g²/Hz
 20-100 Hz--+6dB/oct
 100-500 Hz--0.1, 0.2,0.4,0.6,0.8,1.0,1.2 g²/Hz
 500-2000 Hz-- -6dB/oct
 Overall: 7.9,10.9,15,18,21,23,28 GRMS
 Duration: 60 seconds

Test II specifications
 20 Hz--0.001 g²/Hz
 20-100 Hz--+6dB/oct
 100-1000 Hz--0.8 g²/Hz
 1000-2000 Hz-- -6dB/oct
 Overall: 28.7 GRMS
 Duration: 440 seconds



Specification for FIRST: 11.2 GRMS

- no change in I(V)
- no change in RF (only 200 GHz measured)

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Multiplier Requirements for FIRST

- Efficient, accurate assembly of multiplier circuits in blocks — need over 100 for FIRST!
- Ruggedness, resistance to shock and vibration for space qualification
- Wide bandwidth (10 to 14 %)
- High power capability (200 – 250 mW)
- High efficiency for multiple cascaded stages
- Cryogenic (100 K) operation



Technology:
Frameless GaAs Membrane

Get rid of frame

- Advantages:
 - Increased design flexibility
 - All shapes possible
 - Split waveguide block implementation possible (no frame in the way)
- Drawbacks:
 - Handling (use of “sacrificial frame” possible)

Extensive use of Beam Leads

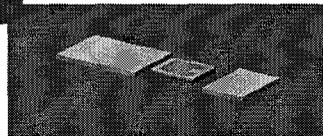
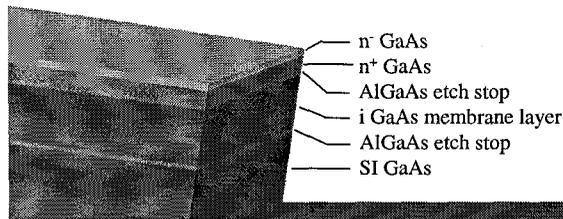
- Advantages:
 - Simplified assembly (no soldering, chip “dropped in”)
 - Simplified bias scheme (no wire bonding)
 - Low loss, high bandwidth antennas/circuits (air dielectric)
- Drawbacks:
 - Fragile during handling



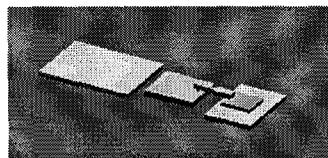
Advanced Local Oscillator Development for Millimeter and Submillimeter-wave Applications



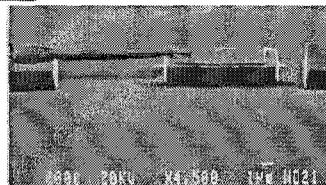
Technology:
Frameless GaAs Membrane flowchart



- recessed Ohmic
- Mesa definition
- Interconnect metal



•E-beam anode



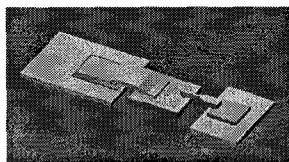
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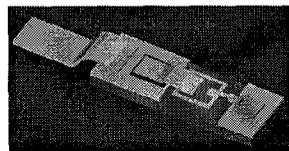
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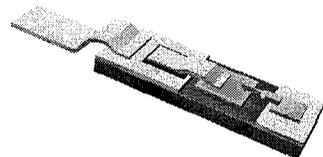
Technology:
Frameless GaAs Membrane flowchart 2



- SiN
- Bridge/capacitor metal



- Membrane definition
- Bridge metal/RF probe/beam leads



•substrate removed

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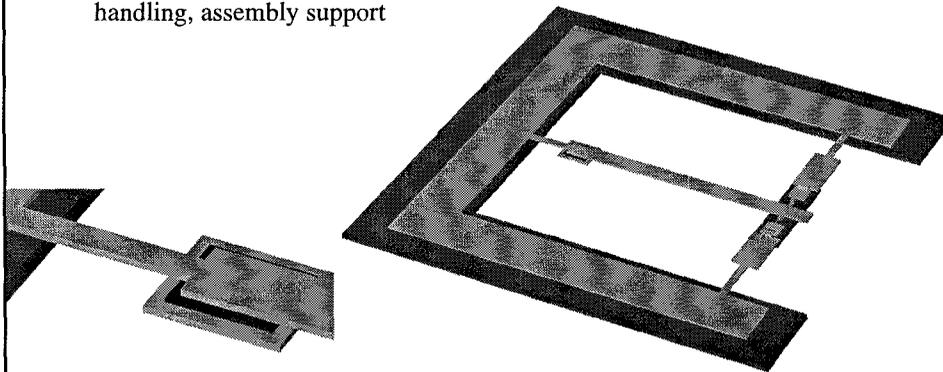
Advanced Local Oscillator Development for Millimeter and Submillimeter-wave Applications



Technology:

Possible Features:

- Sacrificial handling membrane frame
- Substrateless thin film capacitor (for DC bias isolation)
- Multi purpose beam-leads: RF probes, RF ground/short, DC bias, handling, assembly support



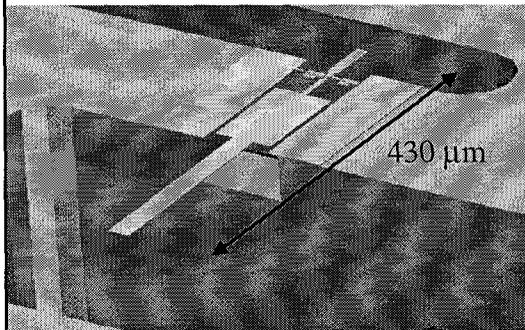
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Advanced Local Oscillator Development for Millimeter and Submillimeter-wave Applications

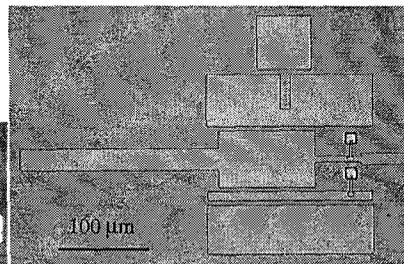
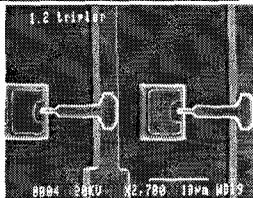


Application: Tripler to 1.2 THz on membrane



- Balanced tripler for idler tuning.
- Split waveguide block.
- Simple bias scheme.
- Predicted efficiency is 2%.

Planar Diode properties:
 Epitaxial doping concentration: $5 \times 10^{17} \text{ cm}^{-3}$
 Anode size: $0.4 \times 0.6 \text{ μm}$



Pictures of the tripler under fabrication, after anode metalization

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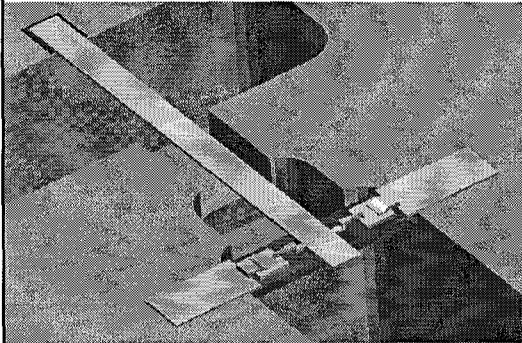
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Advanced Local Oscillator Development for Millimeter and Submillimeter-wave Applications



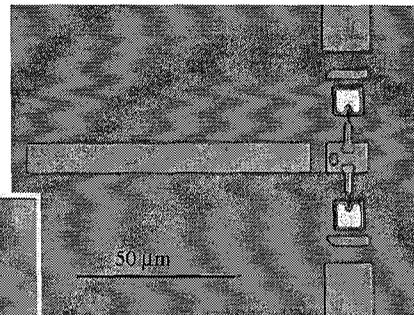
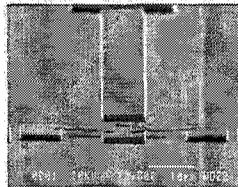
Application: Doubler to 2.4 THz on membrane



- Balanced doubler for simplified circuit (no filters).
- Split waveguide block.
- Low Power.
- Predicted efficiency is 2.5 %.

Planar Diode properties:

Epitaxial doping concentration: $5 \times 10^{17} \text{ cm}^{-3}$
Anode dimensions: $0.14 \times 0.6 \text{ } \mu\text{m}$



Pictures of the doubler under fabrication, after anode metalization

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Advanced Local Oscillator Development for Millimeter and Submillimeter-wave Applications



Conclusion

- High power amplifier technology has been demonstrated at 100 GHz enabling 250 mW in w-band
- Balanced doublers work with about 20% efficiency to 200 GHz, enabling 50 mW
- Balanced planar doublers to 400 GHz have demonstrated 15% efficiency, enabling 8 mW
- Devices are currently under fabrication that will extend the range of this chain to 1.2 and 2.4 THz
- Cooling is expected to improve the output power and efficiency of each stage (more drastically in the lower stages)

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