



Integrated Magnetic Components for Distributed Power Electronics

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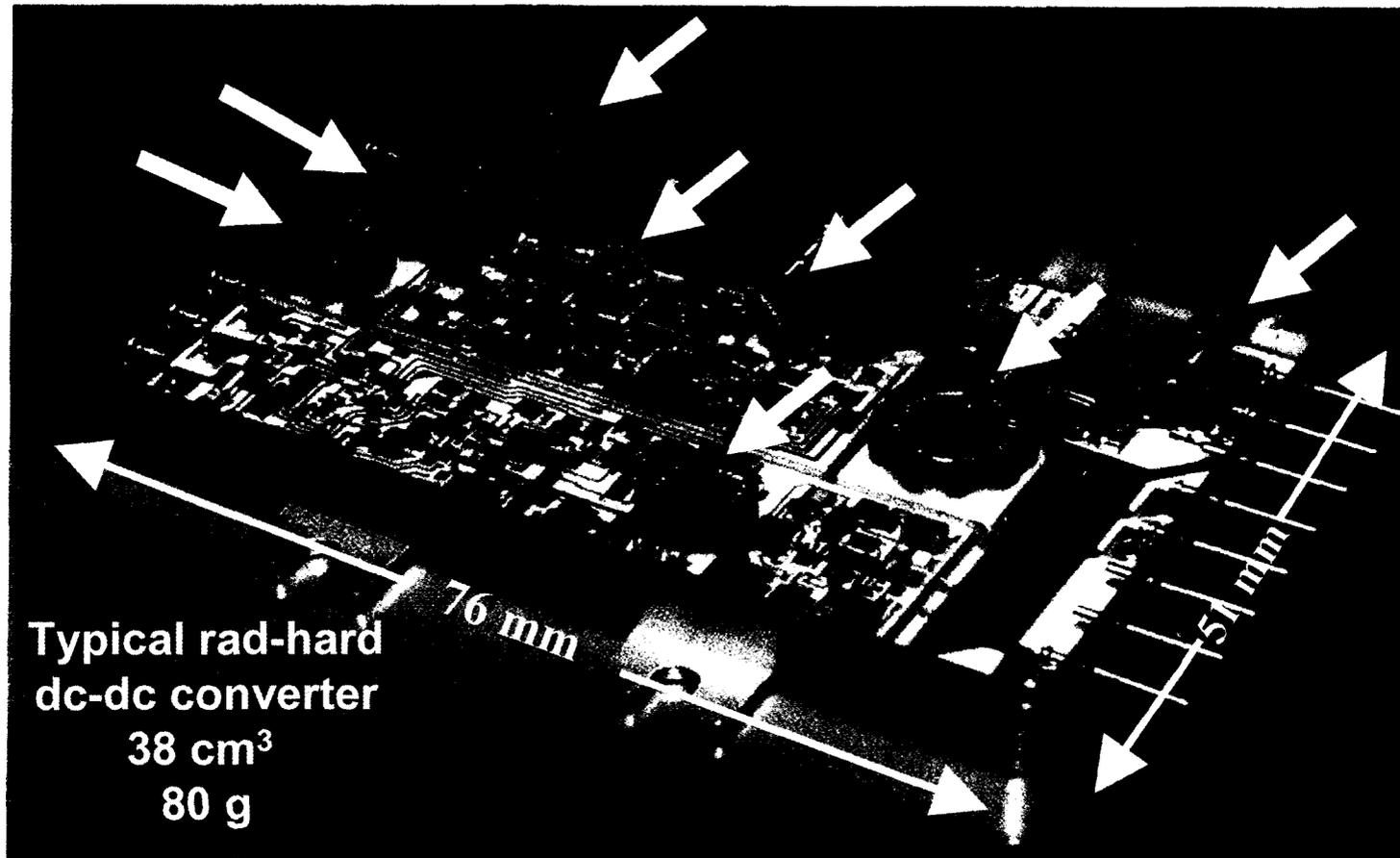
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Integral Wave Technologies



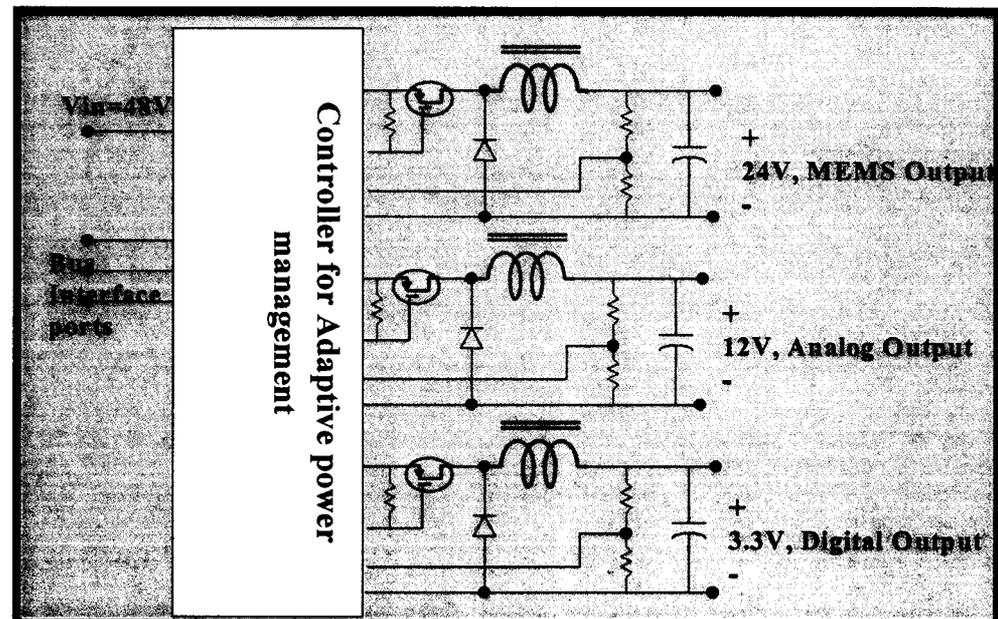
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- magnetic components required for energy storage, filtering and isolation
- still difficult to miniaturize and integrate power magnetics
- power electronics remain a mass/volume burden for spacecraft avionics

JPL/NASA Philosophy--*Need design flexibility*

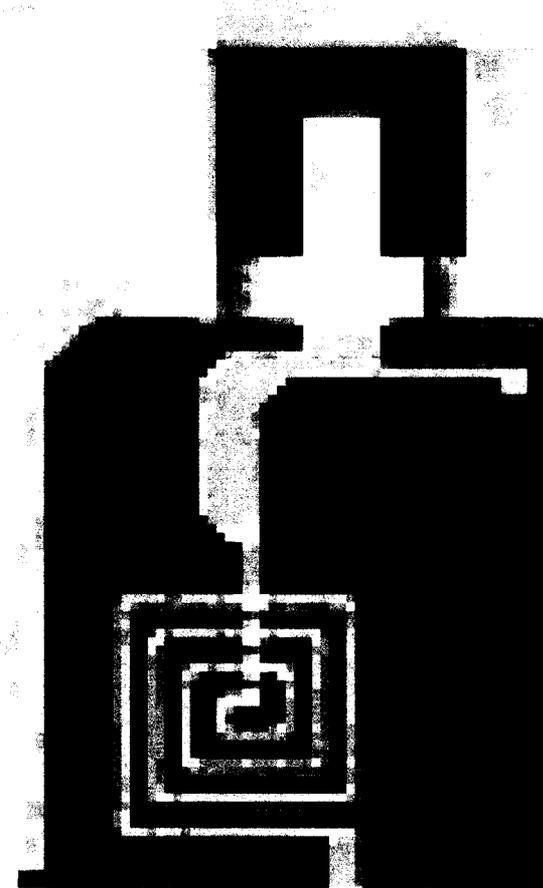
- would rather develop one small (e.g., 10 W) converter
- parallel smaller converters for 20, 30, 100 W (using modular *slices*)
- avoid designing a 100 W converter that is never used again
- looking for methods of high density packaging to cut down on passives
- combine passives/switching/control
- move to distributed power
- no longer wind our own magnetics
- batch fabrication would be great
- are *integrated* magnetics the answer?



**Discrete, surface mount inductors**

Heavy gauge copper wire wound around
a ferrite based core

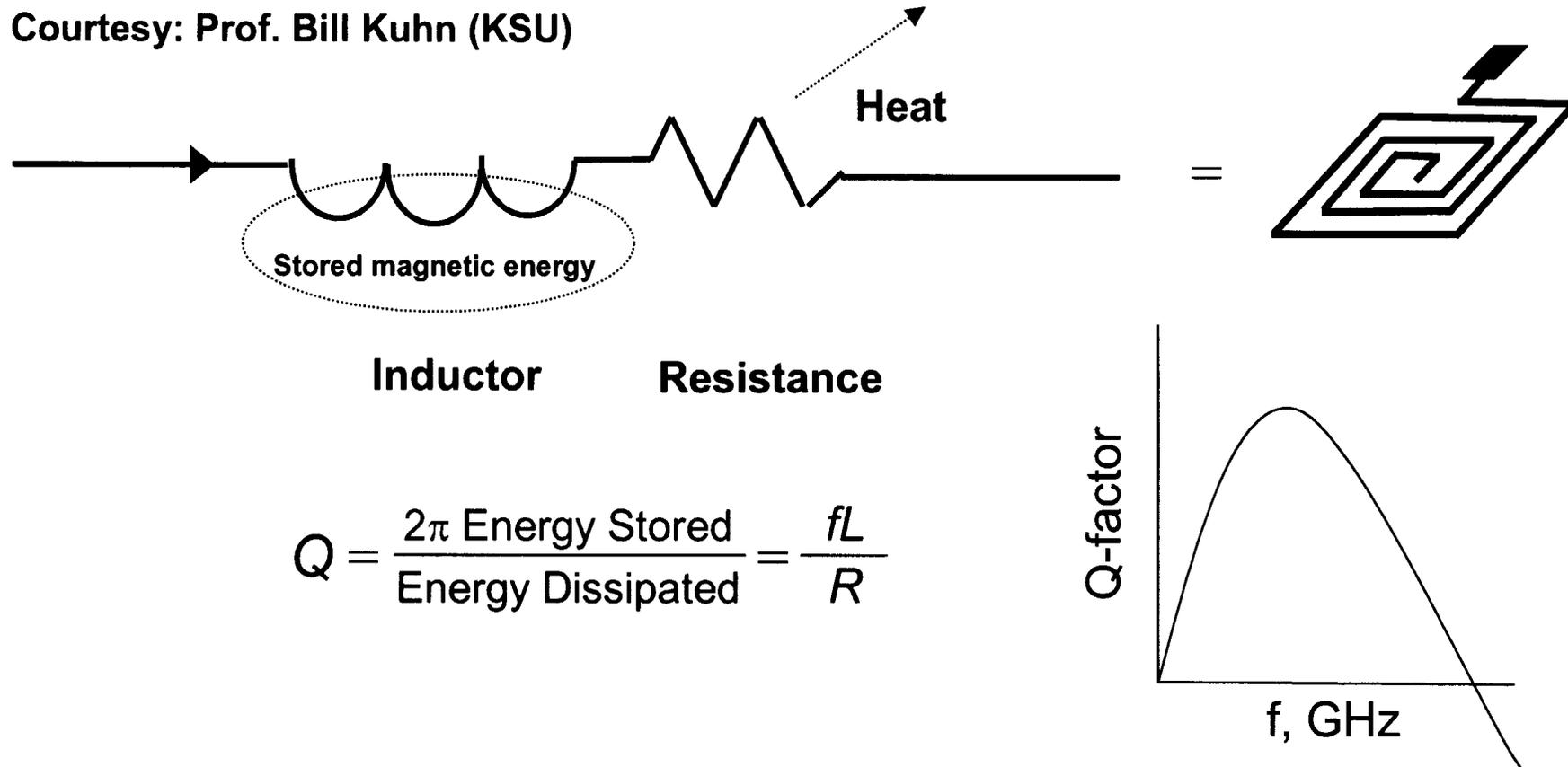
**High inductance *but*
high mass and volume**

**Integrated inductors**

Spiral metal trace on silicon

**Low mass and volume *but*
low inductance**

Courtesy: Prof. Bill Kuhn (KSU)



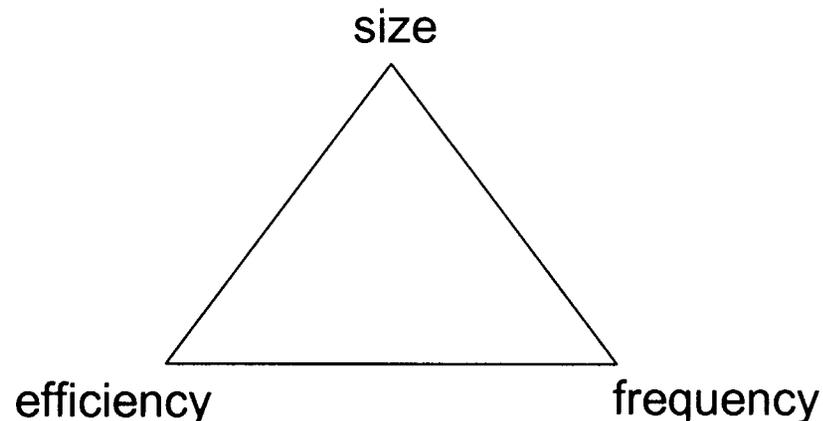
- Increasing N means increasing R , thereby decreasing Q and SRF
- Could operate at a higher (>500 MHz) frequency, but not optimal for power
- Enhance L by adding magnetic materials; keep R low by using thick Cu lines
- Important to have Q peak in key power region of 1-10 MHz

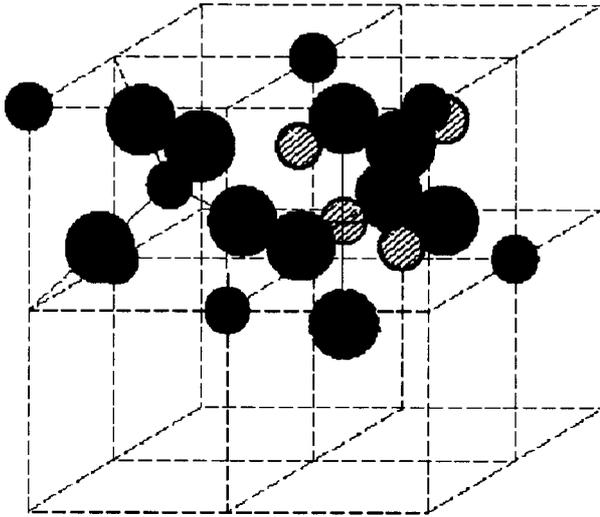
- Small volume of core
 - t= film thickness, effective cross section area of core limited
 - $\mu \bullet t$ is critical parameter (permeance)
- Frequency response
 - reduce losses at 1-10 MHz (smaller size, but less efficient)
 - need new “power materials” that can be readily integrated
 - don't have access to hundreds of core materials and shapes
- Packaging/Integration
 - minimize footprint
 - thermal management (can be benefit)
 - performance (parasitics, sensitivity to environment)
- Need the proper combination of:
 - inductance
 - resistance
 - area
 - Q (1-10 MHz)
 - current handling

- Earliest investigations in the 1970's (sputtered/evaporated alloys as the “core”)
- Honeywell investigated electroplated inductors in the early 1980's
- Lucent and others investigated in the 1990's
- More recently various academic groups (Japan, Europe, U.S.)
- Still no real application of a microinductor for power



- Inductance (favored by more turns, which increases R)
- Resistance (favored by less turns, which decreases L)
- Size (very restricted)
- Low loss and high Q (difficult between 1-10 MHz)
- Frequency of operation (sufficient Q difficult)
- Current handling and power (less volume, easy saturation)
- Ease of fabrication (annealing? magnetic fields? materials costs? laminations?)





Spinel Ferrite structure

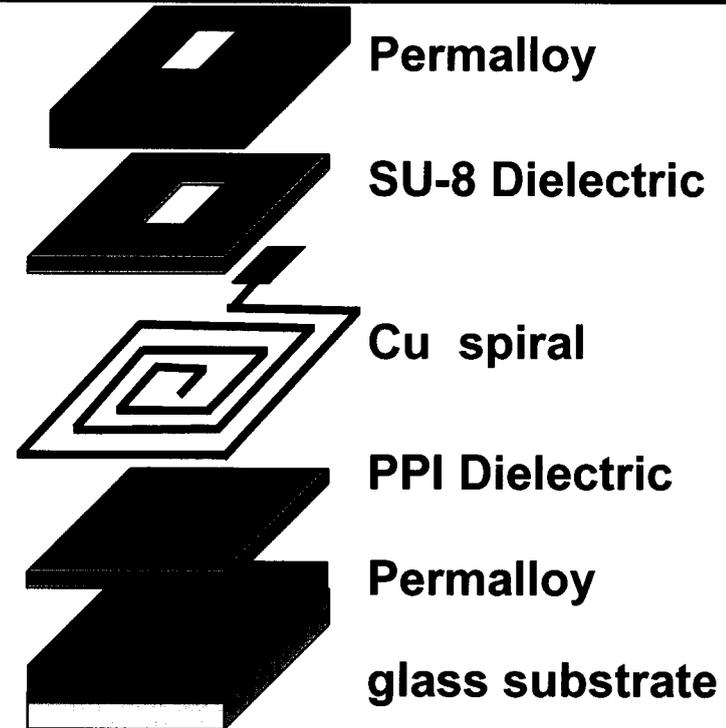
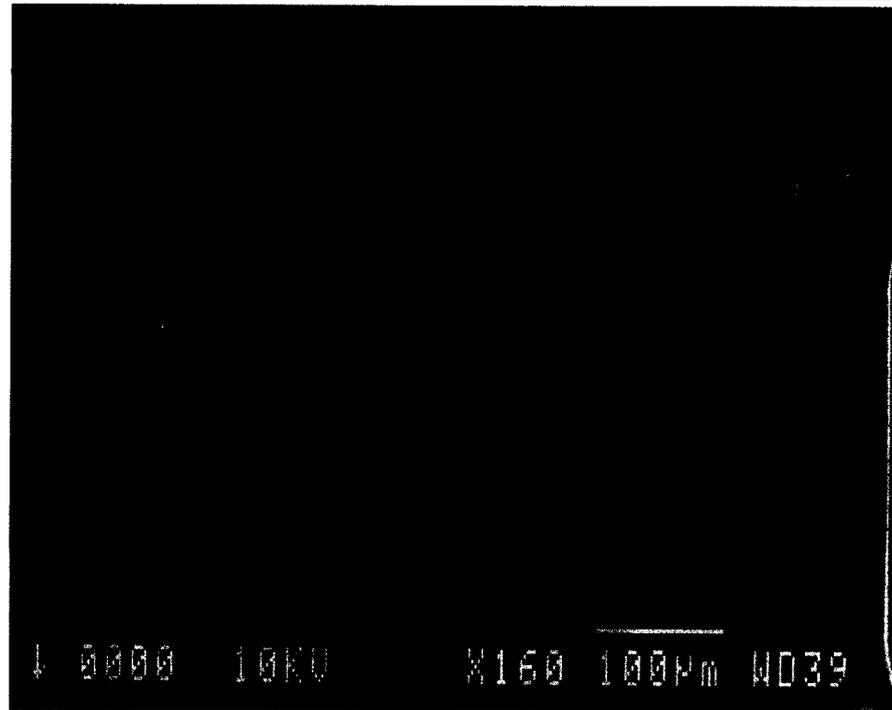
Ferrites

- classic high frequency material
- low saturation magnetization
- difficult to deposit, require high temp. processing

Ferromagnetic metals

- well suited for thin film deposition
- high permeability leads to enhanced inductance
- low resistivity limits high frequency application

Material	B_{max} , G	μ	H_c , Oe	ρ , $\mu\Omega\text{-cm}$	Deposition Methods
Ferrites	5,000	1000	1	10^7	sputtering, stencil printing
Ferromagnetic metals	24,000	3500	<0.05	10^2	sputtering, electroplating



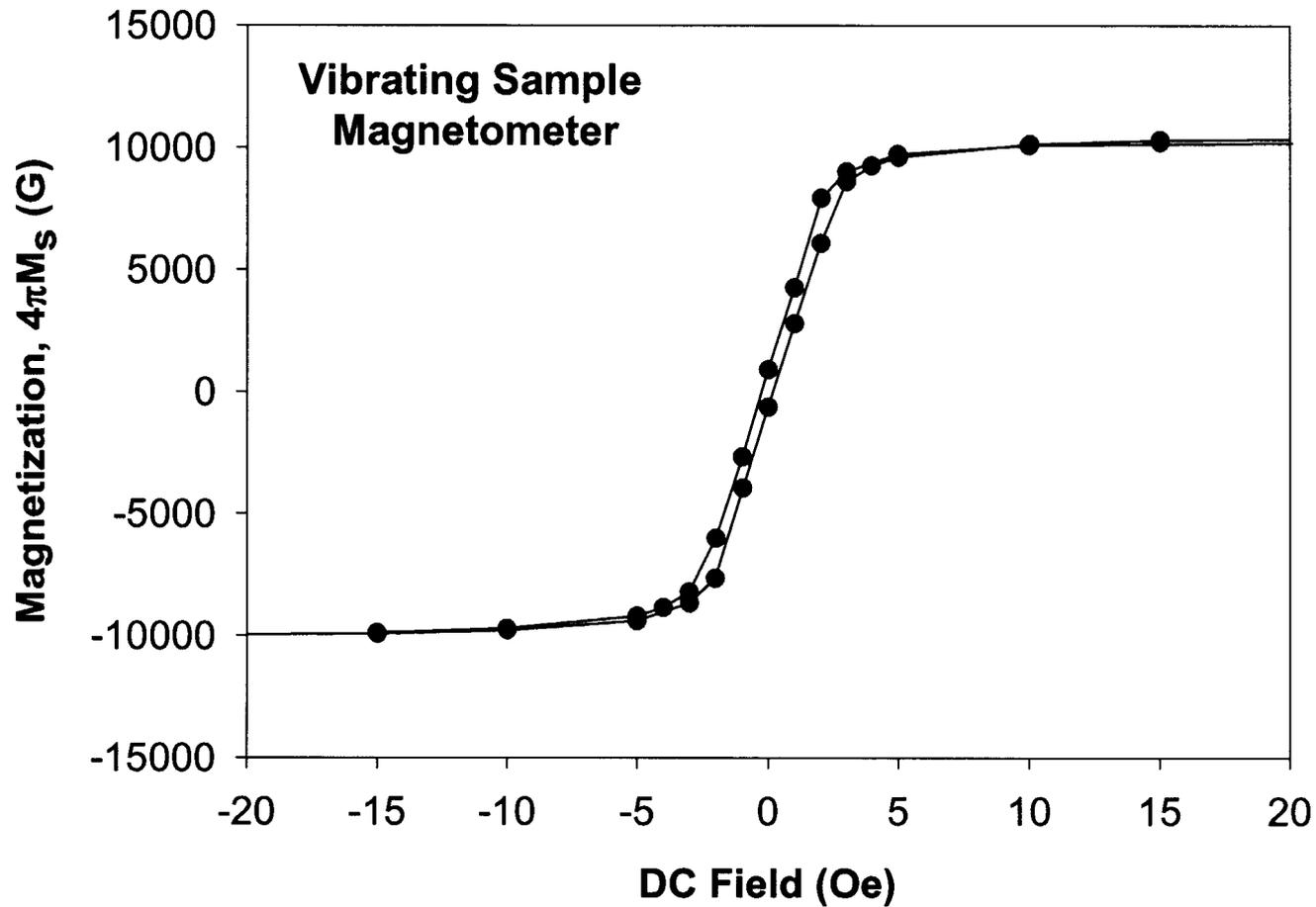
Permalloy: electroplated, using SJR 5740 photoresist

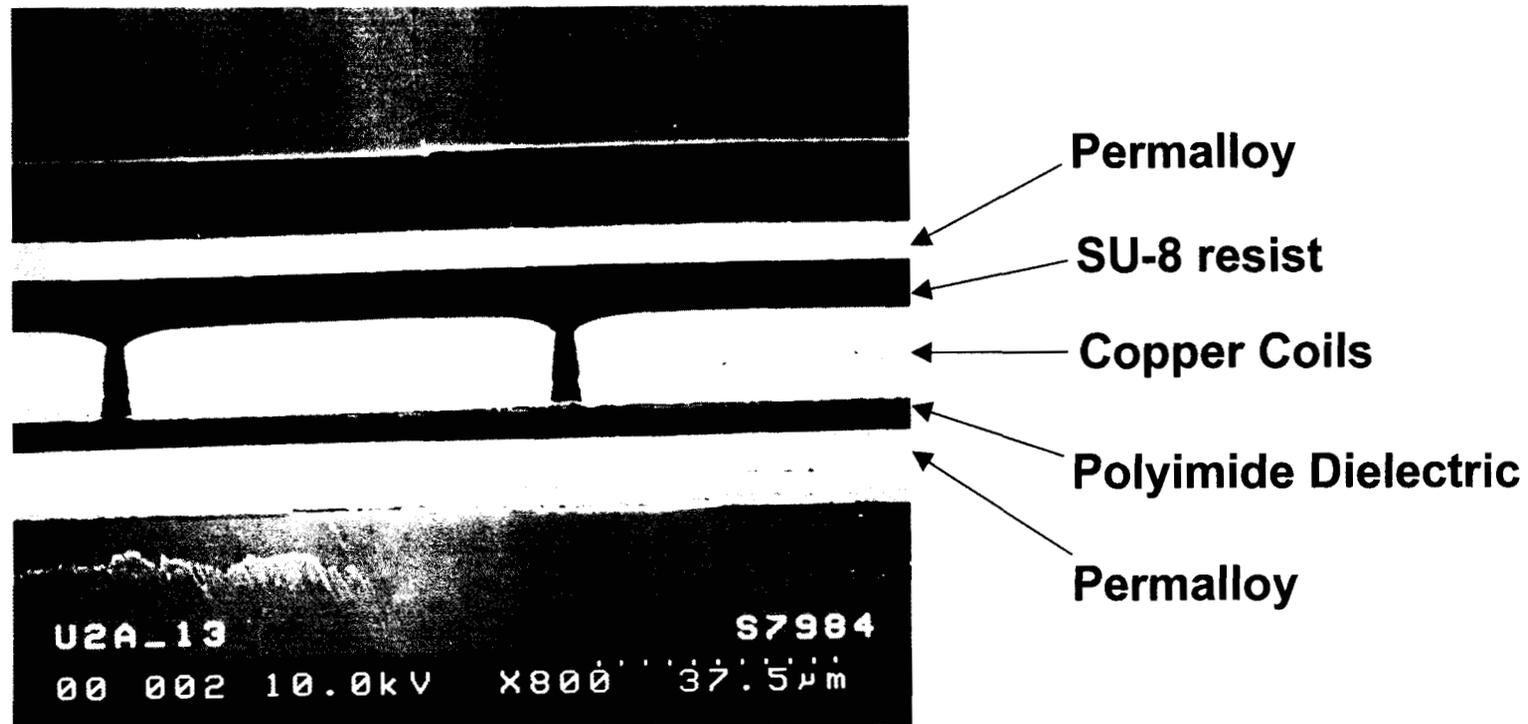
SU-8: applied with multiple spin coats

Copper: plated, using SJR 5740 photoresist

Polyimide: photo-imaged, PPI

Electroplated NiFe using standard Permalloy Bath
composition $\approx 80\%$ Ni 20% Fe



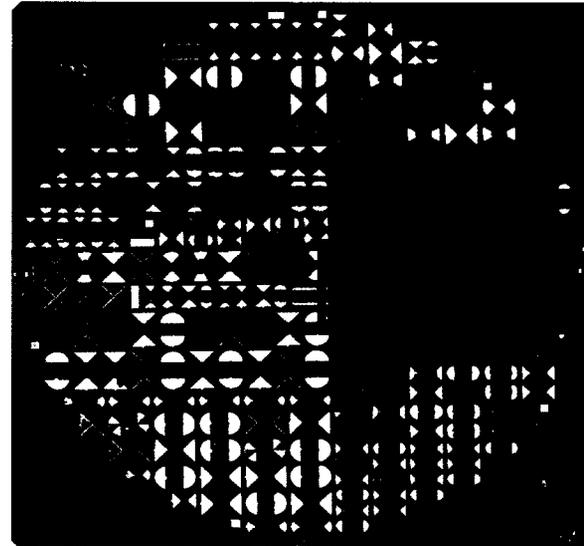


-resembles "pot core" geometry in which windings are buried in magnetics

-should be better for shielding of EMI



Silicon wafer with 284 microinductors



Close-up of microinductors



Top view of microinductor

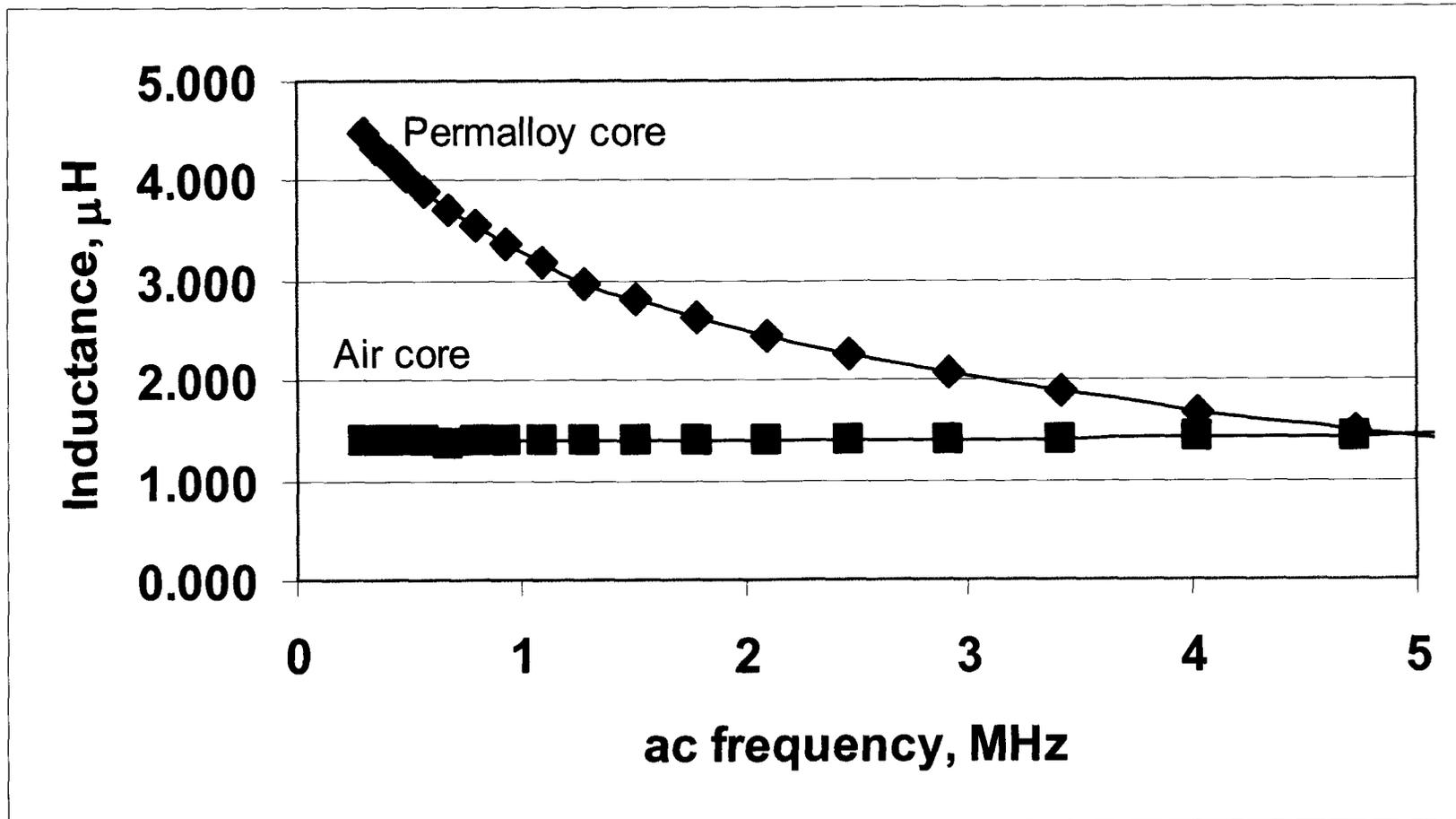
Example test structure on glass:**N = 30 turns****Area = 13 mm² (round)****Line width = 58 μm line widths****Line spacings = 6 μm****Copper thickness = 11.4 μm****Lower Permalloy thickness = 2.3 μm****Upper Permalloy thickness = 3.5 μm**

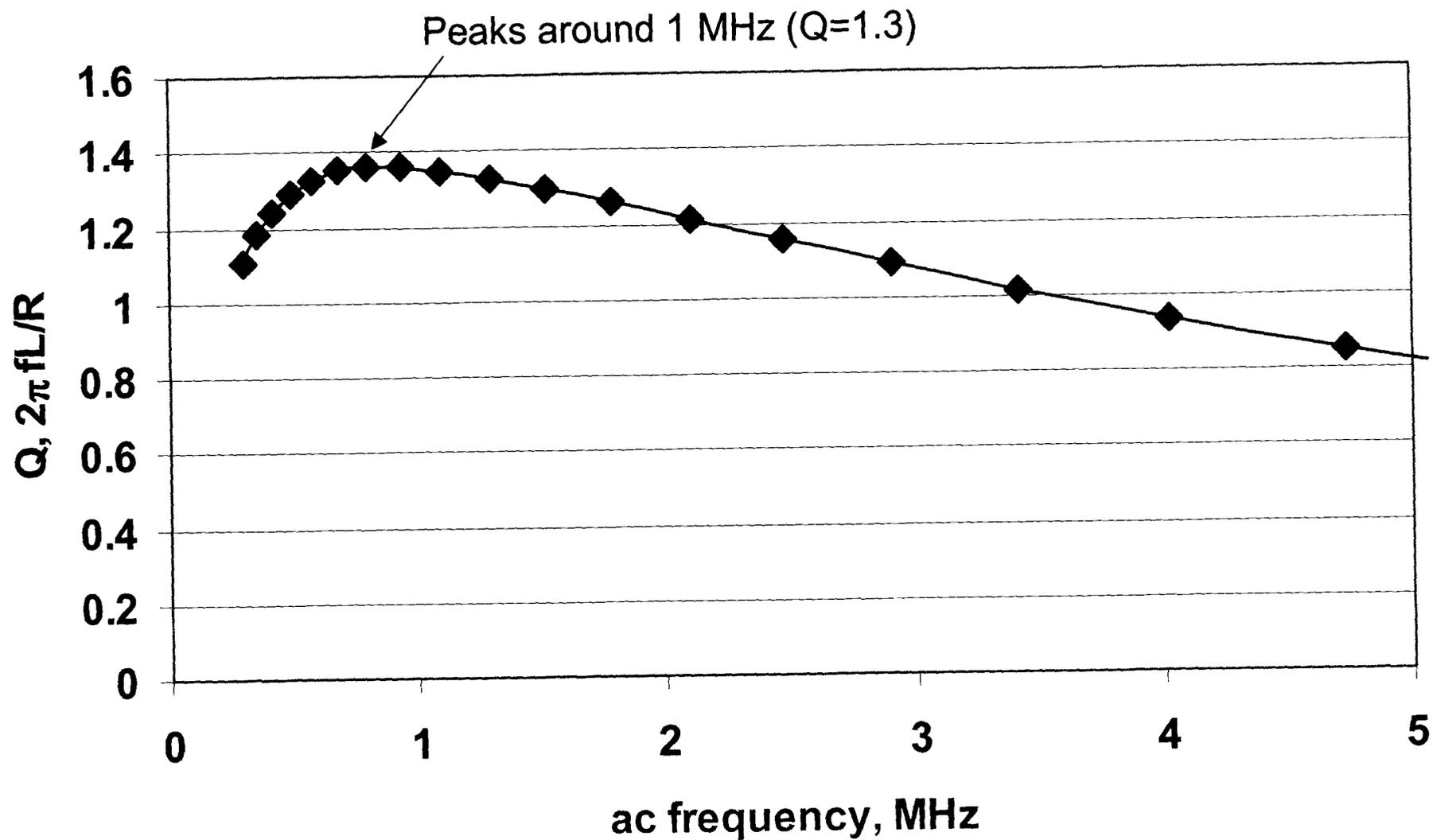
Enhancement over air core values

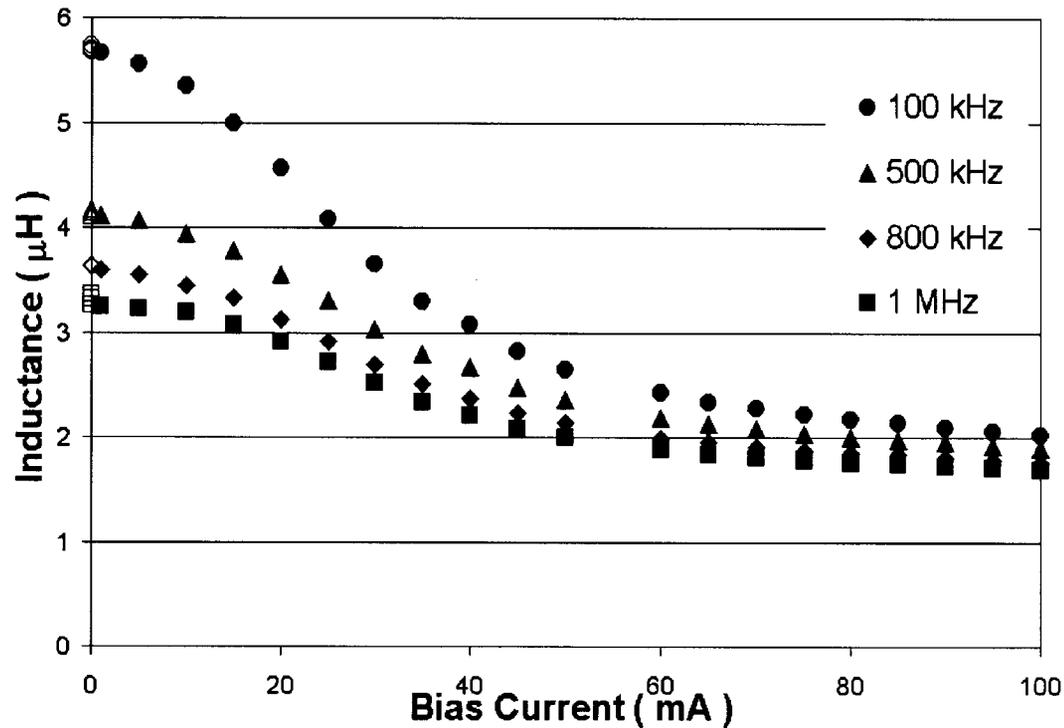


$L = 3.2 \mu\text{H}$ at 1 MHz

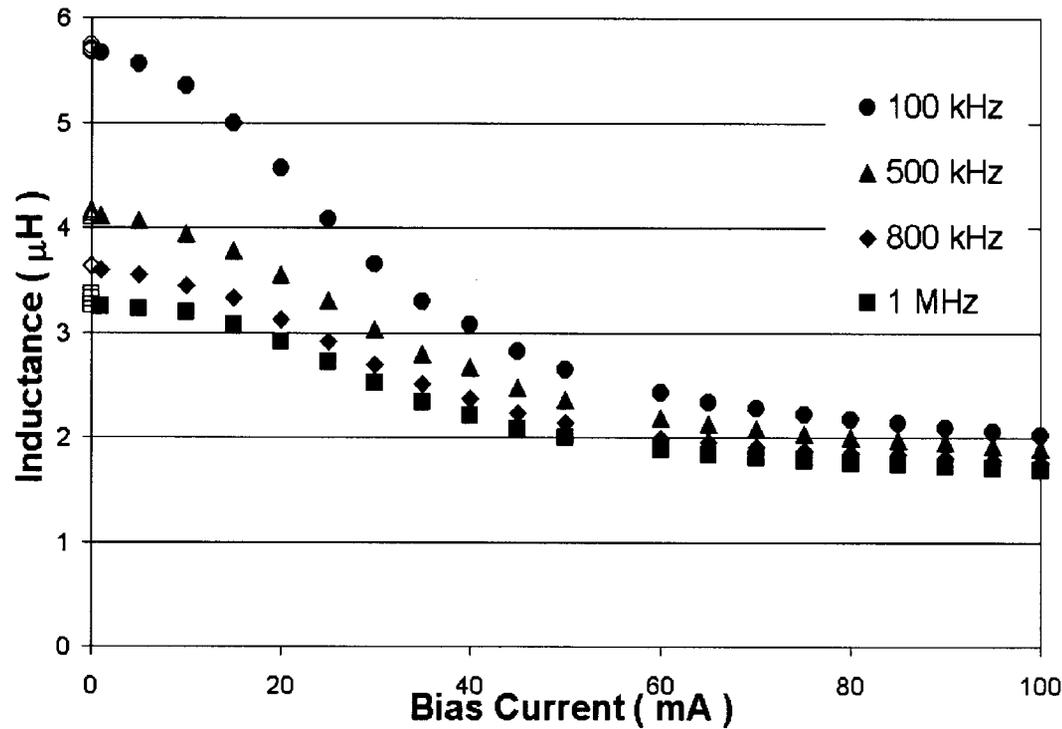
$R = 16.3 \Omega$ at 1 MHz (DCR = 5.1Ω)



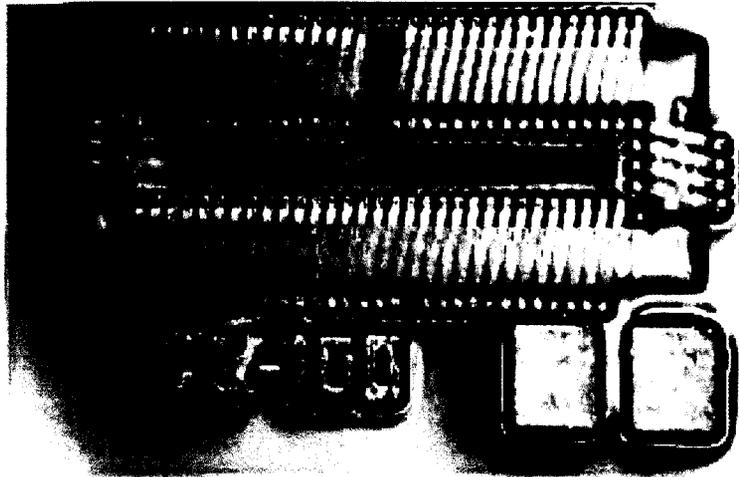
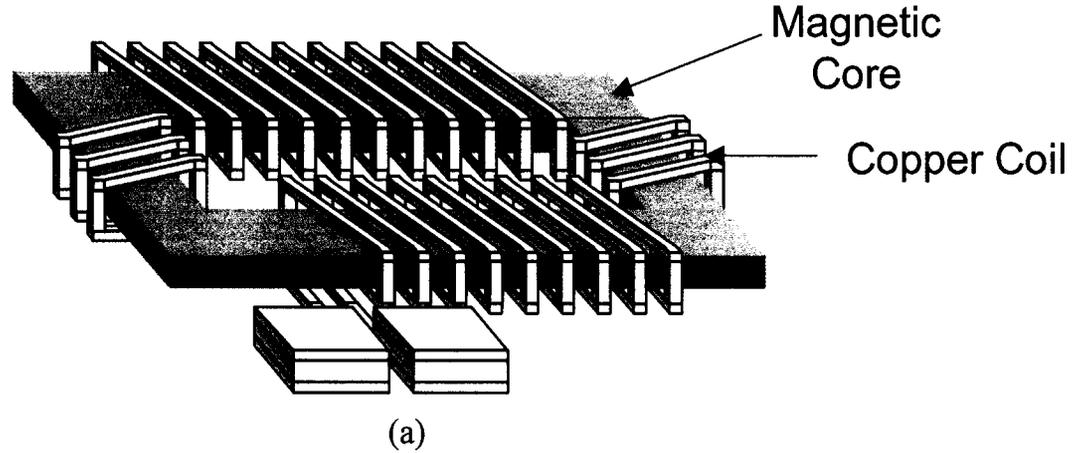




Inductance vs. bias current with 7.5 mA RMS alternating current at 100 kHz, 500 kHz, 800 kHz, and 1 MHz

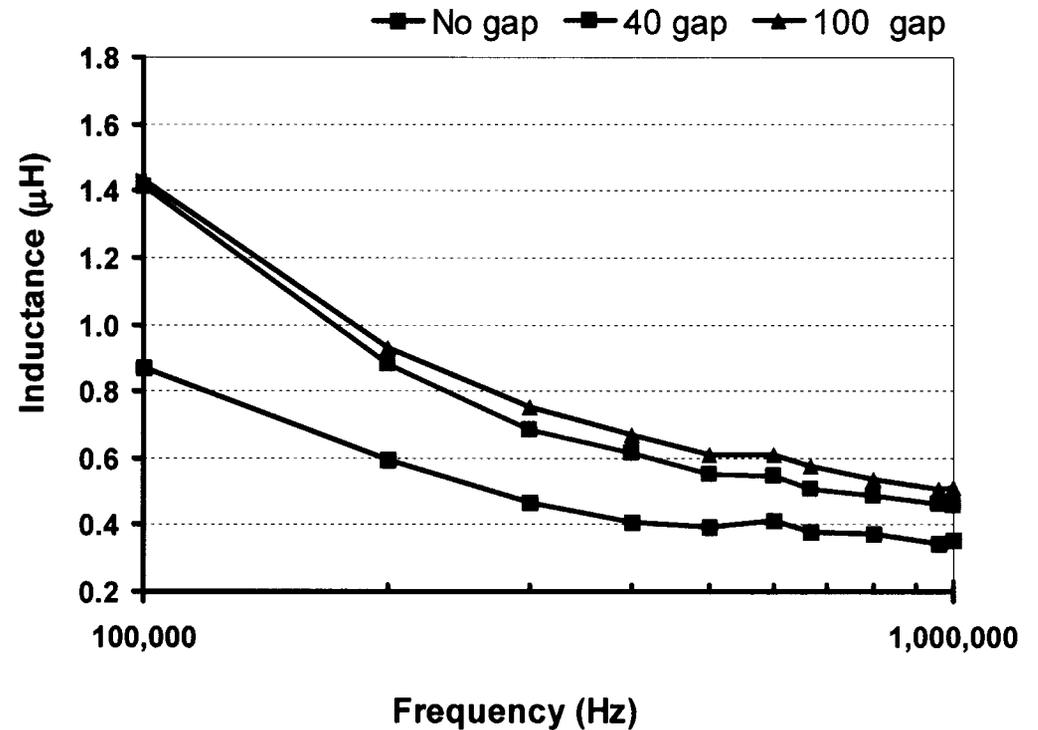


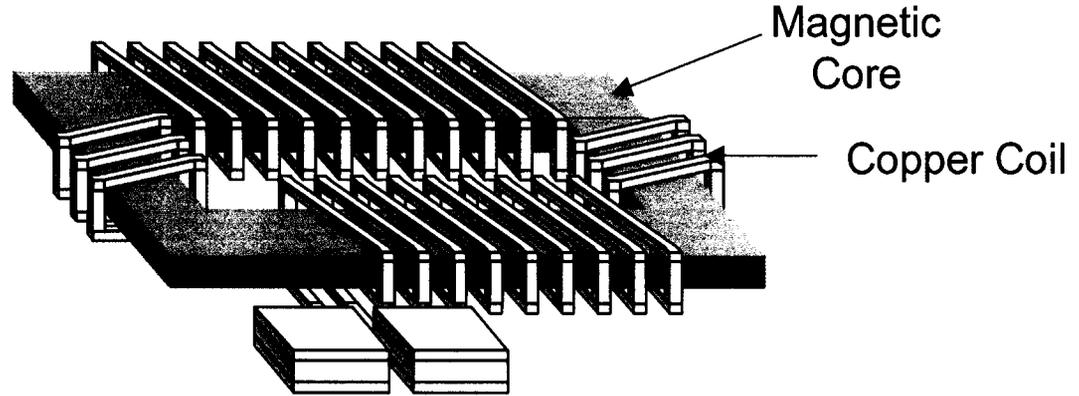
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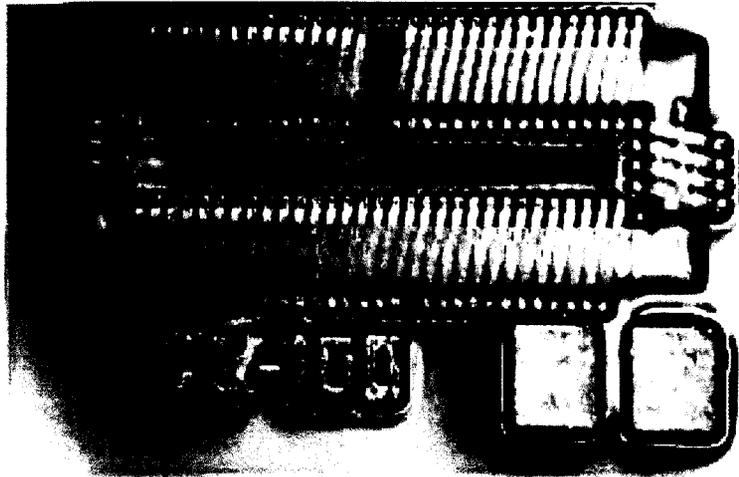
Courtesy: Prof. Chong Ahn (UC)

(From Final Report to JPL)



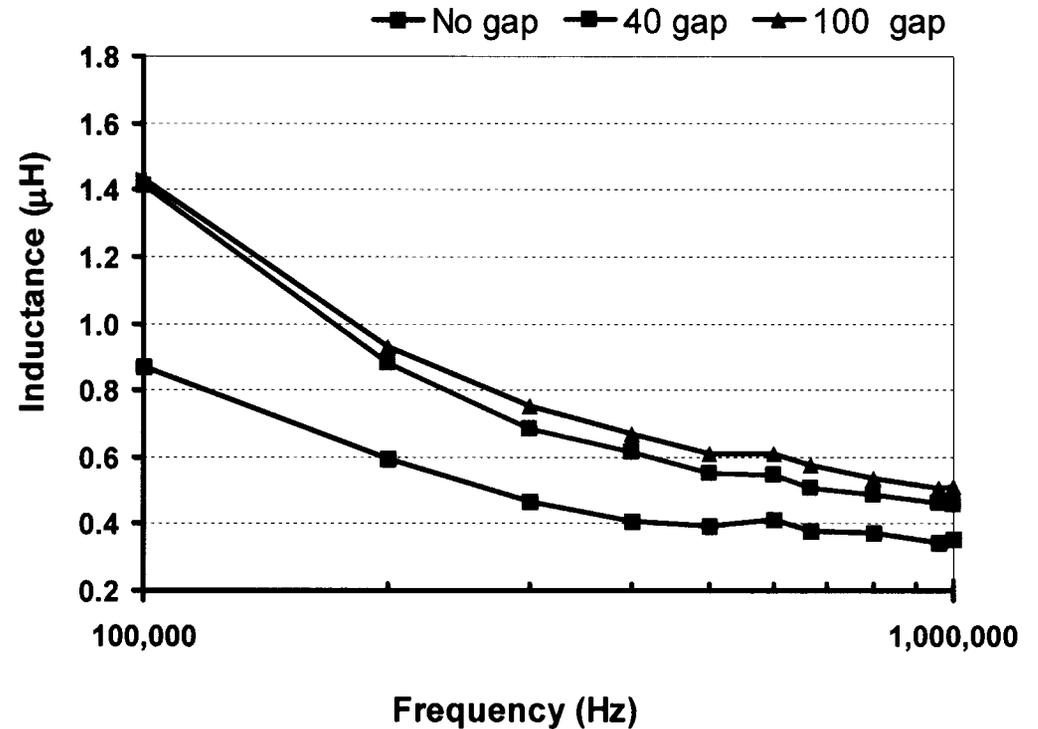


(a)



Courtesy: Prof. Chong Ahn (UC)

(From Final Report to JPL)



Frequency response

- add laminations (costly and more processing)
- new materials (ternary and quaternary alloys, ferrites)
- control anisotropy (how much does this help?)

Current

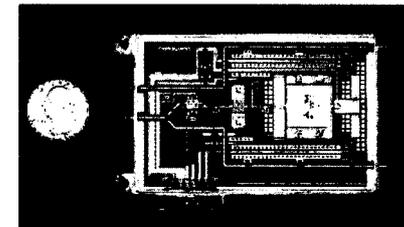
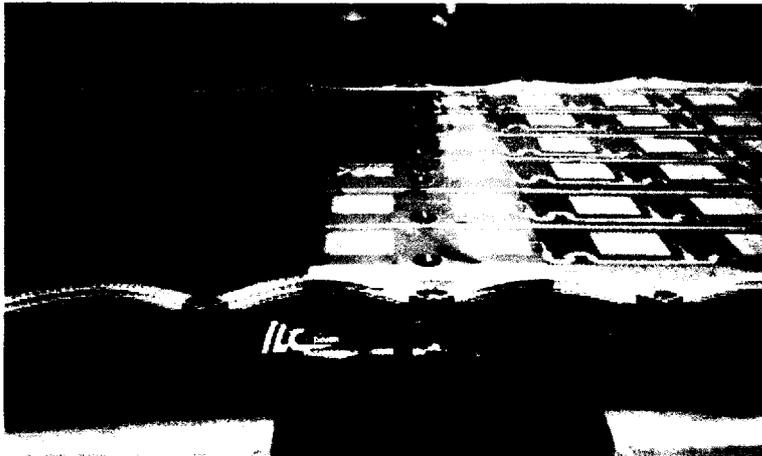
- gaps (difficult to model)
- new materials (Co alloys)

DC resistance

- thicker copper (at the sacrifice of higher ac resistance?)
- larger area (sacrifice miniaturization)

Active membrane synthetic aperture radar (SAR) antennas including flex-compatible T/R modules (for mapping, surface monitoring and change detection of Earth)

Courtesy: Dr. Alina Moussessian (JPL)



T/R module

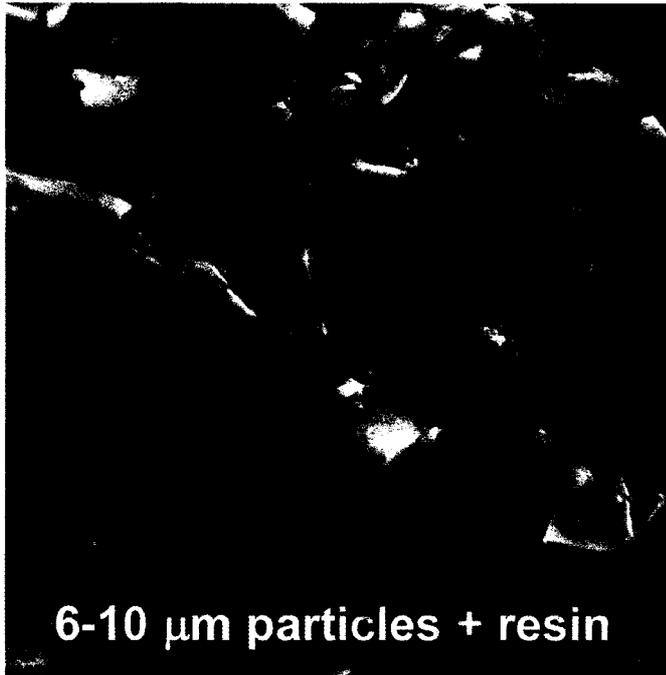


Current passive inflatable membrane antenna

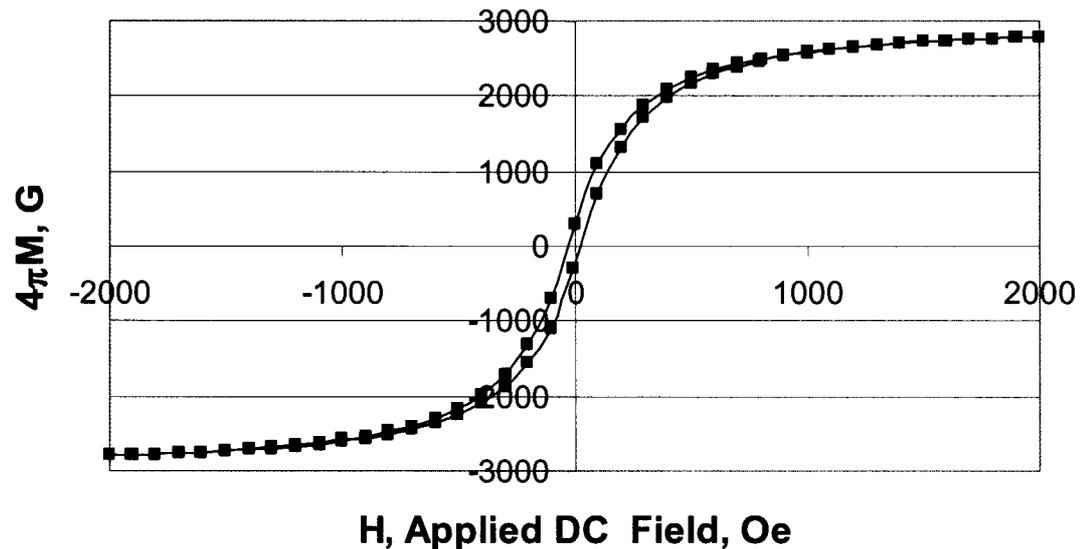


Benefits of an active antenna:



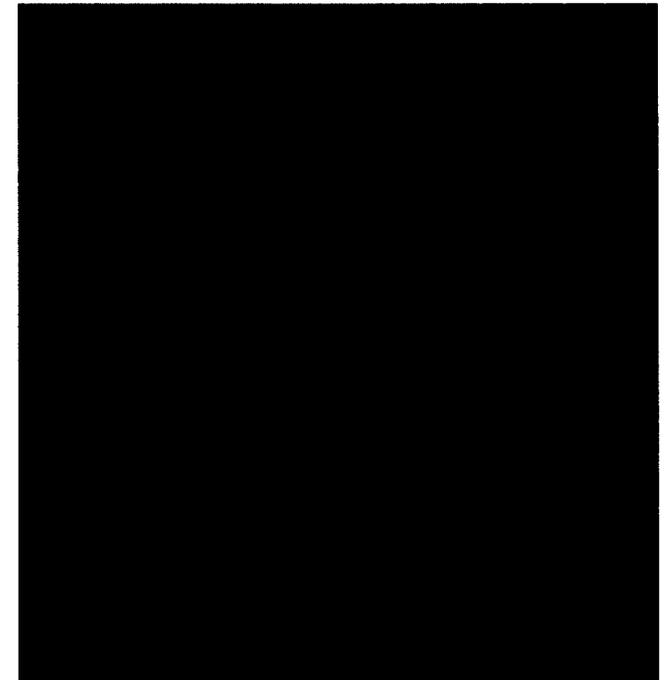
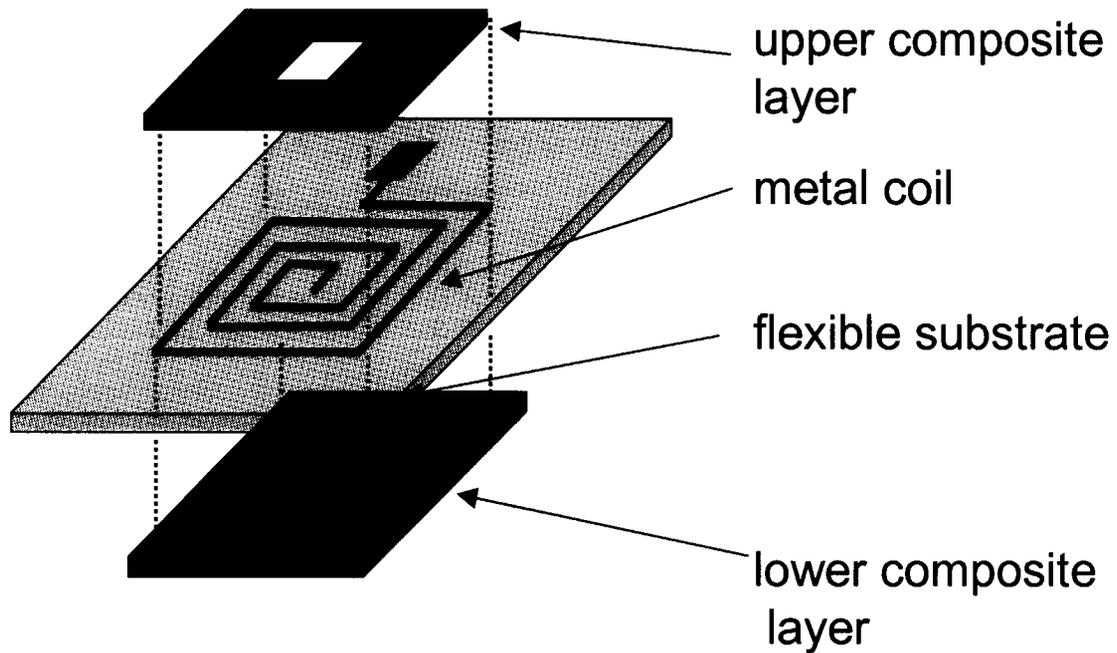


SEM of stencil printed
Ferrite-polymer composite film



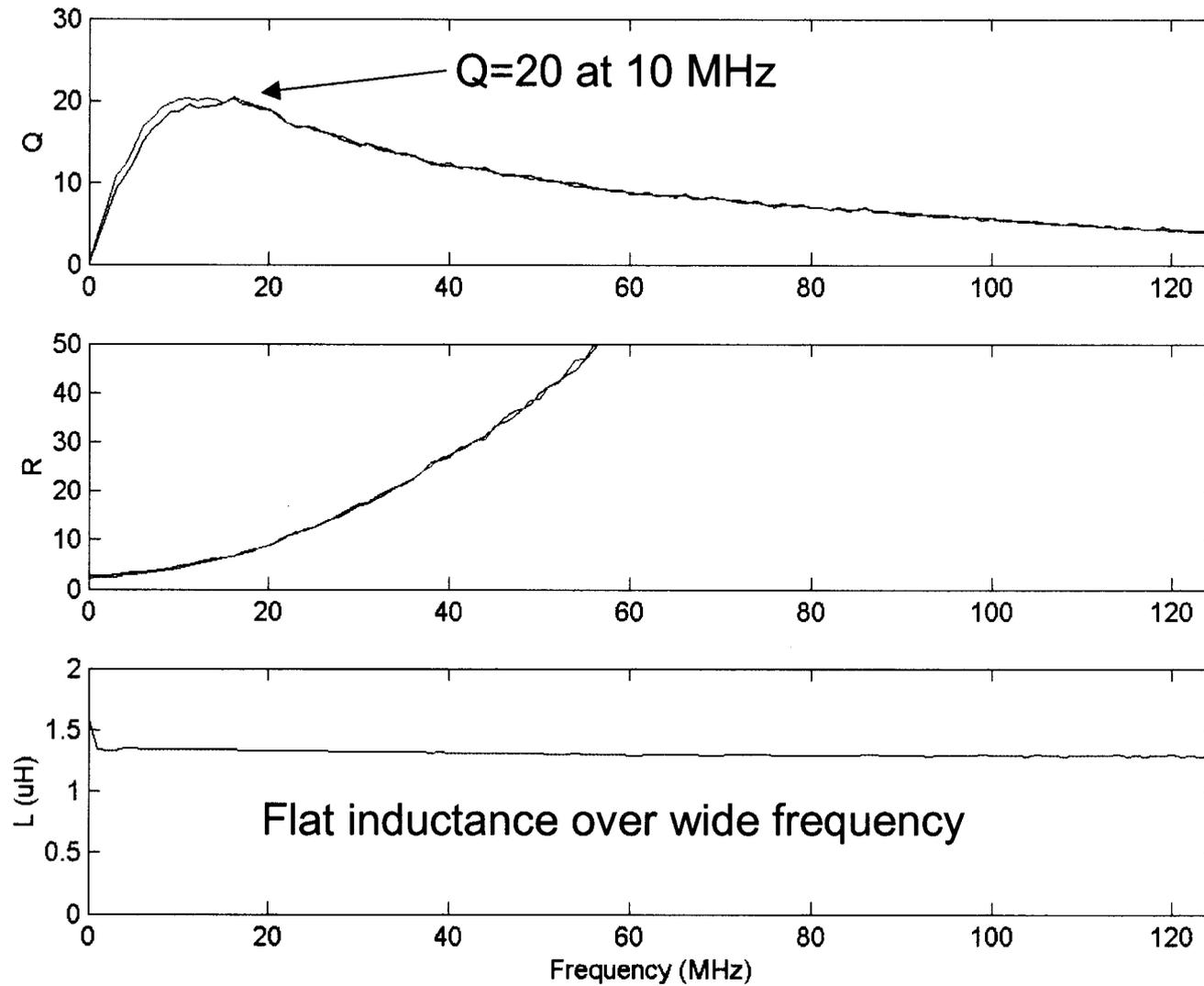
Magnetization curve for printed magnetic film

- Developing novel stencil printed ferrite-polymer composite films
- Stencil and screen printed inks with solvent + resin + ferrite
- Cured at low temperatures-easy integration with heat sensitive substrates
- Enable thicker films to be deposited
- Provide higher frequency operation and higher current handling
- Lower magnetization due to use of ferrites

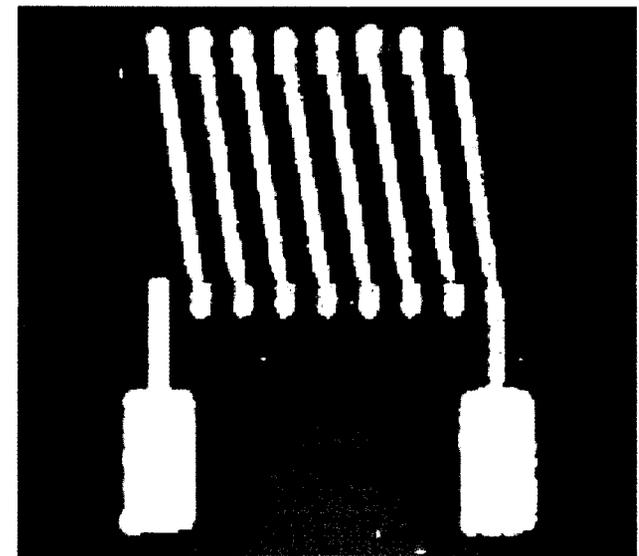
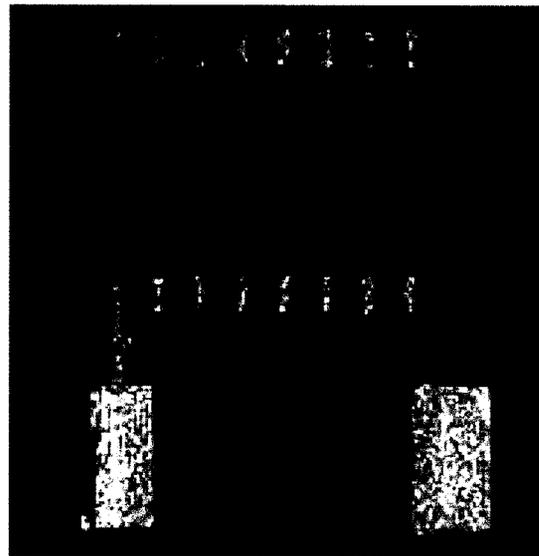
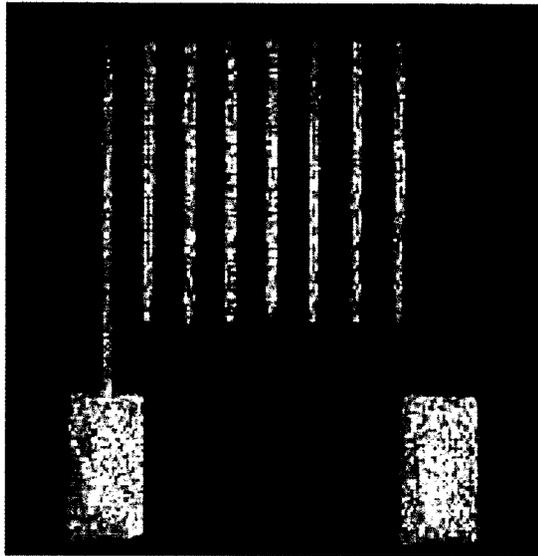


5 mm x 5 mm, 11 turn
coil-on-flex
Mn-Zn composite

Q peaks between 1-10 MHz, flat inductance



Data courtesy of Bill Kuhn (KSU)



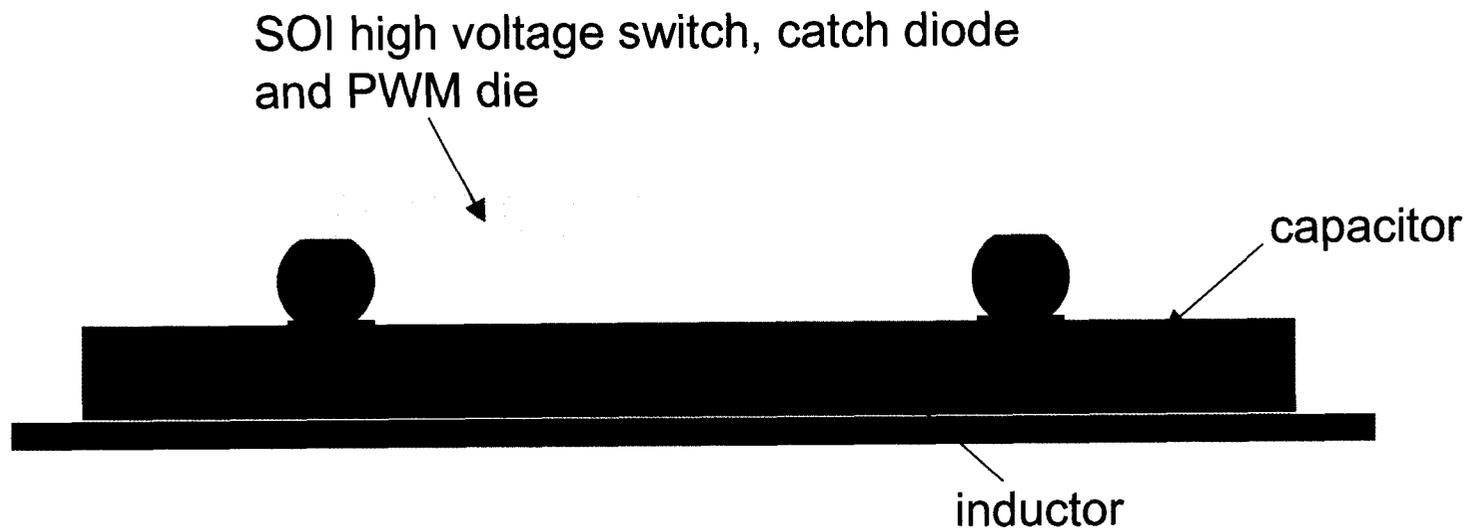
Multilayer, mH inductor coil drawn by printing bottom silver lines, overcoating ferrite layers, and connecting the bottom over the ferrites to complete a spiral coil.

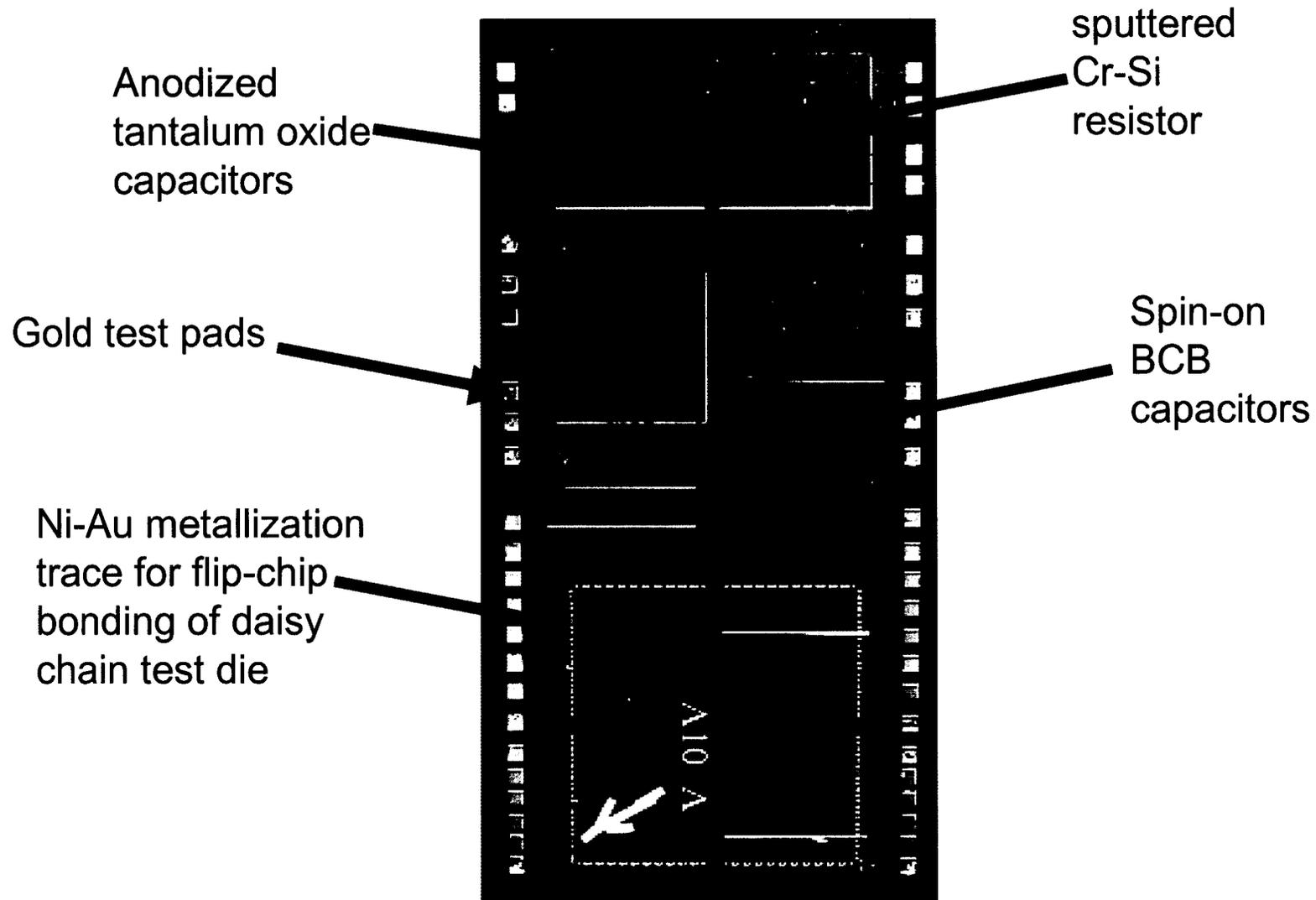
pgclem@sandia.gov

Courtesy: Paul Clem, Sandia National Labs

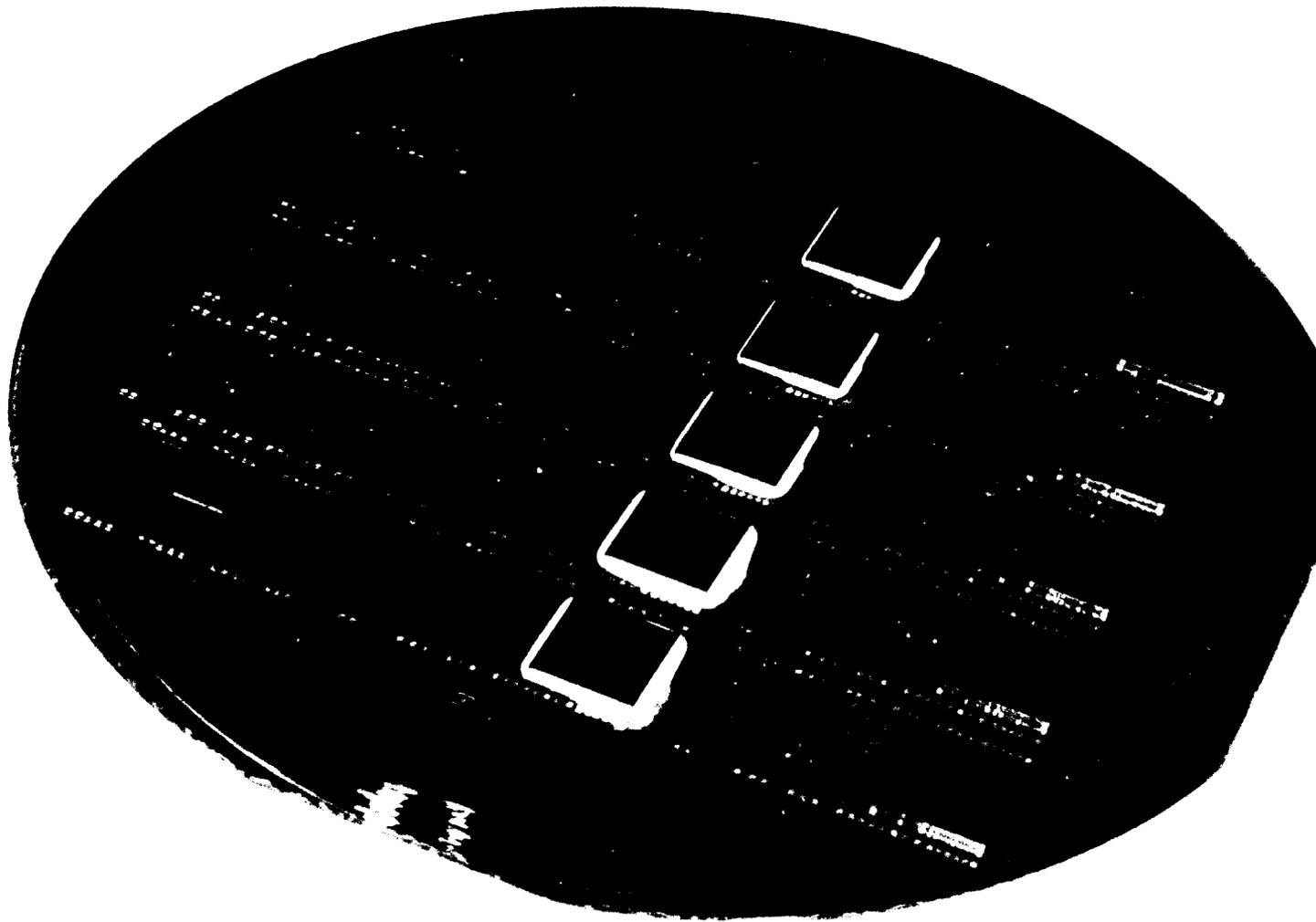
(505) 845-7544,

<http://www.sandia.gov/materials/sciences/factsheets/LoTempWrtElcCom2.html>



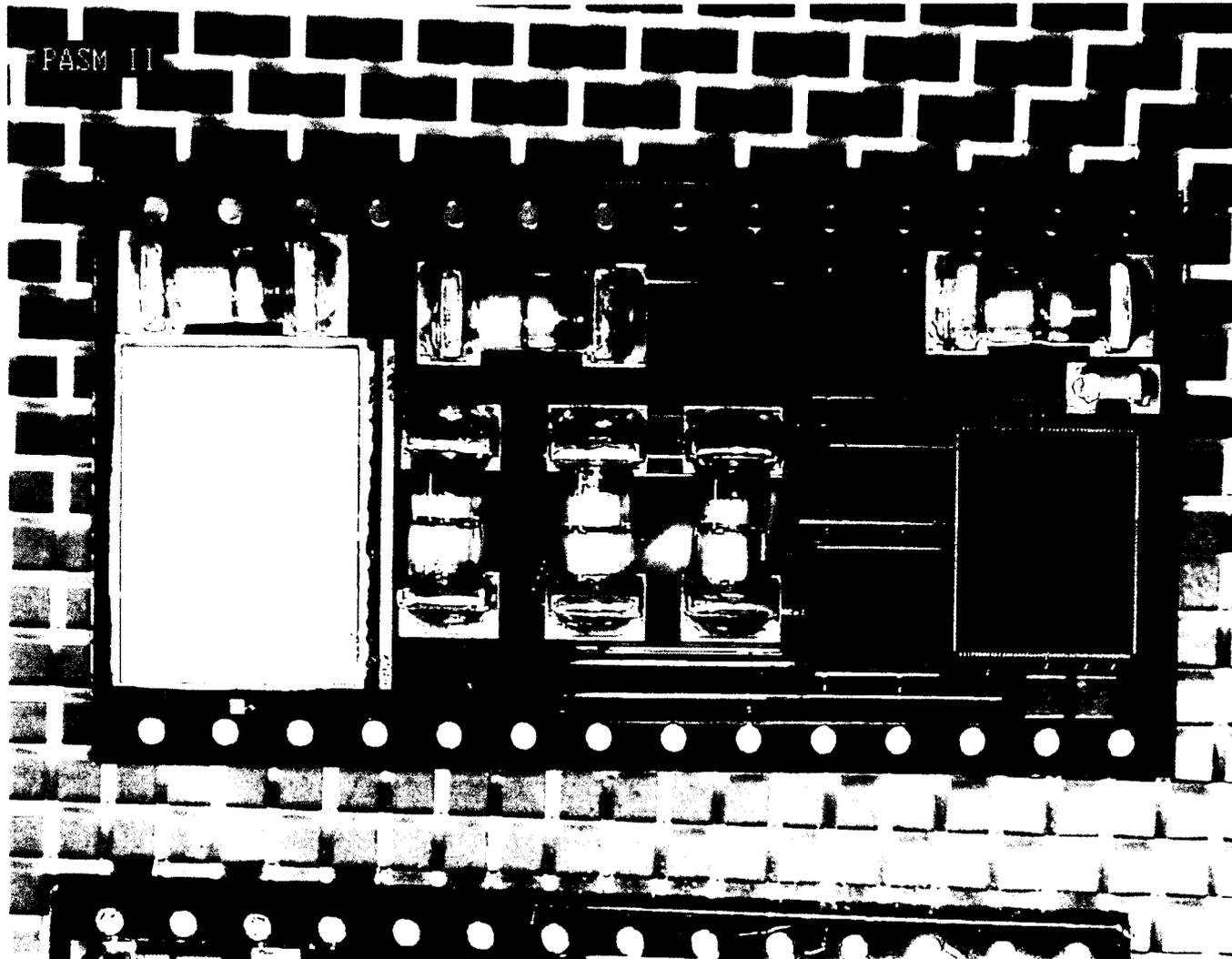


Fabricated by Integral Wave Technologies (Arkansas)



Fabricated by Integral Wave Technologies, Flip Chip at Auburn University

Power switching circuit with integrated passives



Integrated Magnetic Components for Distributed Power Electronics



- Integration of passive components can play a key role in the miniaturization of spacecraft avionics
- Reducing the mass and volume of spacecraft power electronics will require advances in integrated passives, particularly magnetic components
- Significant challenges remain, including choosing proper materials, as well as addressing design, layout and test and re-work issues

