



***Electron-Beam Fabrication of  
Analog-Relief Diffractive Optics on Non-Flat Substrates at  
Jet Propulsion Laboratory***

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### *Outline*

- Introduction
- E-beam fabrication of analog-relief diffractive optical elements
- Fabrication of blazed gratings on convex substrates
- Summary

**JPL E-Beam System Specifications**

<b>Parameter</b>	<b>Old → JEOL JBX-5D2</b>	<b>New → JEOL JBX-9300FS</b>	
Voltage	50 kV	100 kV	50 kV
Minimum Spot Size	8 nm	4 nm	7 nm
Beam Current for: 100 nm spot	10 nA	175 nA	125 nA
10 nm spot	10 pA	10 nA	4 nA
Field Size	80 μm	500 μm	1000 μm
Pattern Generator Speed	2 MHz	25 MHz	
Field Stitching Accuracy	75 nm 3σ	20 nm 3σ	
Write Area	5 in sq	9 in sq	
Wafer Size	5 in dia	12 in dia	
Writing Grid	25 A	10 A	
Electron Source	LaB <sub>6</sub>	Field Emission Gun	
Cabling	Multiconductor Cables	Ethernet	
Control	OEM Interface to PDP11/84, VAX	Local Smarts - 3 Internal DEC Alpha CPUs	

**Advantages of New System**

- 10x Faster Throughput
- One Half Minimum Spot Size
- 2.5 Times Larger Wafers, 1.8 Times Larger Masks
- 3 Times Better Overlay Precision

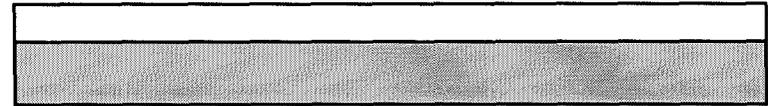
## ***Fabrication Method***

- Thin film of e-beam resist (PMMA or PMGI) spun on substrate
- Direct-write analog-dose electron-beam lithography using JEOL JBX-5DII (50 keV)
- Electron beam breaks bonds in the resist - increases solubility to developer
- Developer etches exposed resist to produce surface relief pattern
- Transfer of patterns into substrate is possible if needed

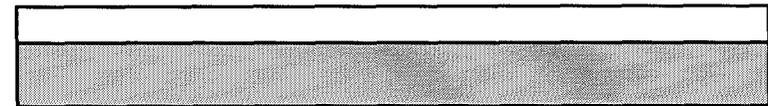
## ***Advantages***

- Well controlled analog depth (< 5% error)
- Arbitrary patterns
- No pattern misalignment
- Prototype elements are efficiently fabricated

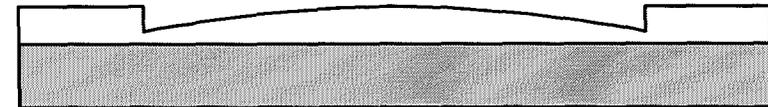
Thin film of e-beam resist on substrate material



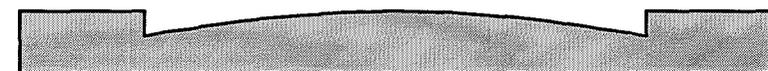
50 keV electrons  
Dwell time



After development



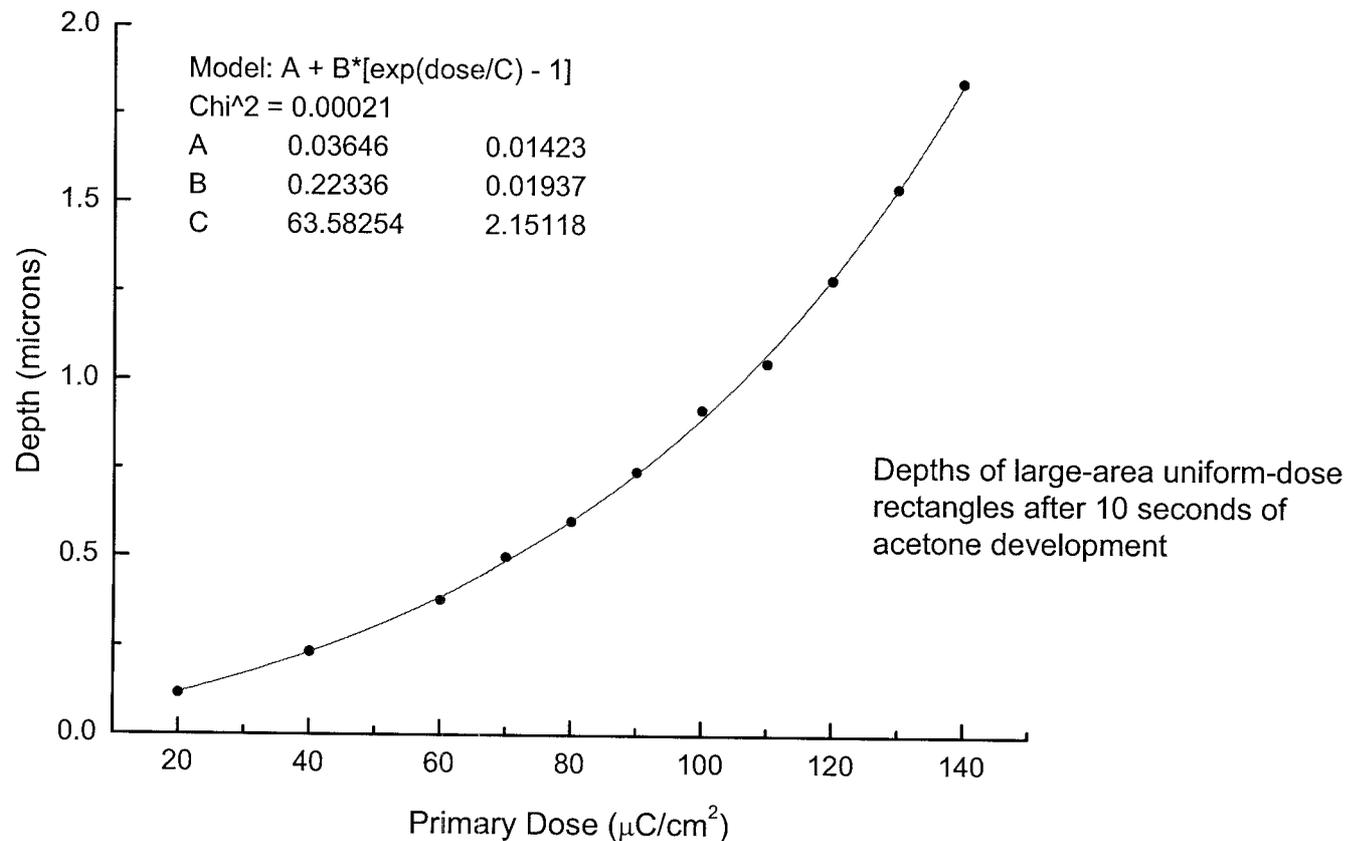
After transfer etching



## E-Beam Pattern Preparation

- Desired surface relief pattern is represented as square pixels (0.025 - 2.5 microns)
- Pixel depths are converted to E-beam doses using the measured nonlinear dose response of PMMA

$$depth = A + B[\exp(dose / C) - 1], \quad dose = C \ln\left(\frac{depth - A}{B} + 1\right)$$



### *E-Beam Pattern Preparation (continued)*

- Proximity effect (dose due to back-scattered electrons) causes neighboring pixels to contribute dose to each other

$$D_{\text{total}}(\mathbf{r}) = D_{\text{primary}}(\mathbf{r}) \otimes PSF(\mathbf{r})$$

$$PSF(\mathbf{r}) = \delta(\mathbf{r}) + \frac{\eta}{\pi\alpha^2} \exp(-r^2/\alpha^2)$$

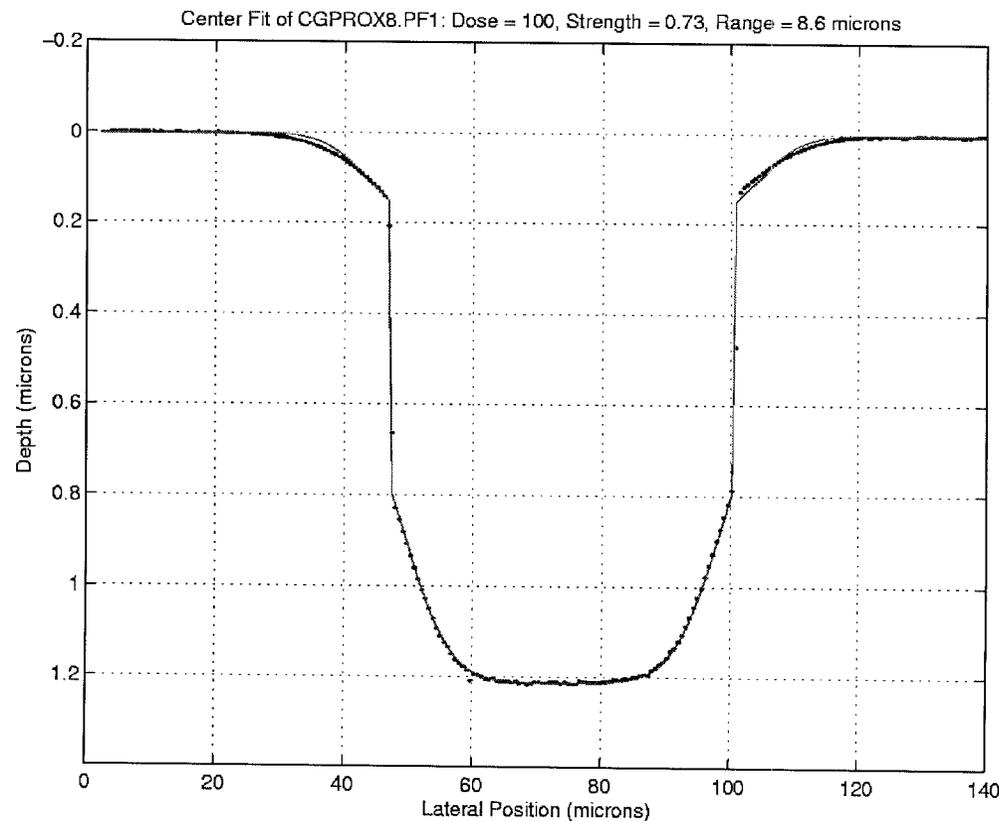
- Fourier deconvolution is used to correct pixel doses so they produce desired total dose

$$D_{\text{primary}}(\mathbf{r}) = F.T.^{-1} \left\{ \frac{F.T.\{D_{\text{total}}(\mathbf{r})\}}{F.T.\{PSF(\mathbf{r})\}} \right\}$$

## E-Beam Proximity Effect Measurement

- Uniform-dose rectangles are developed for 10 seconds in pure acetone then profiled with an atomic force microscope (AFM)
- Depth profiles are fit with analytical convolution of rectangle with PSF to yield strength  $\eta$  and range  $\alpha$

$$D_{tot} = D_p \text{rect}\left(\frac{x}{w}\right) + D_p \frac{\eta}{2} \left[ \text{erf}\left(\frac{x+w/2}{\alpha}\right) - \text{erf}\left(\frac{x-w/2}{\alpha}\right) \right], \quad \text{depth} = A + B \left[ \exp\left(\frac{D_{tot}}{C(1+\eta)}\right) - 1 \right]$$



$$PSF(\mathbf{r}) = \delta(\mathbf{r}) + \frac{\eta}{\pi\alpha^2} \exp(-r^2/\alpha^2)$$

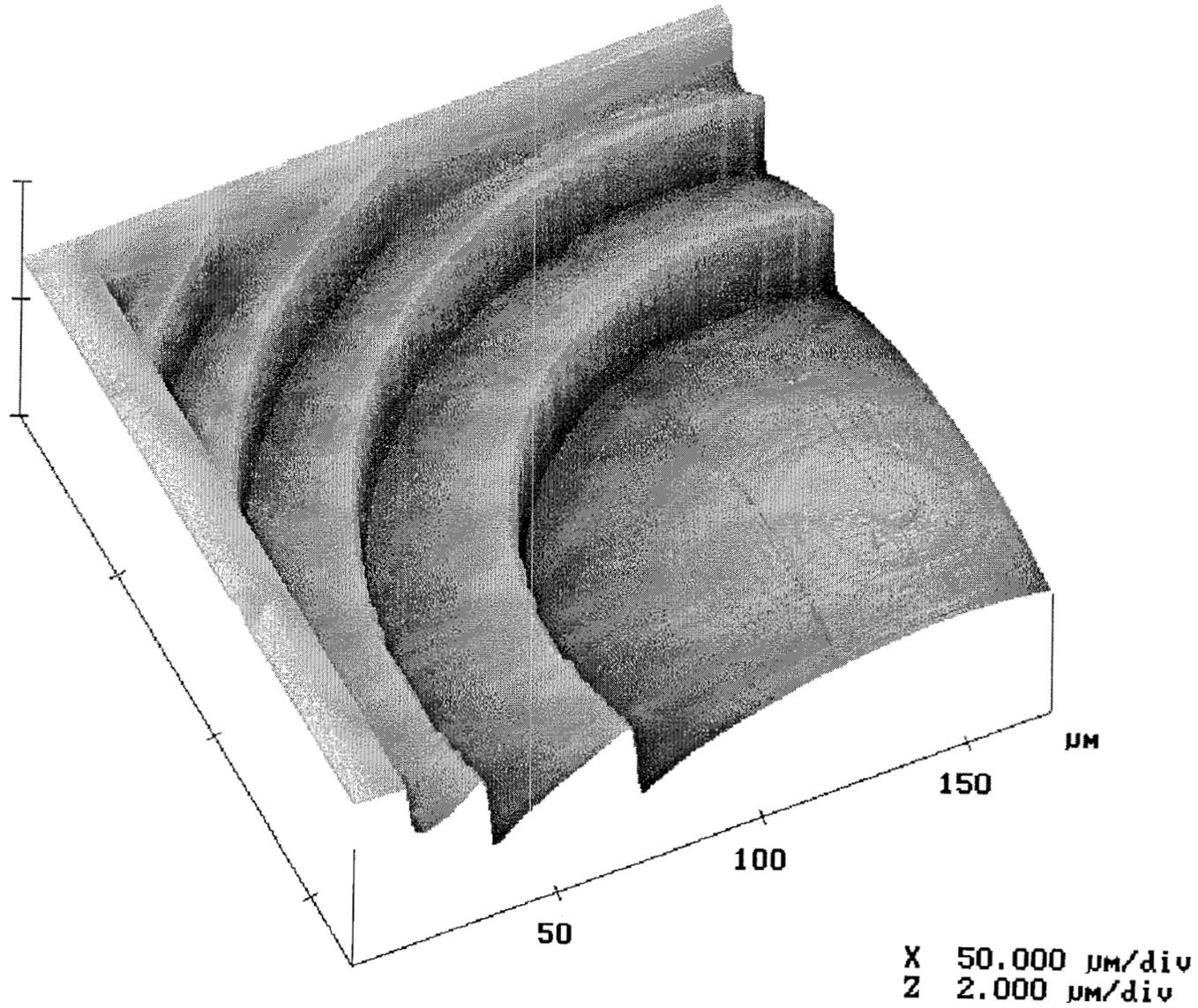
Substrate	Strength $\eta$	Range $\alpha$ ( $\mu\text{m}$ )
Fused Silica	0.50	10.7
Schott CG-455	0.73	8.6
GaAs	0.93	6.0
Aluminum	0.47	9.3

## *Exposure*

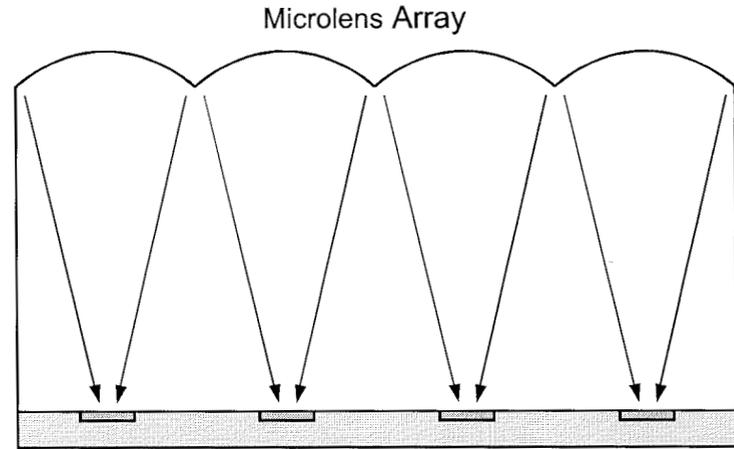
- Blazed profiles
  - Use few E-beam spots per pixel, high current
  - Example: 1.2 micron pixels: 3x3 spots/pixel, 40 nA - **0.7 hrs/cm<sup>2</sup>**
- Sharp-edged pixels
  - Use multiple E-beam spots per pixel, low current
  - Example: 2 micron pixels: 10x10 spots/pixel, 9 nA - **7 hrs/cm<sup>2</sup>**

## *Development*

- Iterative, with measurement in-between development steps
- Reflective optics
  - Surface profile measurement
- Transmissive optics
  - CGH that produces null zeroth order at correct depth

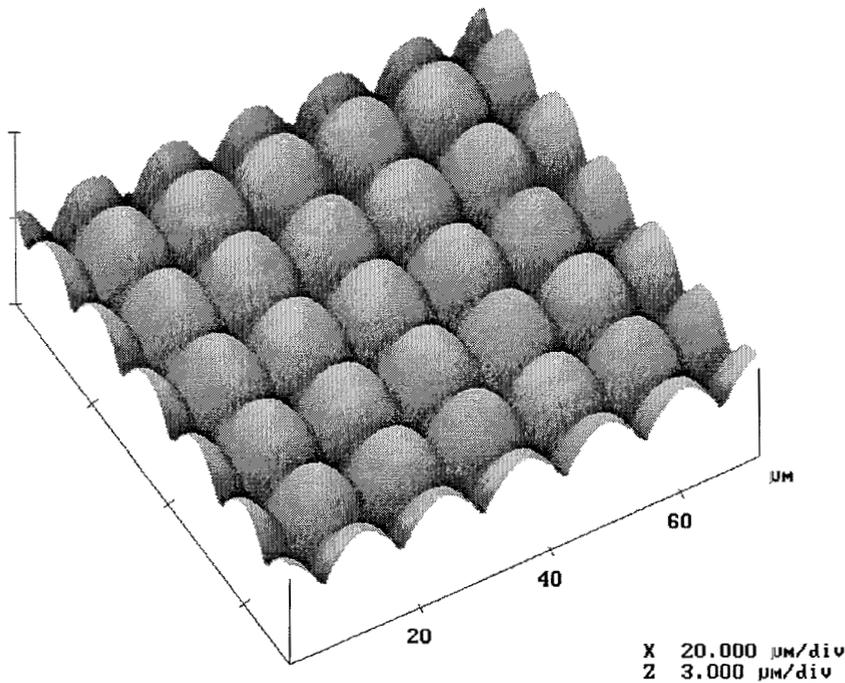


- Microlenses can improve the fill factor of focal plane arrays (CCDs, CMOS active pixel sensors)
- Lenses fabricated by direct-write electron-beam lithography in PMMA on thin quartz substrate
- Lens array aligned and bonded to detector

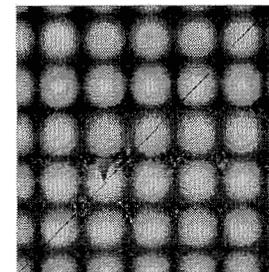
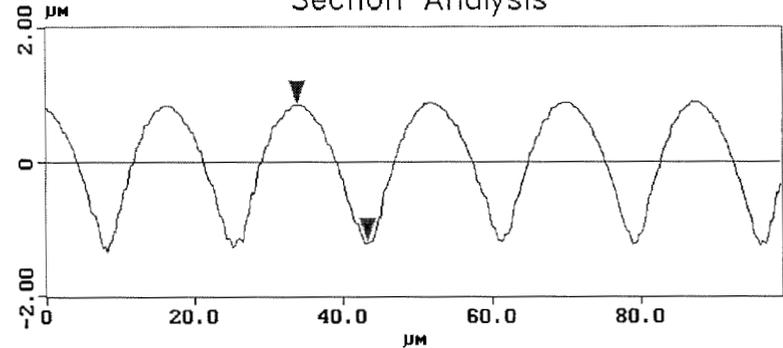


Focal plane array with < 100% fill factor

Surface Profile of Microlens Array

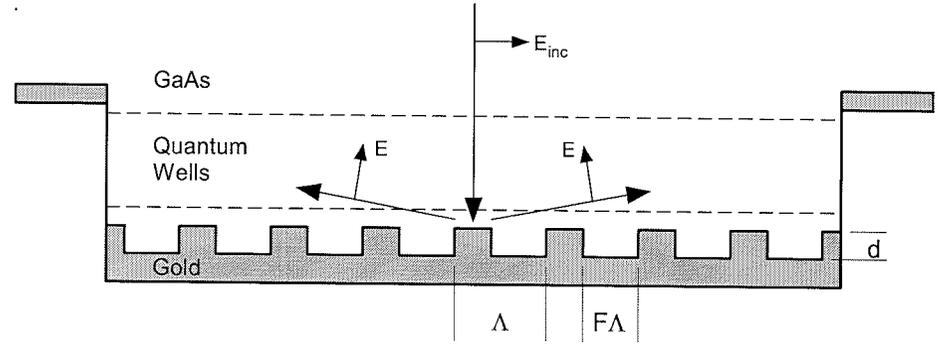


Section Analysis



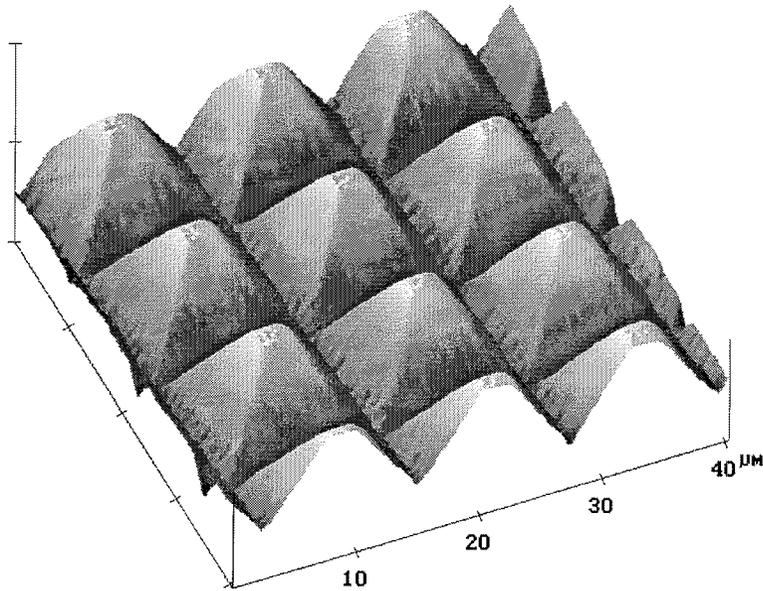
Horiz	9.563 µm	Desired
Vert	2.066 µm	2.01
Angle	12.193 deg	

- Quantum well infrared photodetectors (QWIPs) require that light propagate parallel to quantum well layers to be absorbed

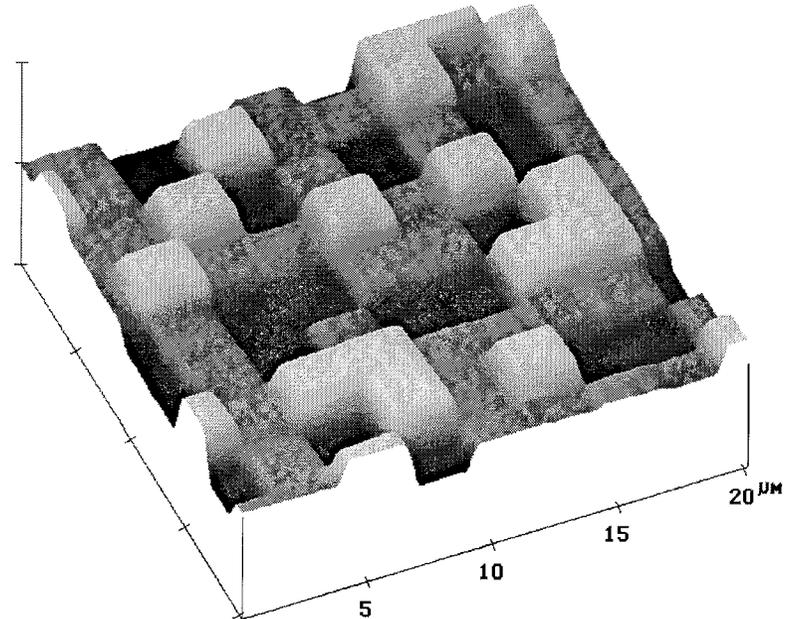


Pyramid structure reflects incident light horizontally inside pyramids

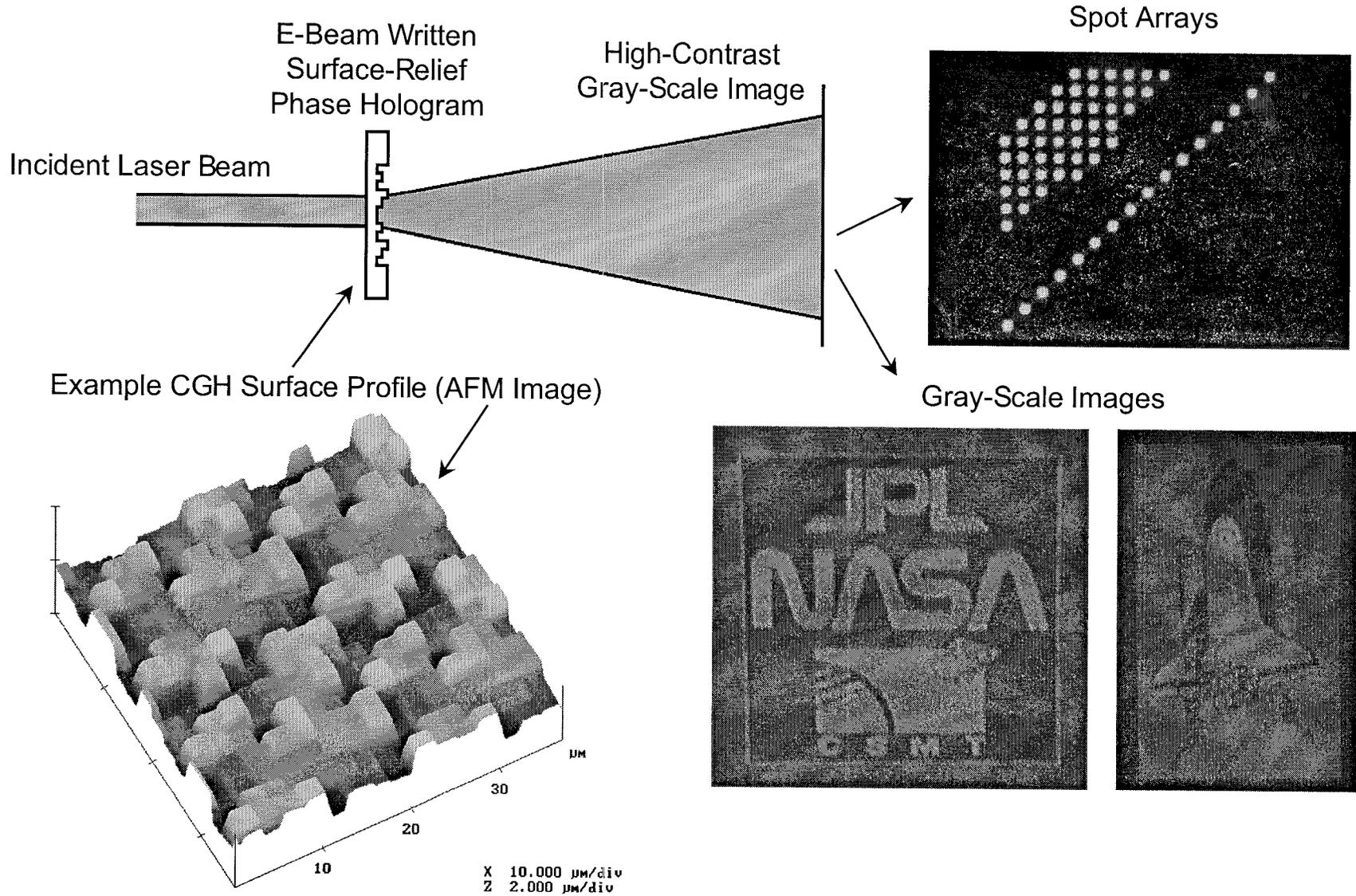
Achromatic random reflector is designed to have zero normal-incidence reflectivity at 2 wavelengths



X 10.000  $\mu\text{m}/\text{div}$   
Z 1.500  $\mu\text{m}/\text{div}$



X 5.000  $\mu\text{m}/\text{div}$   
Z 1.000  $\mu\text{m}/\text{div}$



## Imaging Spectrometry

1. Measure the spectra of all pixels in a scene
2. Analyze the spectra to obtain useful information about the scene

## Applications

### Remote Sensing

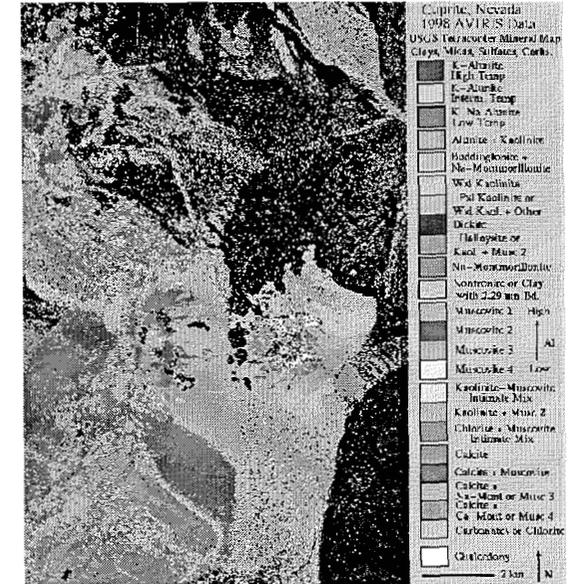
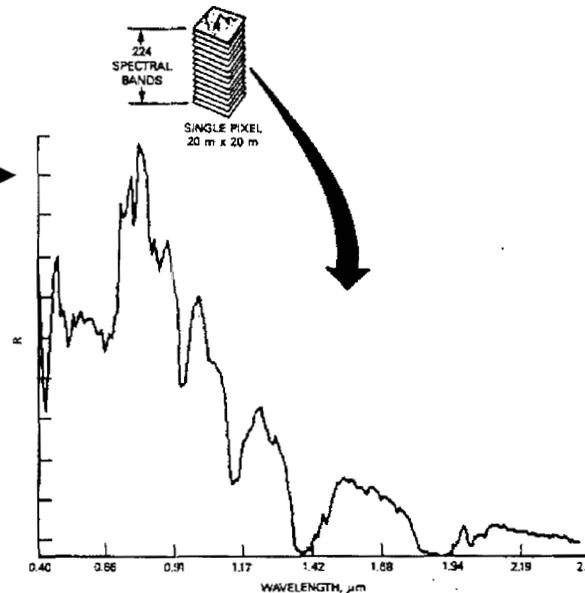
- Mineral exploration
- Hazardous waste monitoring
- Crop/forest health
- Fire/Wetlands monitoring

### Defense

- Target identification
- Chemical warfare warning

### Biology/Medicine

- Abnormal tissue identification
- Fluorescence studies of cellular processes

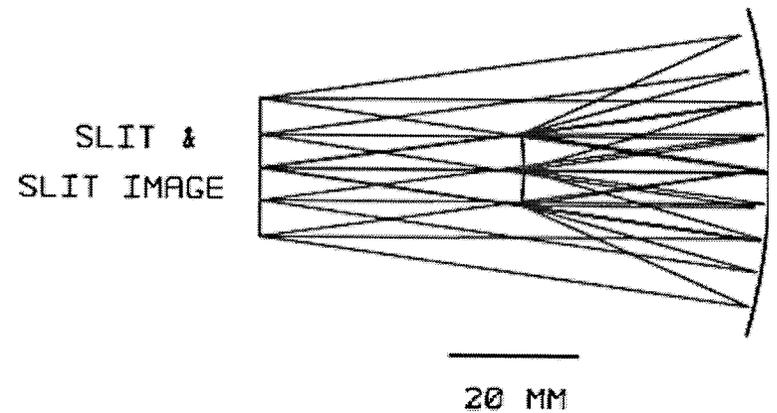
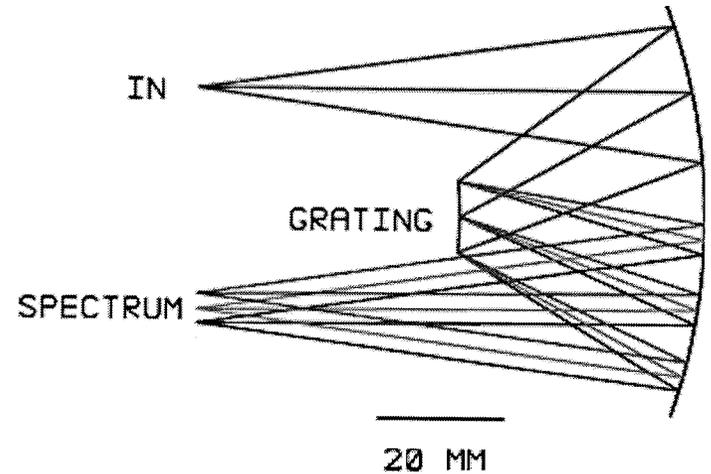
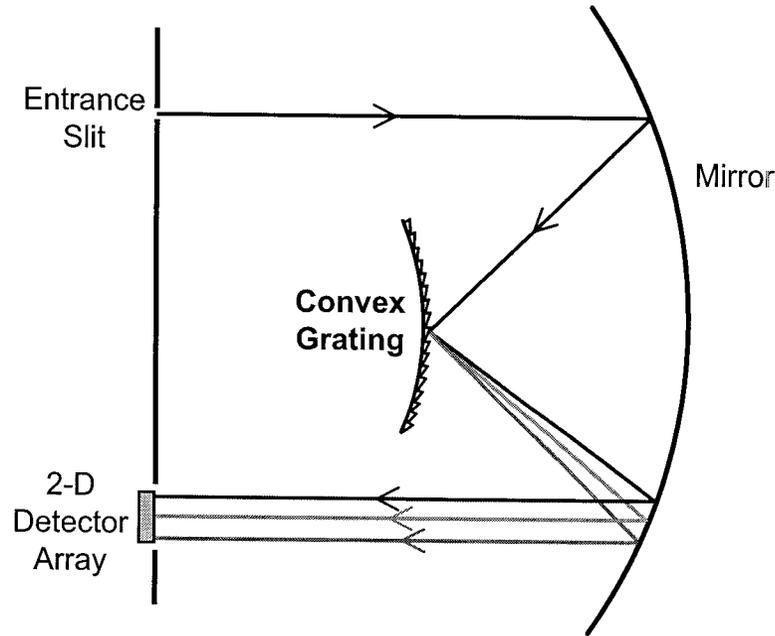


AVIRIS Data of Cuprite, Nevada

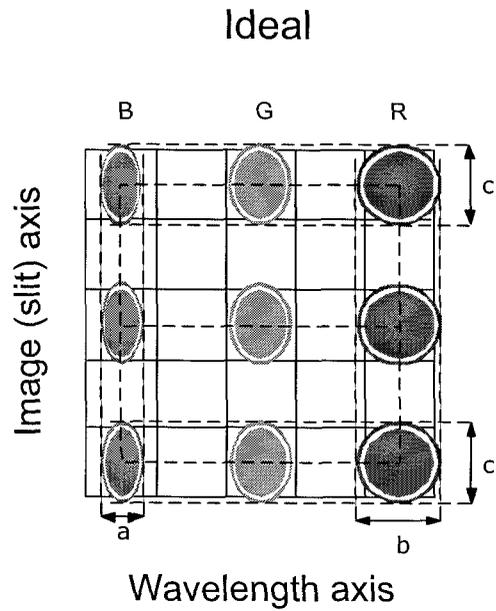
## Slit Imaging Spectrometer

- Spectrometer measures spectra for all points along a slit. Spectrometer is mounted aboard a scanning platform (aircraft or spacecraft) to collect spectra for a 2D area (“pushbroom scanning”)

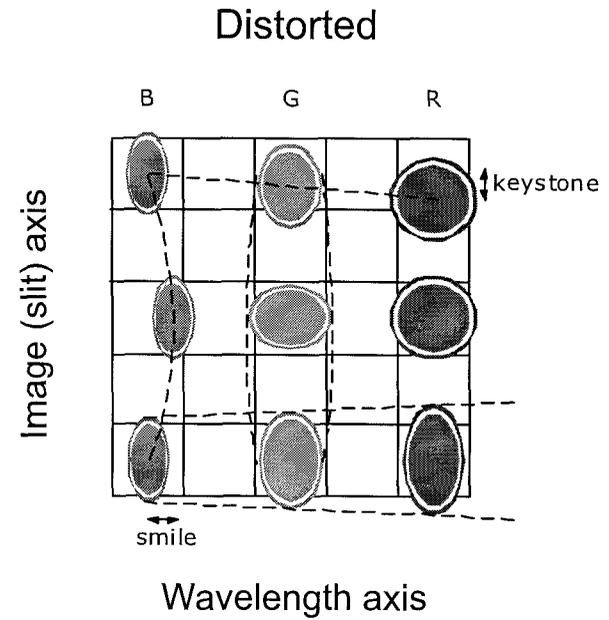
*Slit imaging spectrometer based on the Offner concentric two-mirror design*



- Can be designed to have *very low slit-image distortion*
  - Minimizes pixel crosstalk
  - Greatly simplifies calibration of the spectrometer
- Can be very compact and lightweight
- Requires a convex grating (blazed for high efficiency)

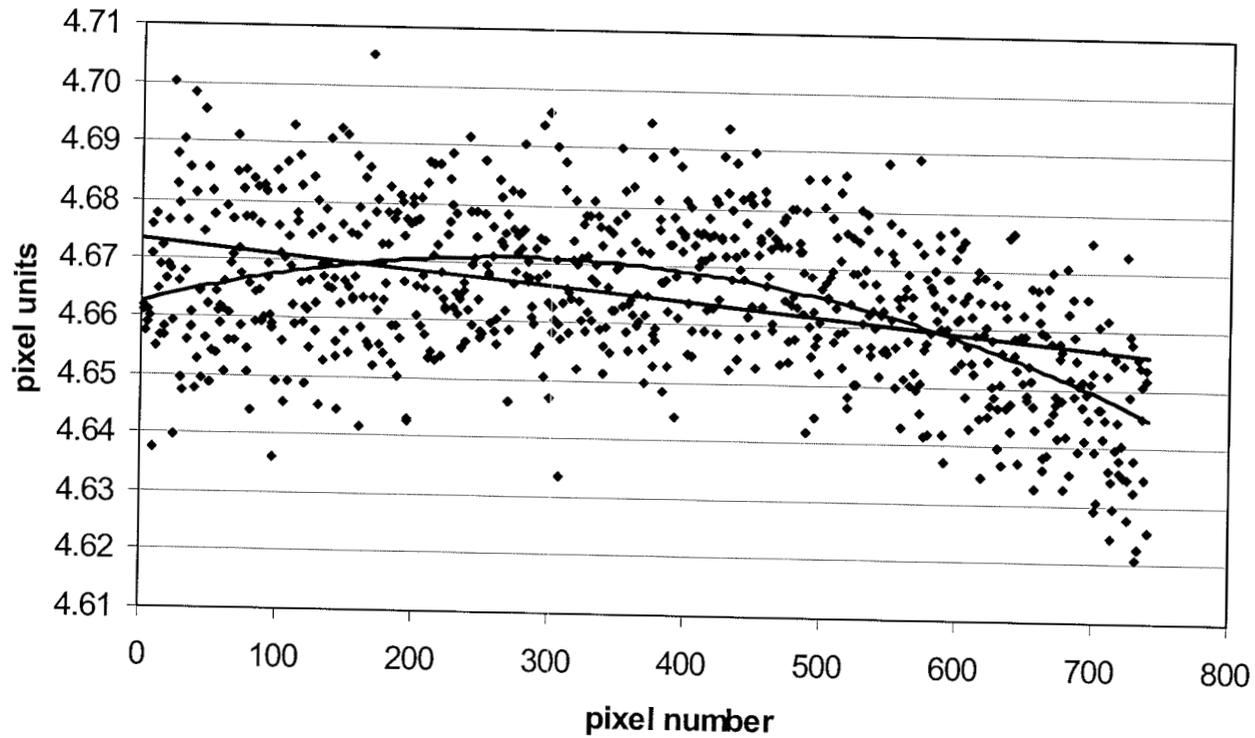


High spectral and spatial uniformity



Low spectral and spatial uniformity  
Compromises data recovery

Image of the 546.1 nm Hg spectral line: smile < 0.03 pixel

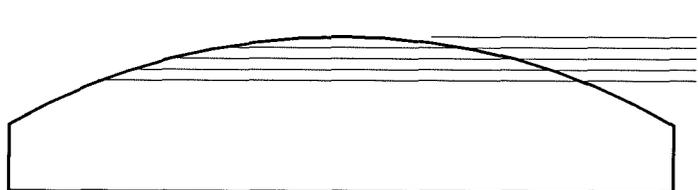
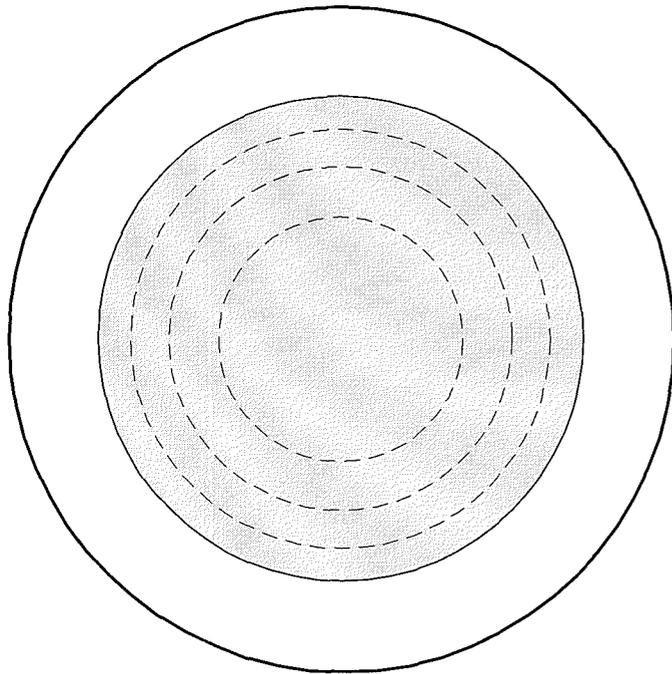


## Convex Grating Fabrication

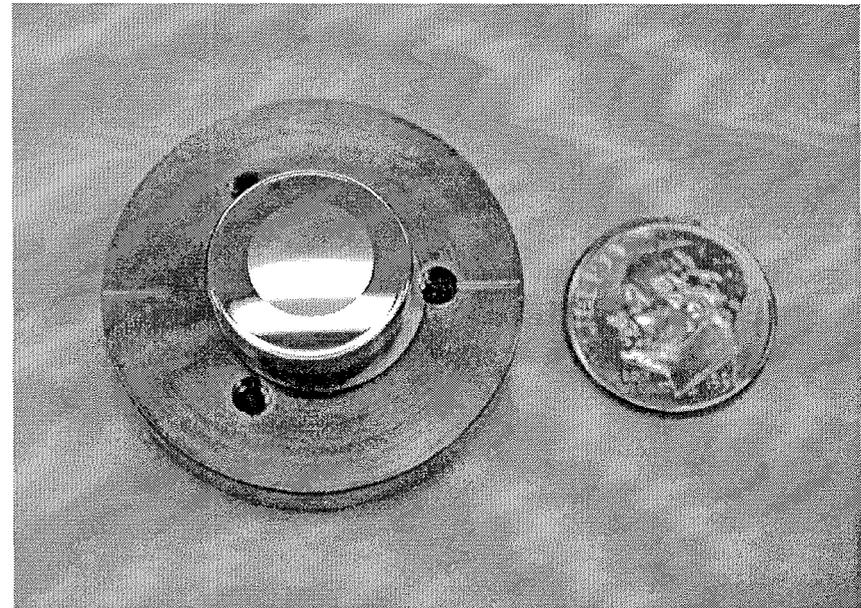
- Pattern is broken in to annular sections that cover equal height steps of ~50 microns (E-beam depth of field)
- E-beam *focus, deflector gain, and rotation* are corrected for each annular pattern

Single-blaze grating on aluminum substrate for NASA New Millenium EO-1 Mission

- Selected over diamond-ruled and holographic gratings based on measurements of efficiency, scattering, and wavefront quality



Equal height slices



Delivered gratings for

- TRW Hyperion (NASA New Millenium EO-1 mission)
- Another project “Spectrometer 1 and Spectrometer 2”

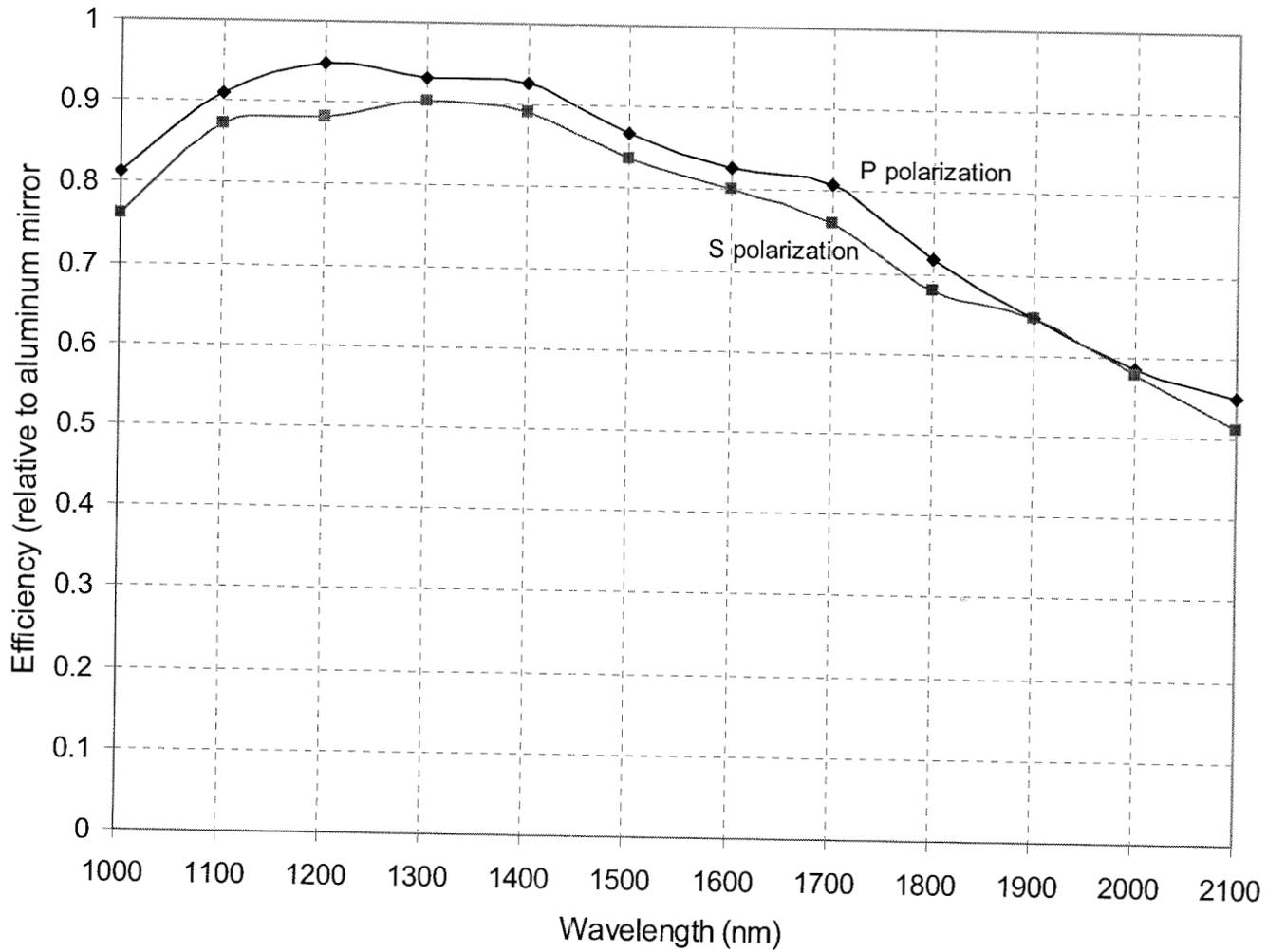
Specifications and performance of flight-instrument gratings

Grating	Diameter	Period	Blaze Angle	Substrate Sag	Wavelength range (order)	Peak Efficiency <sup>†</sup> , Wavelength (order)	Ghosts, Scatter <sup>‡</sup>
Hyperion VNIR	14 mm	17.4 $\mu\text{m}$	0.55 deg	0.23 mm	0.4 – 0.85 $\mu\text{m}$ (-1)	92% @ 490 nm	0.025%
Hyperion SWIR	14 mm	17.4 $\mu\text{m}$	2.27 deg	0.23 mm	1.13 – 2.55 $\mu\text{m}$ (-1)	92% @ 1450 nm	0.16%
Spect. 1 Dual-band	29 mm	35.7 $\mu\text{m}$	1.19 deg	1.27 mm	0.5 – 0.85 (-2) 1.0 – 2.45 (-1)	91% @ 0.63 $\mu\text{m}$ (-2) 93% @ 1.26 $\mu\text{m}$ (-1)	0.05%
Spect. 2 MWIR	36.6 mm	103.6 $\mu\text{m}$	1.12 deg	0	3 – 5 $\mu\text{m}$ (-1)	Not Meas.	Not Meas.

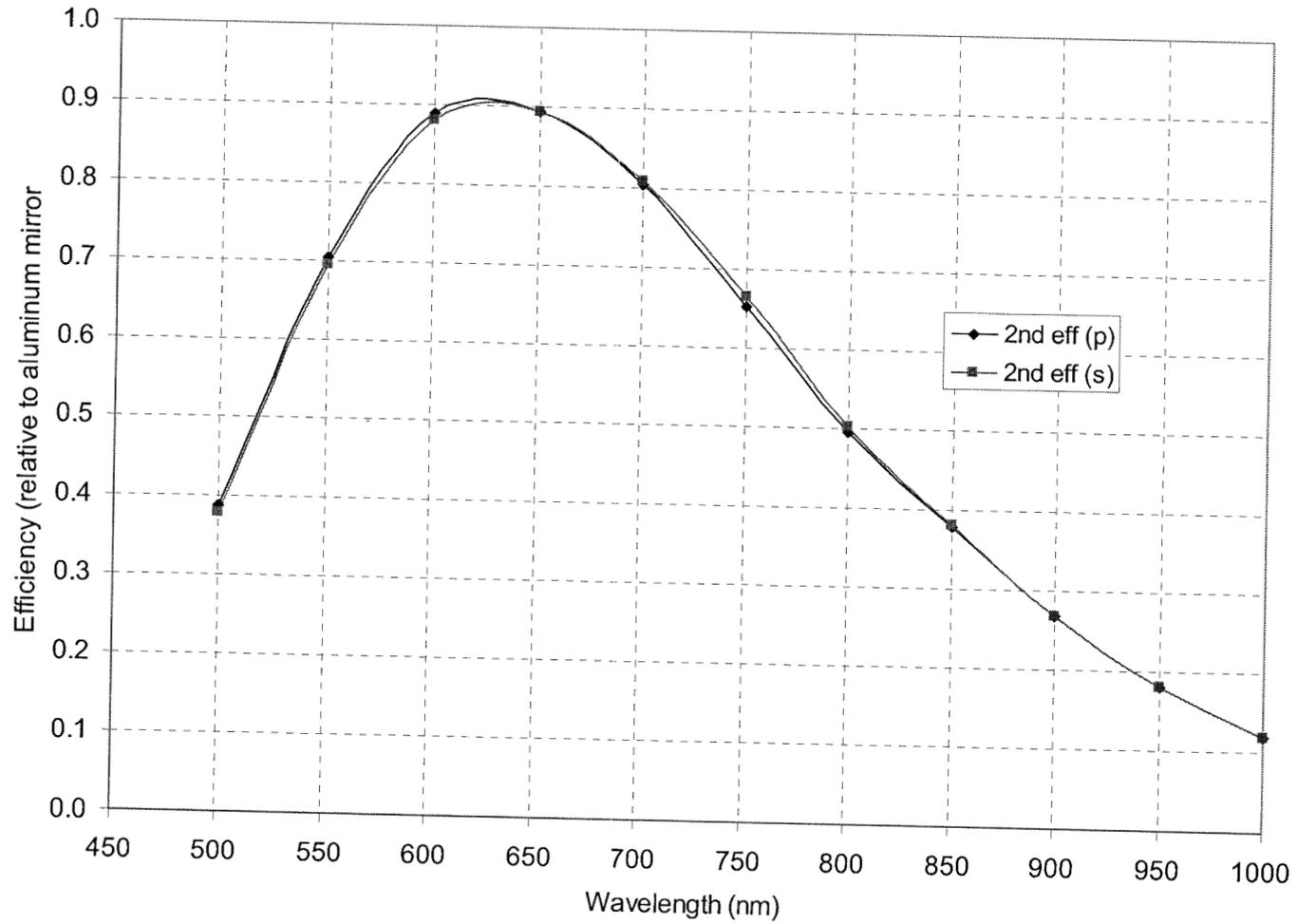
† - relative to an aluminum mirror

‡ - compared to the brightest order at 633 nm, in all cases ghosts dominated over diffuse scatter

Spectrometer 1 Grating (1st Order)



### Spectrometer 1 Grating (2nd Order)



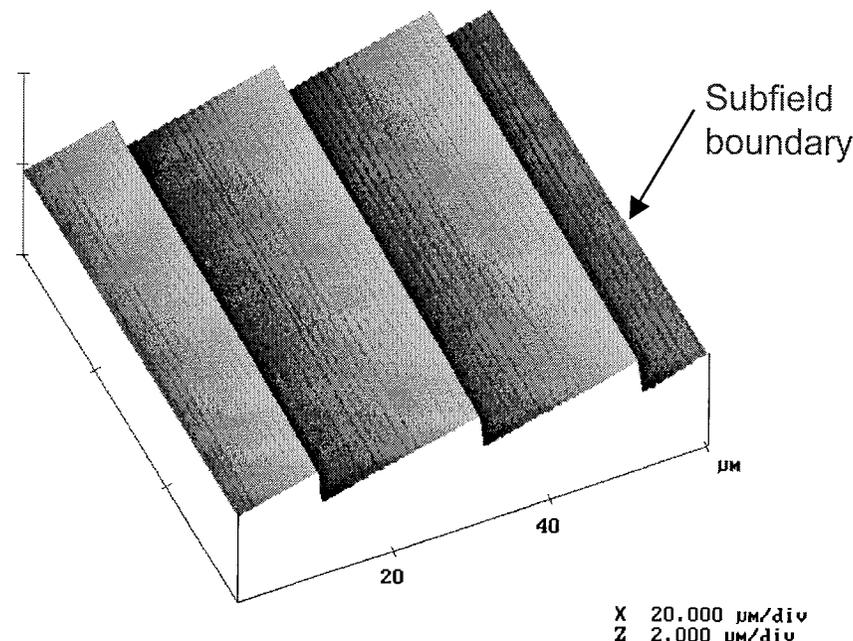
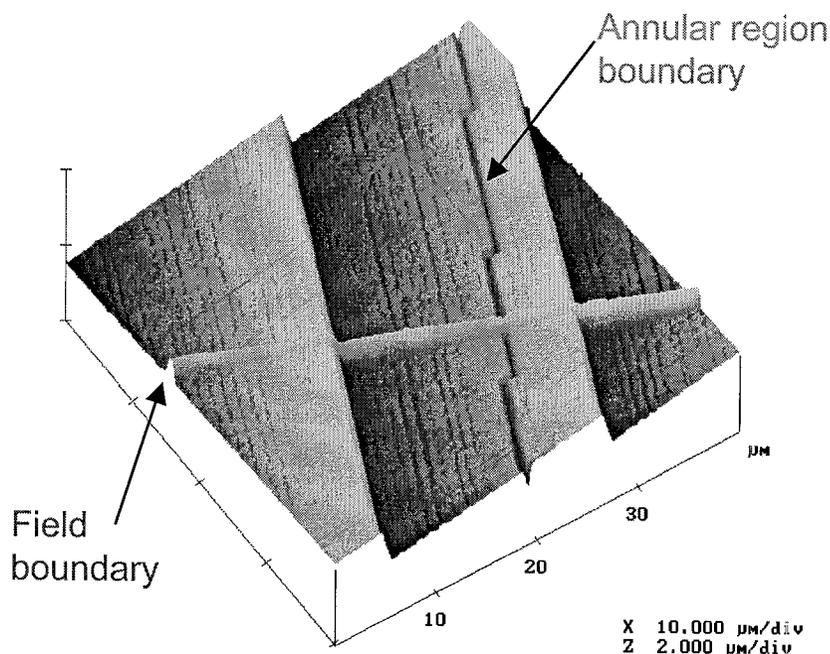
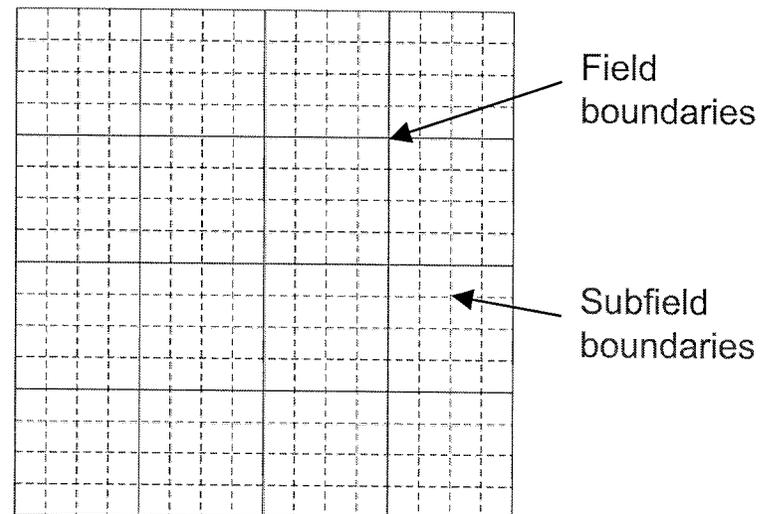
**Pattern broken into square regions (JEOL JBX5D2)**

- Fields (800 microns max) - stage moves
- Subfields (100 microns max) - region of deflector calibration

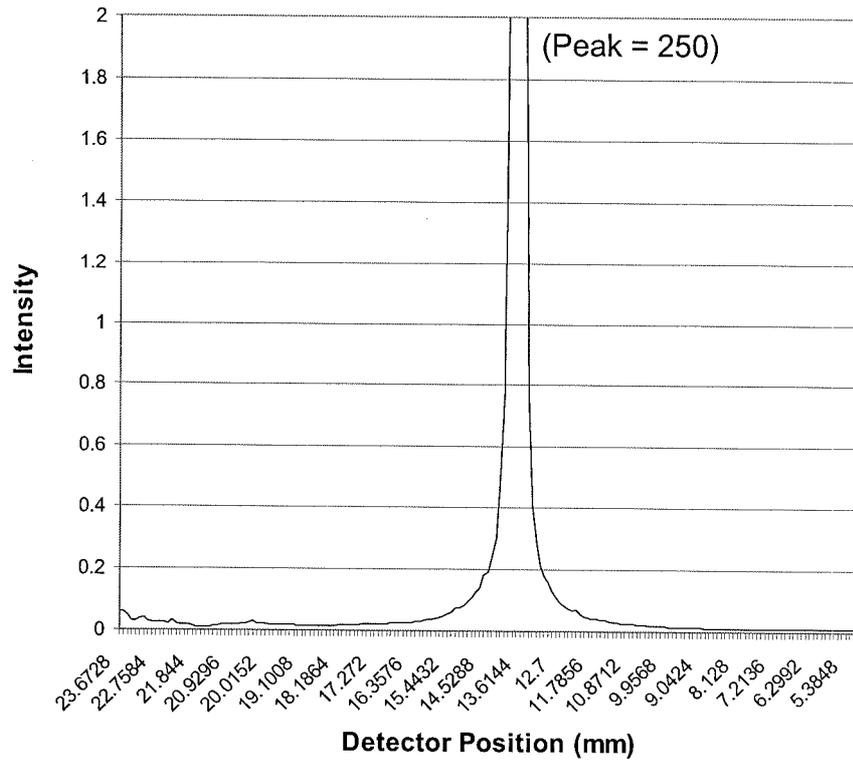
**Subfield ghost orders**

- If  $N$  periods per subfield
- Period for ghost is  $N$  times grating period, so sine of ghost angle is  $1/N$  times sine of grating angle
- $N-1$  ghost orders appear between main diffraction orders

Total Pattern

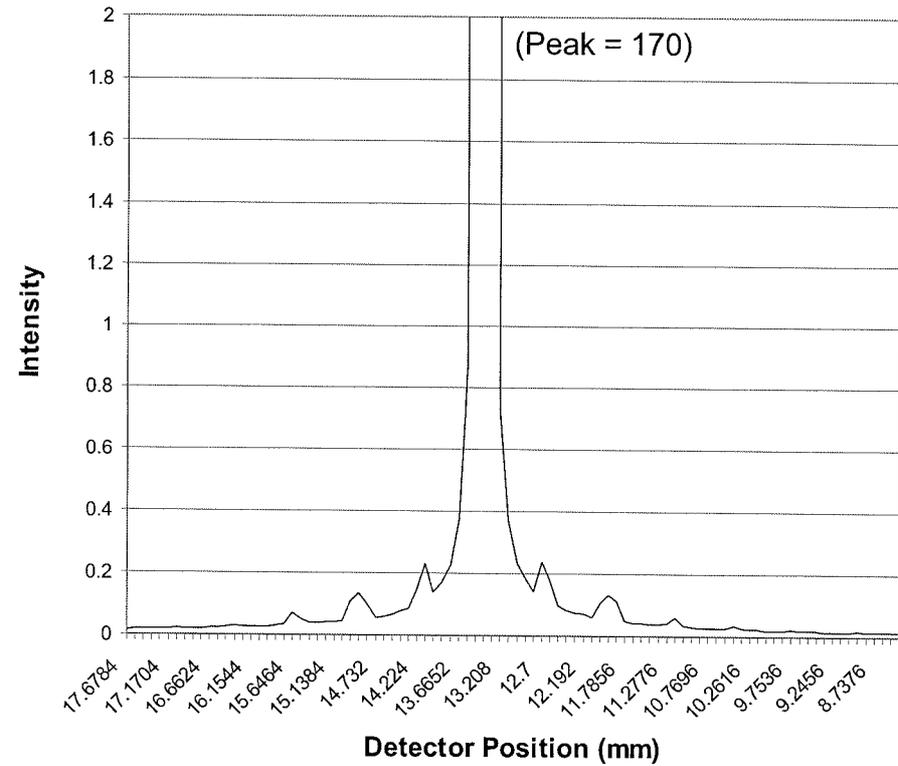


**VERTICAL SCATTER of VNIR GRATING (S/N 7)**



Scatter = 0.025%

**VERTICAL SCATTER of SWIR GRATING (S/N 3)**

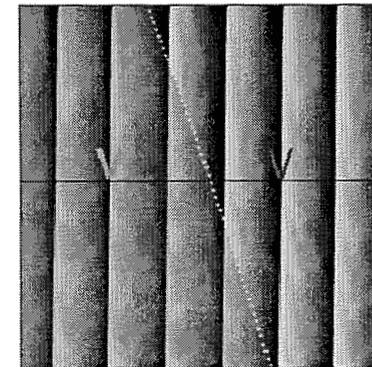
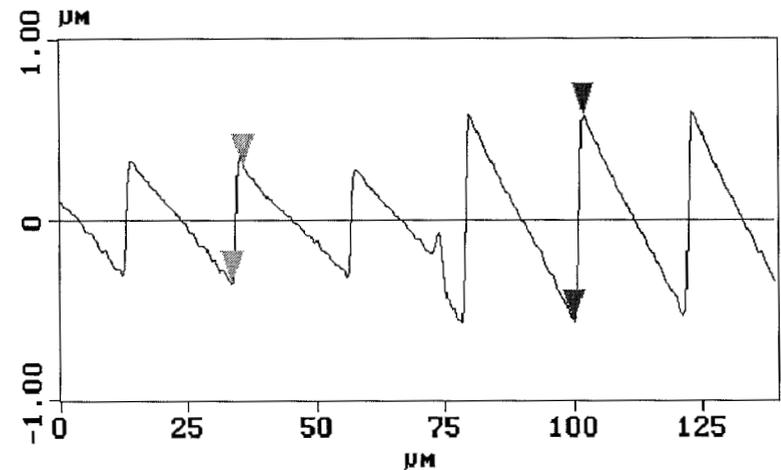
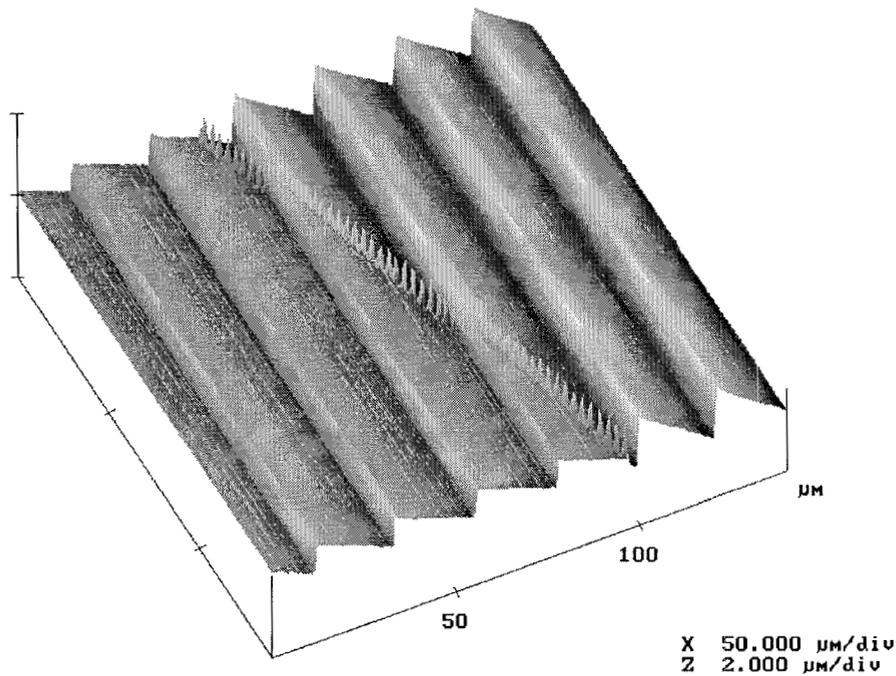


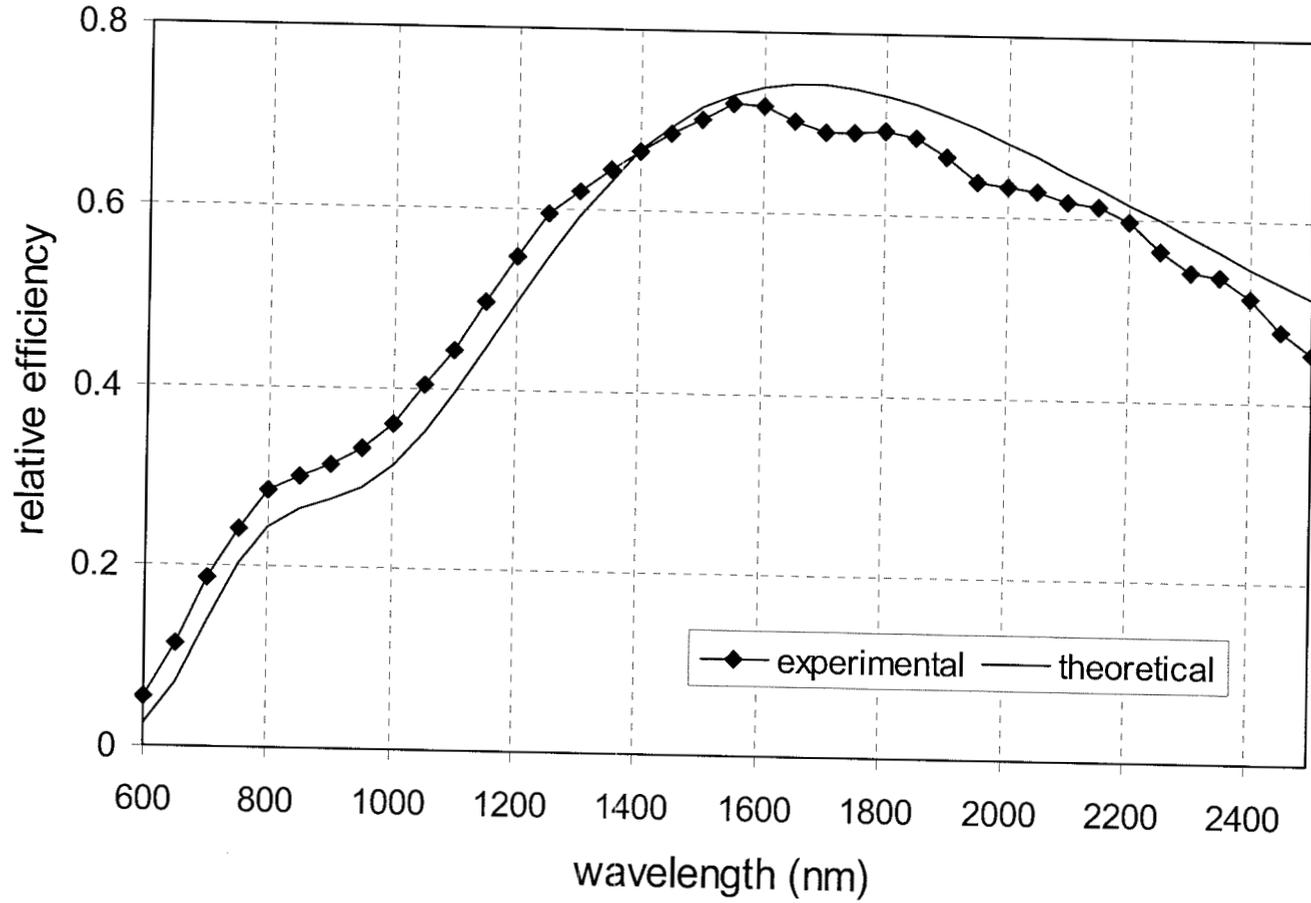
Scatter = 0.16%

**Dual-Blaze Convex Grating**

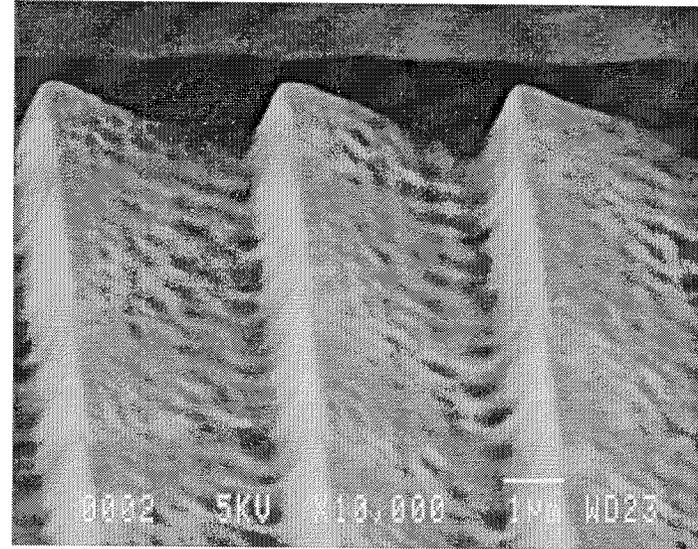
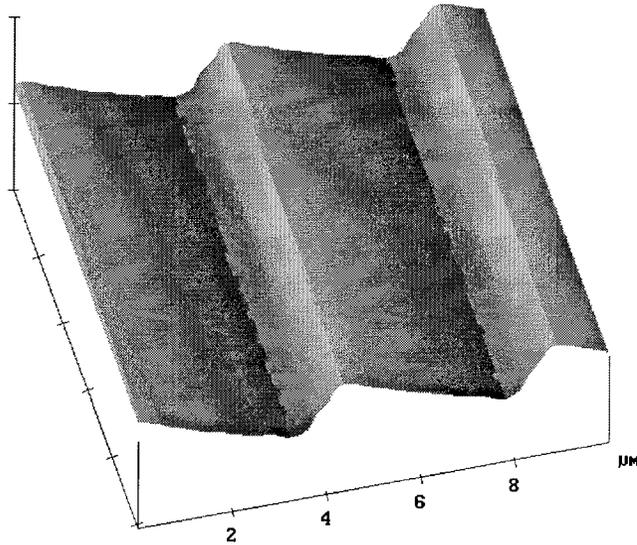
- Constant period over entire area
- Two blaze angles:
  - center circle blazed for visible
  - outer annulus blazed for infrared
- High Efficiency for both Visible and Infrared
- Provides flat and high signal to noise ratio.

AFM profile of a dual-blaze convex grating showing blaze-angle zone boundary

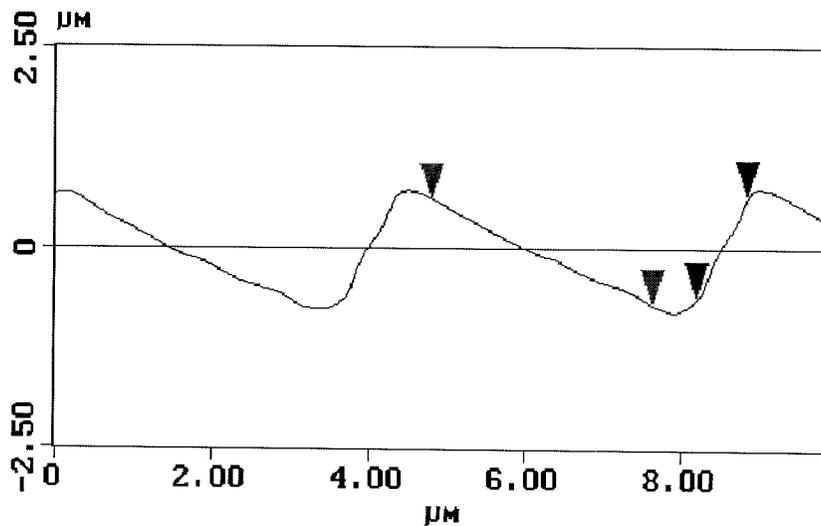




- Period = 4.34 microns
- Blaze angles = 26.2 deg, 63.8 deg (depth = 1.626 microns)



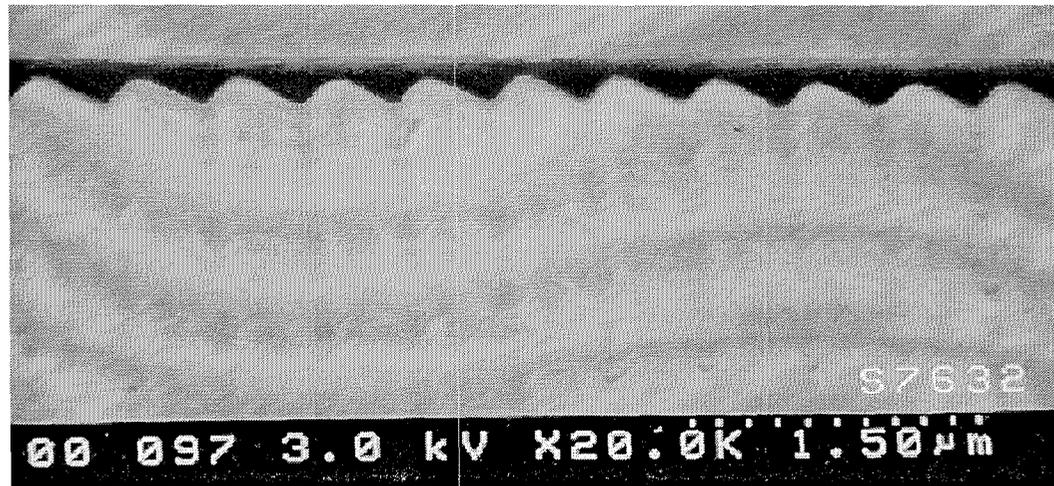
X 2.000  $\mu\text{m}/\text{div}$   
Z 3.000  $\mu\text{m}/\text{div}$



Horiz distance(L)	2.813 $\mu\text{m}$
Vert distance	1.316 $\mu\text{m}$
Angle	25.068 deg
Horiz distance	625.00 nm
Vert distance	1.269 $\mu\text{m}$
Angle	63.776 deg

Sharp AFM tip was used so both angles are accurate.

Blazed grating with 0.5 micron period (2000 lines/mm)



## *Summary*

- Analog E-beam lithography can produce high-performance diffractive optical elements
- Convex gratings are required for Offner imaging spectrometers
- Direct-write electron-beam fabrication technique works well
  - Non-flat substrates (convex or concave, aspheric)
  - Very efficient blazing (arbitrary groove profile)
  - Can write non-straight grooves for aberration correction
  - Ghost orders and roughness can be improved
  - For fine-period gratings, field stitching is an issue

## **Electron-Beam Fabrication of Analog-Relief Diffractive Optics on Non-Flat Substrates at Jet Propulsion Laboratory**

Dan Wilson, Paul Maker, and Rich Muller

### Abstract

Electron-beam lithography can be used to fabricate high-performance analog-depth diffractive optical elements (DOEs). We have recently extended our technique to allow fabrication of analog DOEs on non-flat (convex and concave) substrates. Specifically, we have fabricated convex blazed gratings that exhibit greater than 90% diffraction efficiency. Several of our gratings have been used in compact space borne imaging spectrometers. We will describe the details of our fabrication process including height calibration, pattern fracturing, proximity effect compensation, E-beam exposure, and resist development.