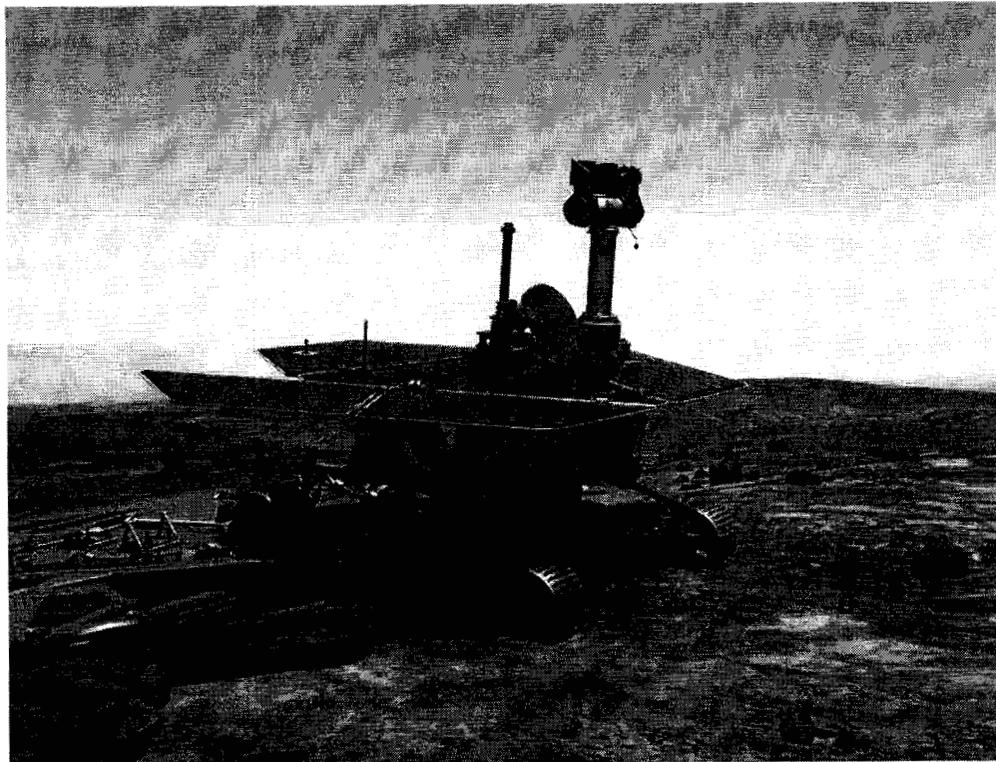




JPL

Development of a Thermal Control Architecture for the Mars Exploration Rovers



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Jet Propulsion Laboratory/California Institute of Technology**

STAIF 2003 Conference – Feb. 4, 2003



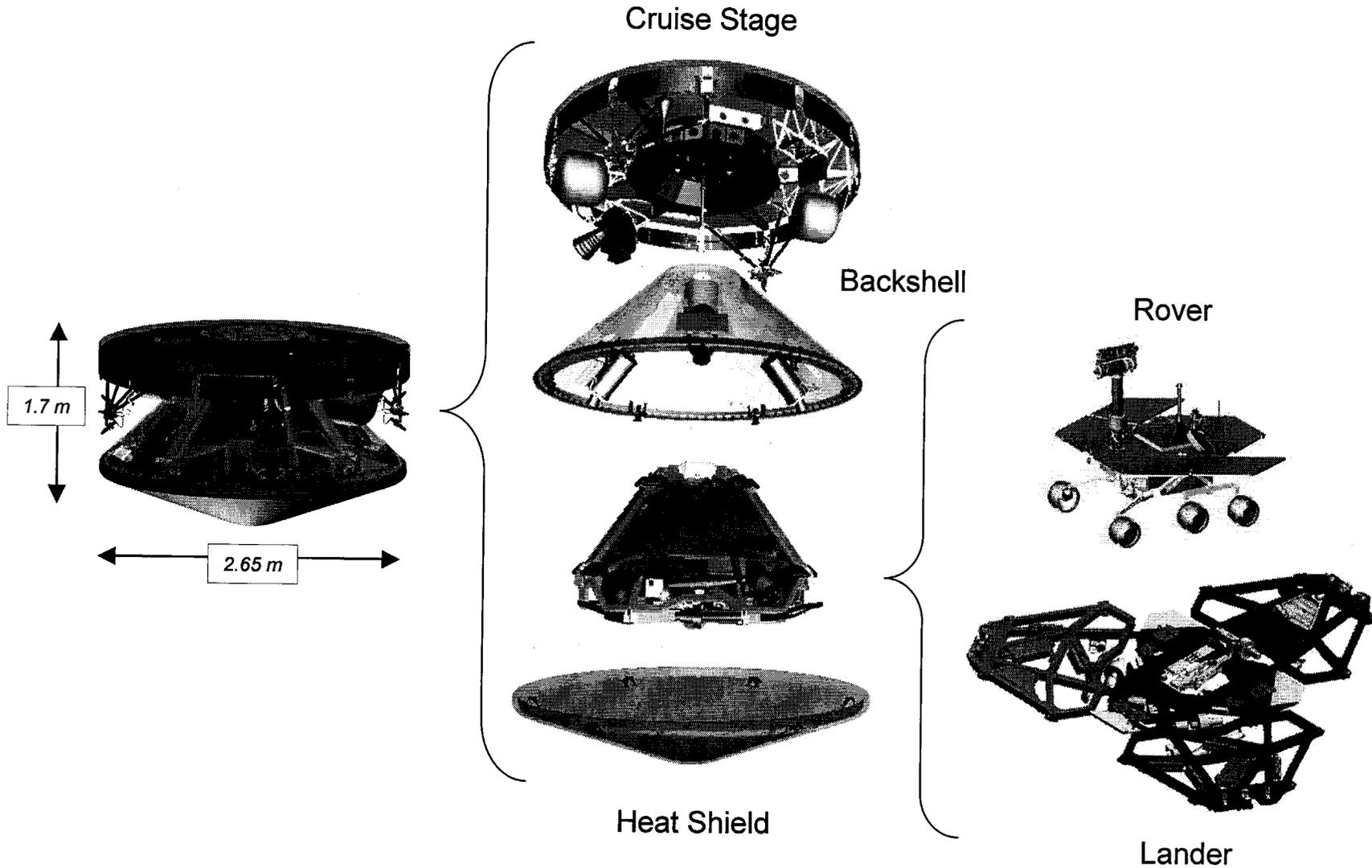
MER Project Description



- **The Mars Exploration Rover (MER) is a mission to land two identical roving science vehicles on Mars and perform geological science data collection with a surface science operations lifetime of at least 90 sols.**
- **The missions will launch in the 2003 opportunity (June - July) on separate Delta II class vehicles, land on Mars in Jan 2004, deploy the rovers and conduct surface operations.**
 - **MER - A is the first launched (May - June 2003), first arriving (early Jan. 2004) flight system.**
 - **MER - B is the second launched (June - July 2003), second arriving (late Jan. 2004) flight system.**
- **Each Flight System consists of:**
 - **A cruise stage and entry, descent and landing system (EDL) with inheritance from the Mars Pathfinder (MPF) development**
 - **A rover based upon the Athena Rover developments undertaken for the Mars '01 and Mars Sample Return projects (1 km traverse capability)**
 - **Athena Science Package, 5 science instruments to conduct remote and in-situ observations**



MER Spacecraft Configuration

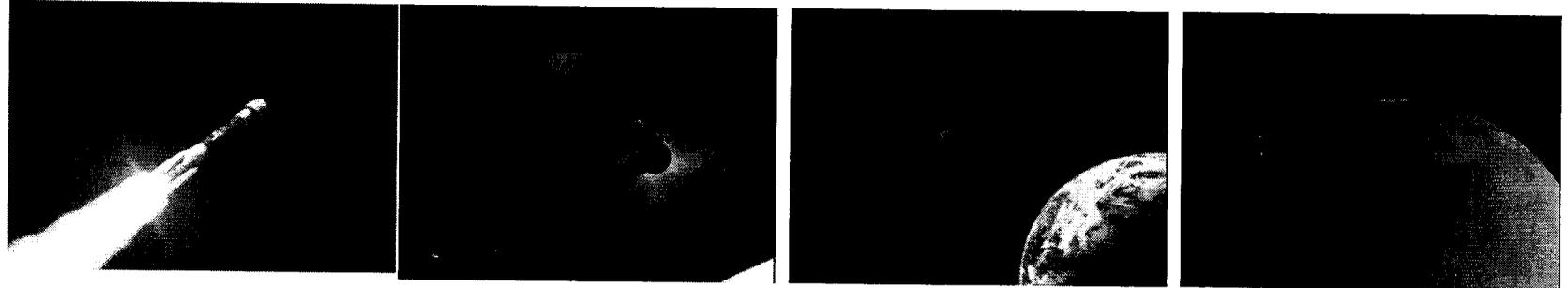




Mission Overview



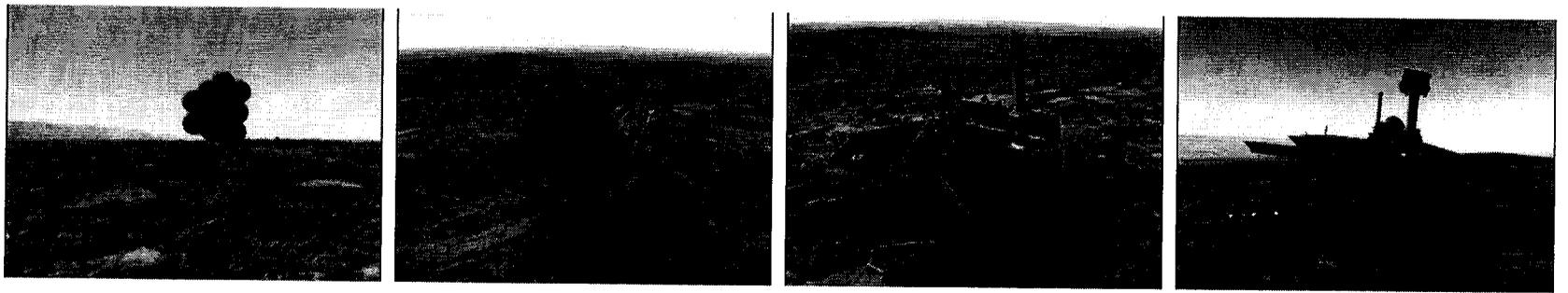
Launch/Cruise



EDL



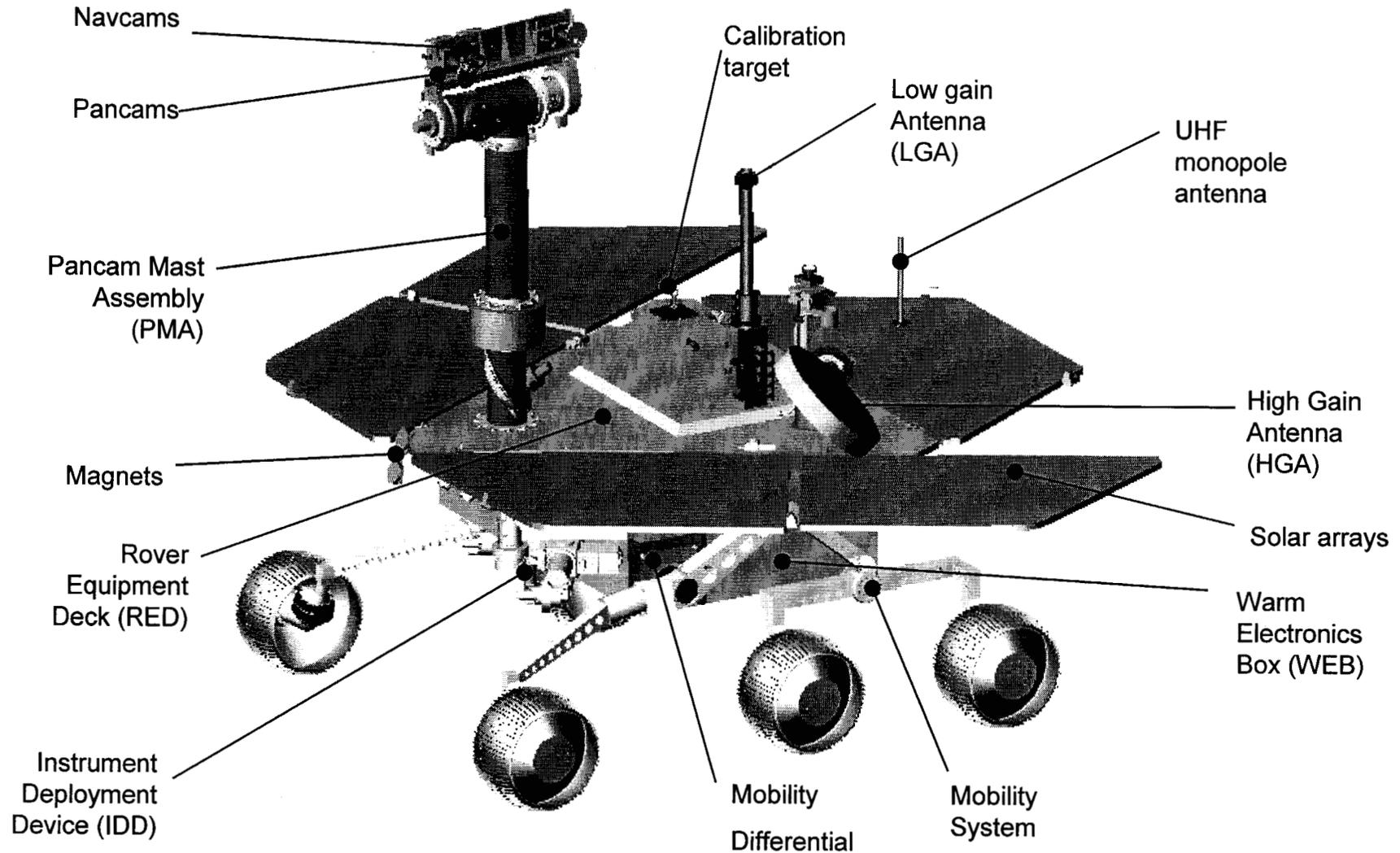
Surface



Images From Mission Animation by Dan Maas

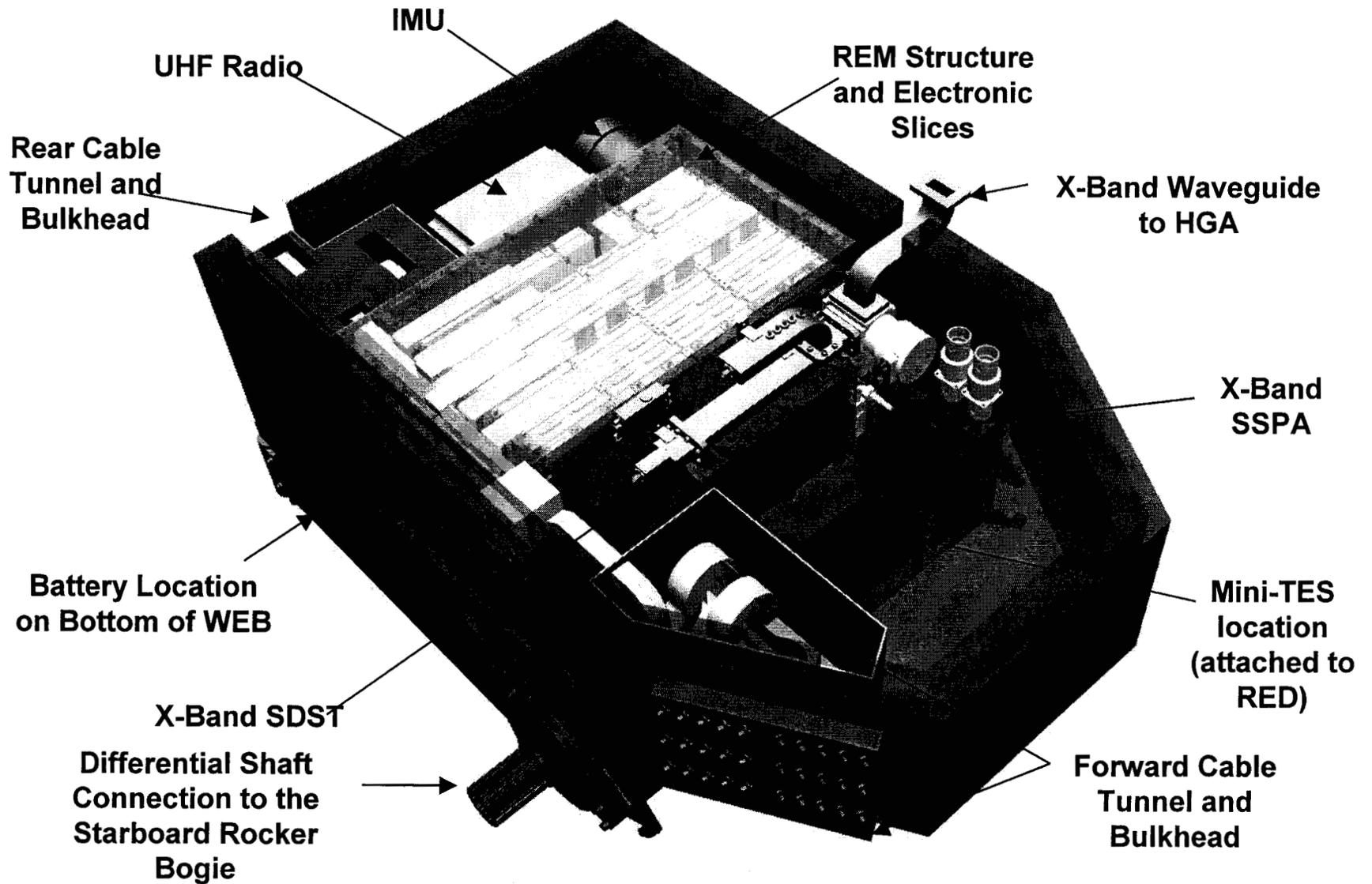


Rover Configuration - Deployed





Rover Warm Electronics Box





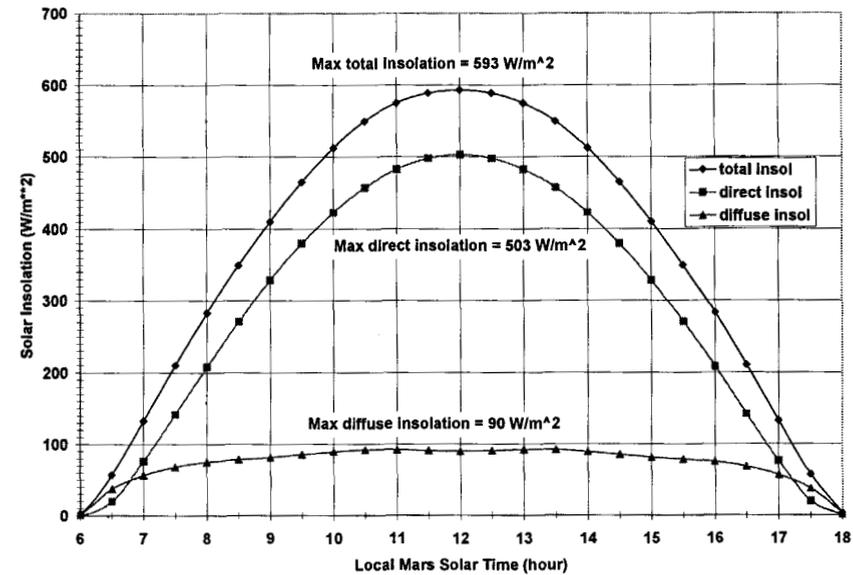
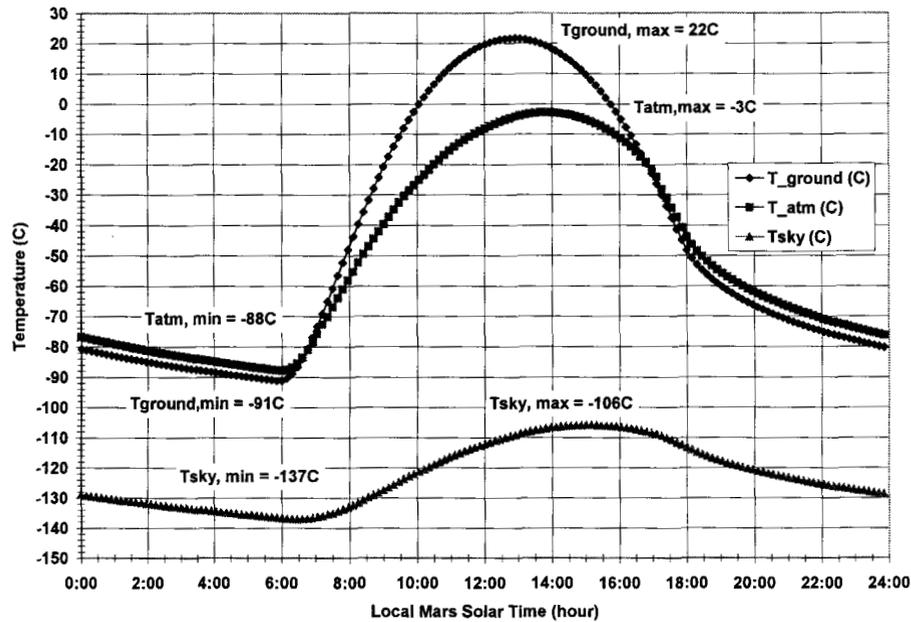
Thermal Design Drivers



- **Mars Surface Thermal Environment**
- **Hardware Temperature Limits**
- **Electrical Energy Usage Constraints**
- **High and Low Energy Operational Scenarios**



Mars Surface Environment



- Driven by landing site latitude (10°N to 15°S), time of year ($L_S = 328$ at BOM, $L_S = 30$ at EOM), ground albedo (0.12 to 0.25) and inertia (rock distribution), dust level ($\tau = 0.2$) in atm & elevation (-1.3km, MOLA)
- Global Circulation Model predicts ground, atmosphere & sky temps, solar insolation during day
- Wind speeds from Viking data (0 to 20 m/sec)



Hardware Temperature Limits



- **Temp Sensitive Hardware Located Inside WEB**
 - Li Ion secondary battery (-20°C/+30°C), charging at >0°C
 - Flight System Electronics (-40°C/+50°C)
 - Mini-TES Science instrument (-40°C/+45°C)

- **Temperature Robust External Hardware - 9 cameras & 34 actuators (-105°C/+50°C)**
 - Deployable Solar Arrays
 - Telecommunications antennas (High Gain, Low Gain, UHF)
 - Robotic arm with science sensors
 - Mobility system
 - Pancam Mast Assembly
 - Cameras (Optics and Electronics)



Power System Constraints & Operational Scenarios



- **Power System**

- 1.3 m² deployable solar array with triple-junction GaAs cells
- Two, 8 A*hr Li Ion rechargeable batteries
- 600 W*hrs electrical energy production per Sol
- Bus voltage maintained between 24V and 36V
- 120 W* hrs available for electrical heater power at night

- **Operational Scenarios**

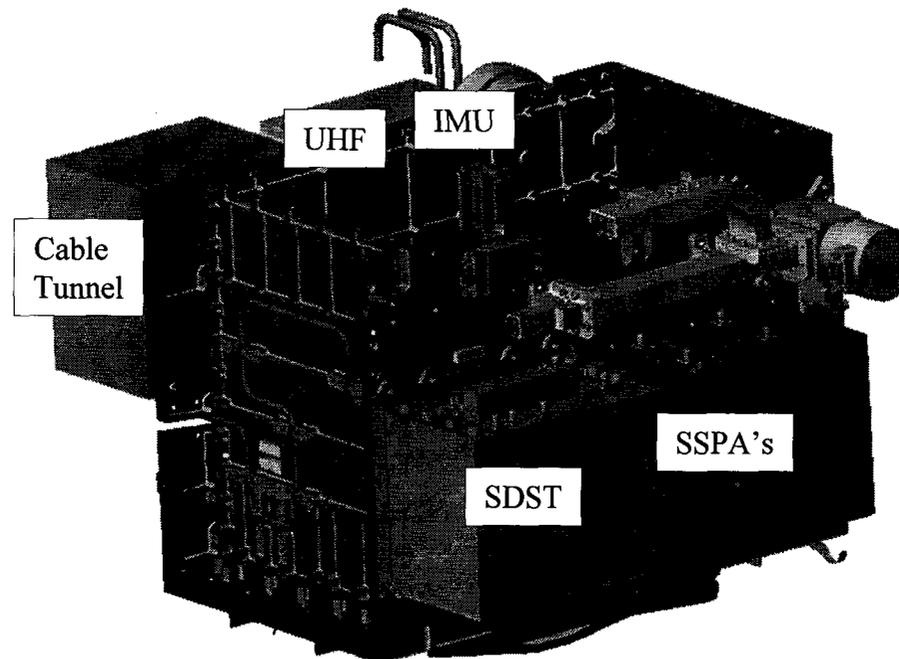
- Hot Case – maximum activity, early in mission, 4 hours of DTE comm, 716 W*hrs of dissipation in WEB (100W peak power)
- Cold Case – late in mission, minimum activity, charge batteries, 470 W*hrs of dissipation in WEB



Rover Internal Thermal Design



- **Maximize Thermal Time Constant** ($\tau = R * C$)
 - Minimize temperature increases driven by internal dissipation profiles and temperature decreases driven by external diurnal environment
 - **Maximize thermal capacitance (C)**
 - Concentrate thermal mass in WEB (36kg) by coupling together
 - Allow power sharing



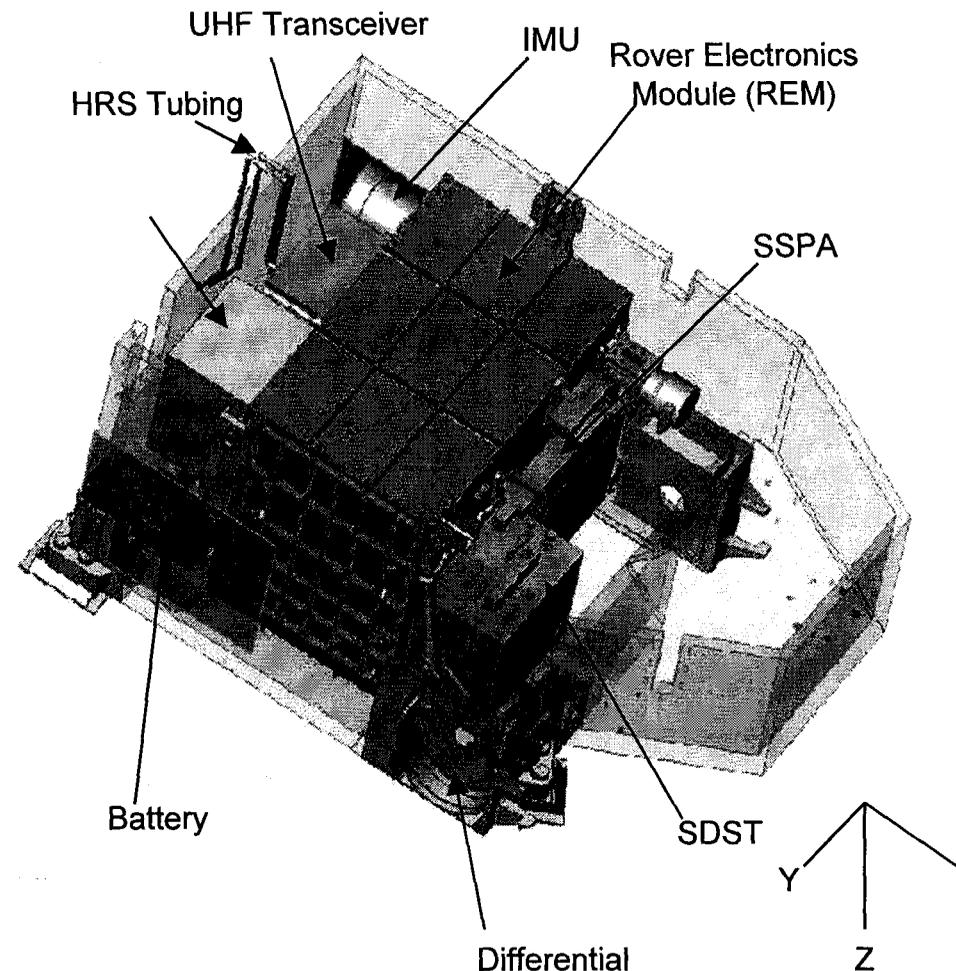


Rover Internal Thermal Design



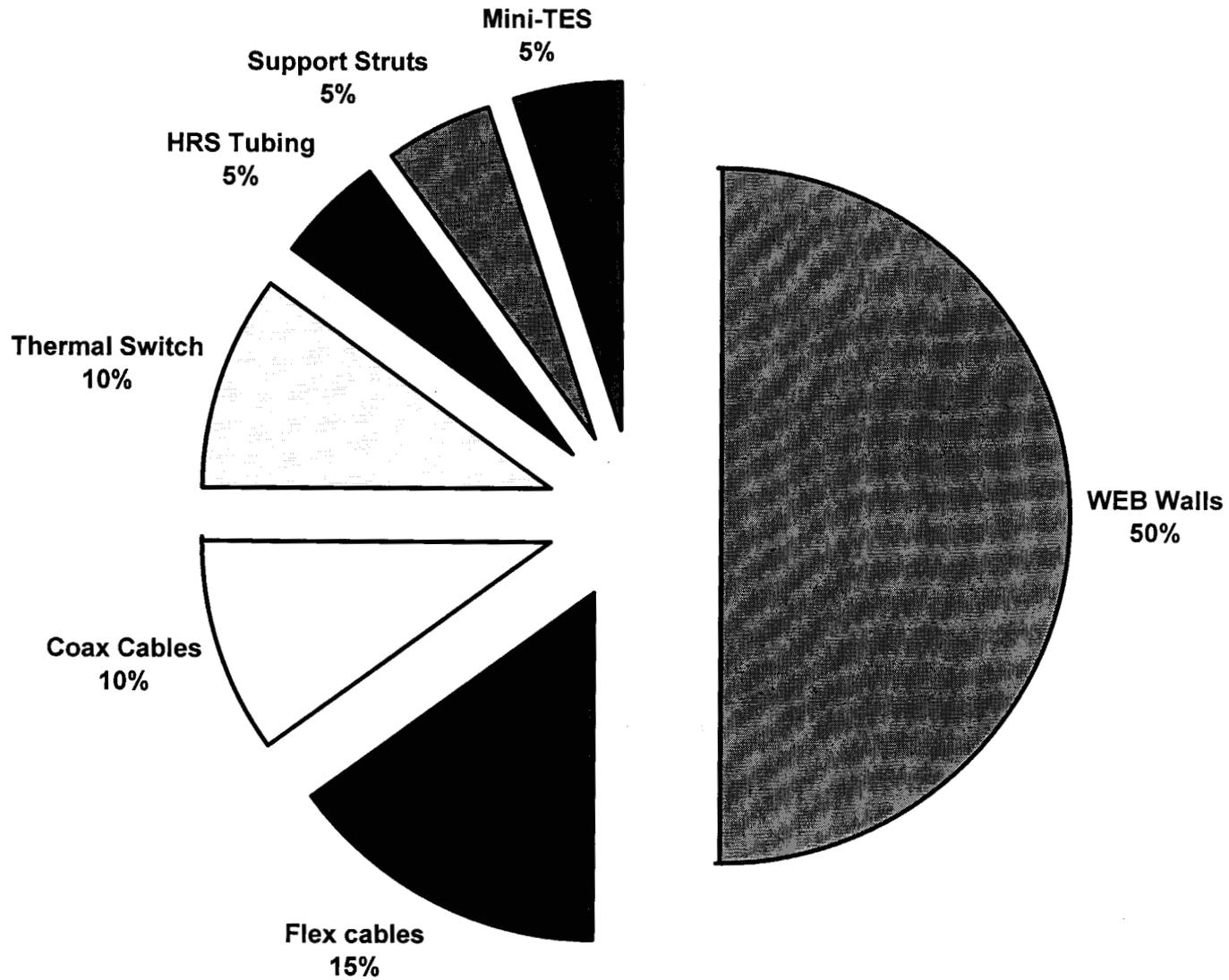
- **Maximize WEB thermal resistance (R) to environment**

- Carbon-opacified aerogel insulation ($k=0.012 \text{ W/m}^*\text{K}$)
- Low emissivity gold internal & external surfaces
- Flex cables with lower copper cross-section
- Cable tunnels for flex & coax
- Battery thermal switches open when battery is cold
- Stainless steel section of HRS tubing at egress
- Low conductivity boron-epoxy tubes support H/W





Heat Leaks from WEB





Web Thermal Hardware



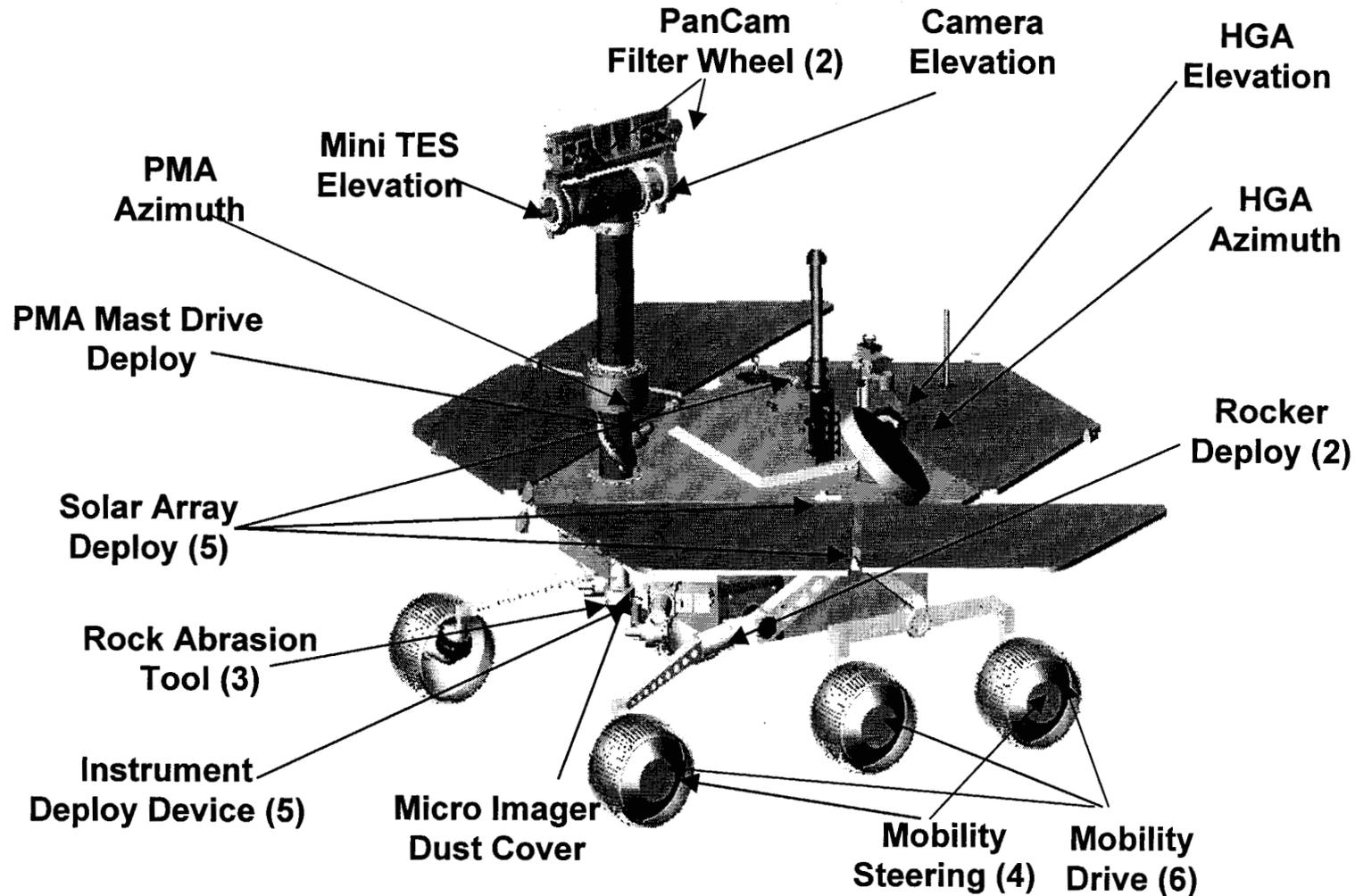
- **Survival heaters on REM, Battery & Mini-TES**
 - Controlled by mech t'stats
 - Operate when flight computer is OFF
- **Warmup Heater on Battery**
 - Controlled by mech t'stats
 - Warmup to optimal charging temp (0°C)
- **Radioisotope Heater Units (RHU's) on REM (2) and Battery (6)**
 - Dissipate 1.0 W each
 - Non-electrical heat source; cannot be turned off
- **Paraffin-actuated thermal switches between battery & radiator**
 - Close when battery temp $> 20^{\circ}\text{C}$ ($G=1.0 \text{ W}/^{\circ}\text{C}$)
 - Open when battery temp $< 18^{\circ}\text{C}$ ($G=0.017 \text{ W}/^{\circ}\text{C}$)



Rover External Thermal Design



- 34 Actuators on Outside of Rover

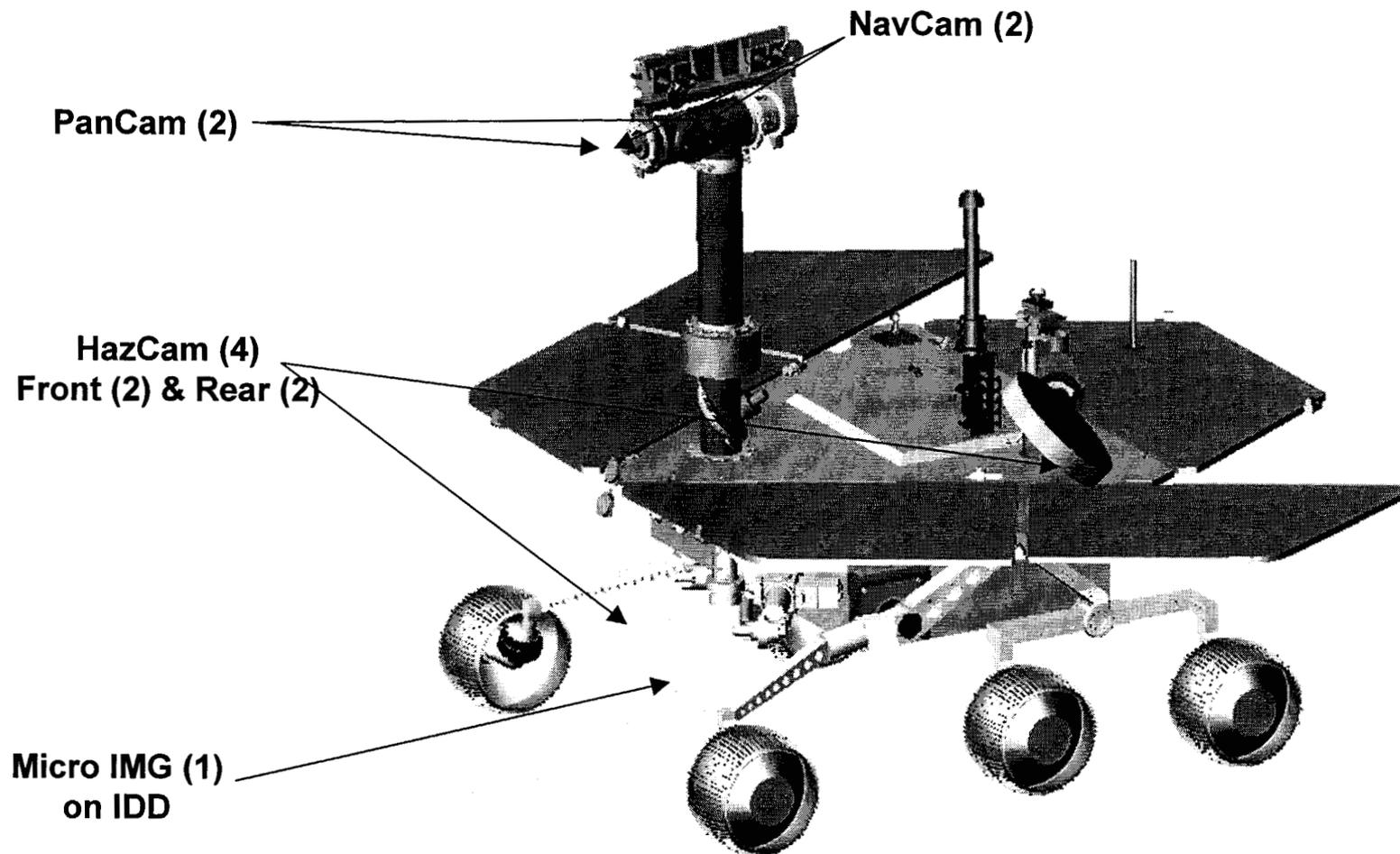




Rover External Thermal Design



- 9 Cameras on Outside of Rover





External Thermal Hardware



- **No survival heaters necessary**
- **Warmup Heaters (to -55°C min op temp)**
 - On all actuators (motors, gearboxes, bearings, harmonic drives)
 - Concern is viscosity of Braycote lubricant at cold temps
 - On all camera electronics boards
 - Allow early morning operations
- **Low a/e coatings**
 - Minimize effect of solar insolation
 - White paint on PMA mast
 - Silvered teflon on motors and gearboxes
 - Silvered teflon on camera electronics housings



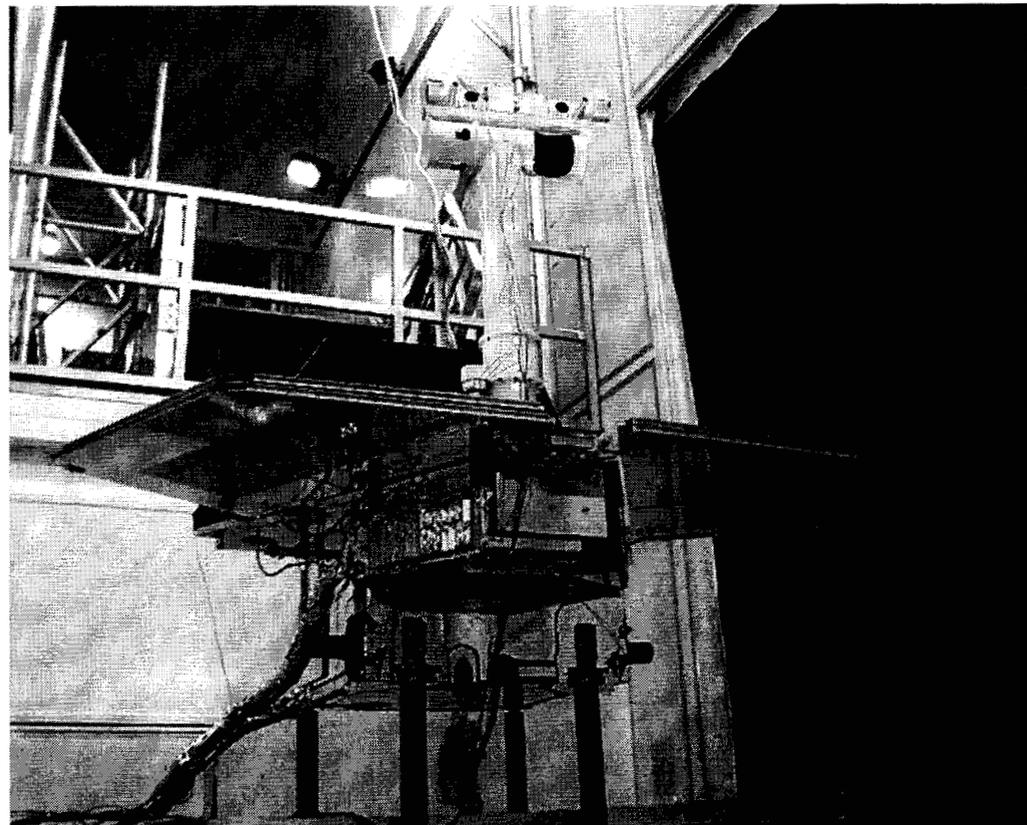
Engineering Model Thermal Testing



- Design validation in Mars environment done by analysis
 - Direct empirical validation is very difficult on Earth
- Thermal testing used to obtain data needed to correlate analytical models

Thermal Test of
Engineering Model Hardware
May 2002

- Derive thermal resistance values from steady state tests
- Derive thermal capacitance values from diurnal transient tests





Thermal Testing

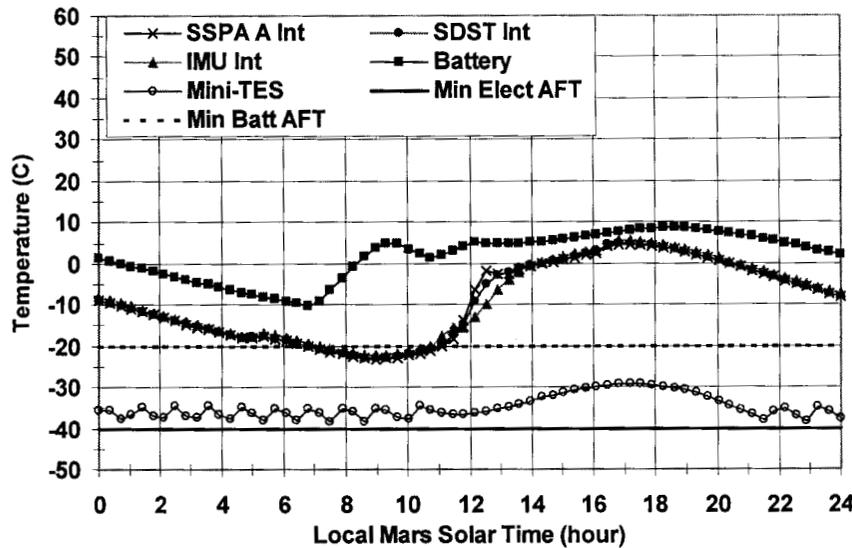


- Comparison of Mars Environment and Chamber Environment

Environment	Mars	Chamber
Atmosphere	8 torr CO ₂	8 torr GN ₂
Gravitational Acceleration	3/8 G	1 G
Solar Insolation	Up to 600 W/m ²	none
Boundary Temperatures	$T_{\text{sky}} = -140^{\circ}\text{C to } -105^{\circ}\text{C}$ $T_{\text{atm}} = -95^{\circ}\text{C to } 0^{\circ}\text{C}$ $T_{\text{ground}} = -100^{\circ}\text{C to } 20^{\circ}\text{C}$	$T_{\text{sky}} = -95^{\circ}\text{C to } 0^{\circ}\text{C}$ $T_{\text{atm}} = -95^{\circ}\text{C to } 0^{\circ}\text{C}$ $T_{\text{ground}} = -100^{\circ}\text{C to } 20^{\circ}\text{C}$
Wind Speed	0 to 20 m/sec	None, free convection only

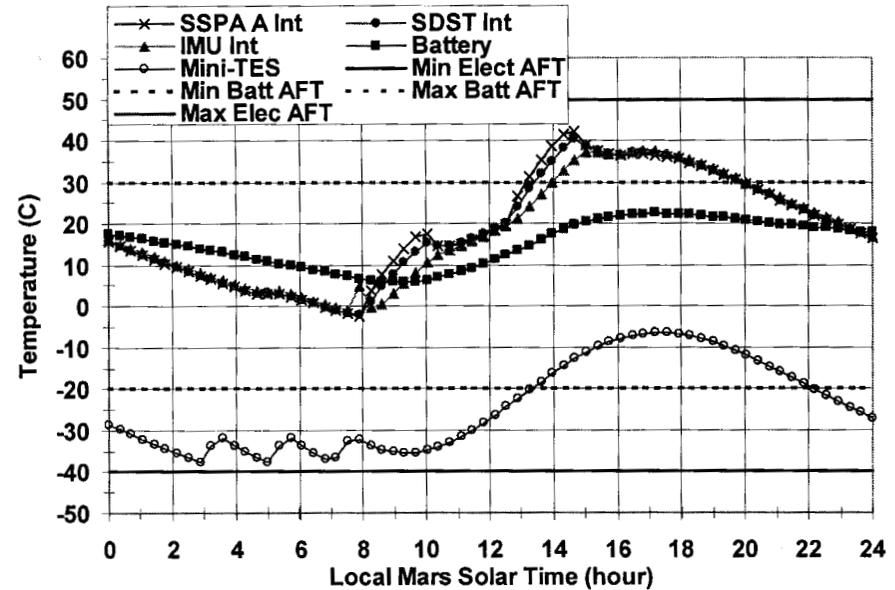


Correlated Thermal Model Predictions



Cold Case Results

Low Energy Scenario (470 W*hrs)
 Mini-TES survival heater on at night
 Battery warmup heater on in AM
 Nighttime energy usage 65 W*hrs
 (well under max allowable of 120 W*hrs)



Hot Case Results

High Energy Scenario (716 W*hrs)
 SSPA on for 4 hours
 (exceeds requirement by 1 hour)
 Max SSPA temp = 44C
 (under max allowable of 50C)
 Max Battery temp = 22C
 (under max allowable of 30C)



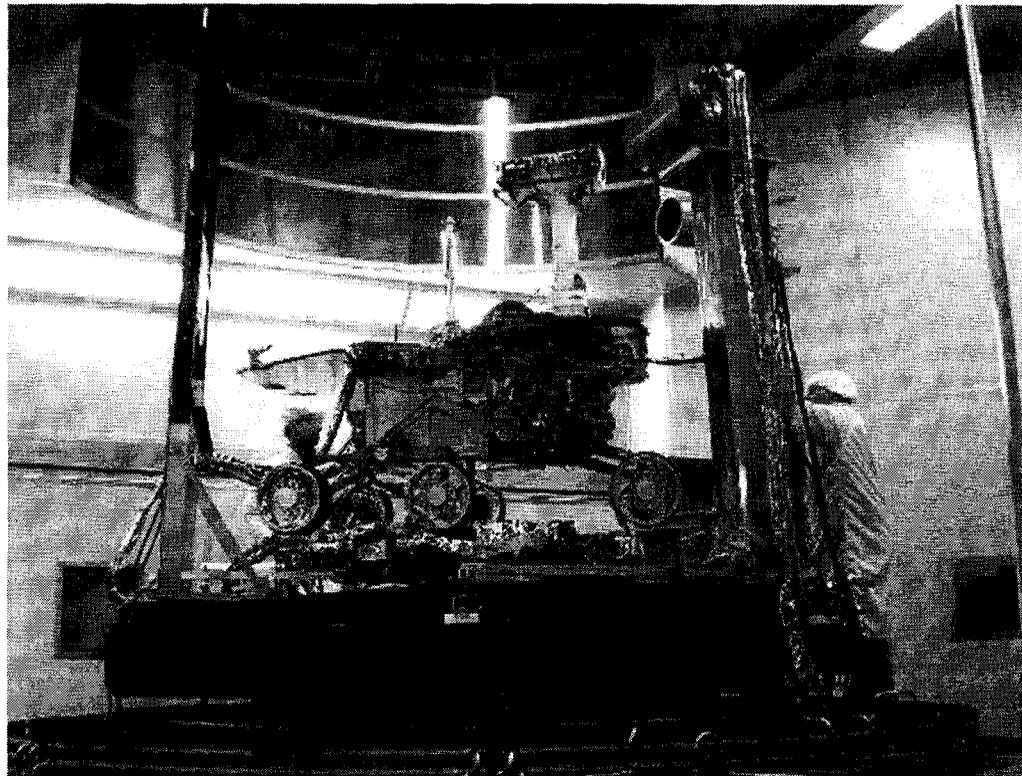
Flight Model Thermal Testing



- Preliminary design validation in Mars environment done by comparison to previous EM test data
 - Followed up by model correlation
- Correlated models to be used in operations to predict Mars surface performance

Thermal Test of
Flight Model Hardware
Dec. 2002

- Compare steady state and transient results to previous EM test
- Generate warmup heater characterization data





Conclusion & Status

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System Level Thermal Design

- Exceeds performance requirements
- Requires low night heater energy
- Allows 4 hours of communications
- Highly successful design

Current project status

- Thermal test of 2nd rover in Feb. 2003
- First launch May 30, 2003
- First landing Jan 4, 2004



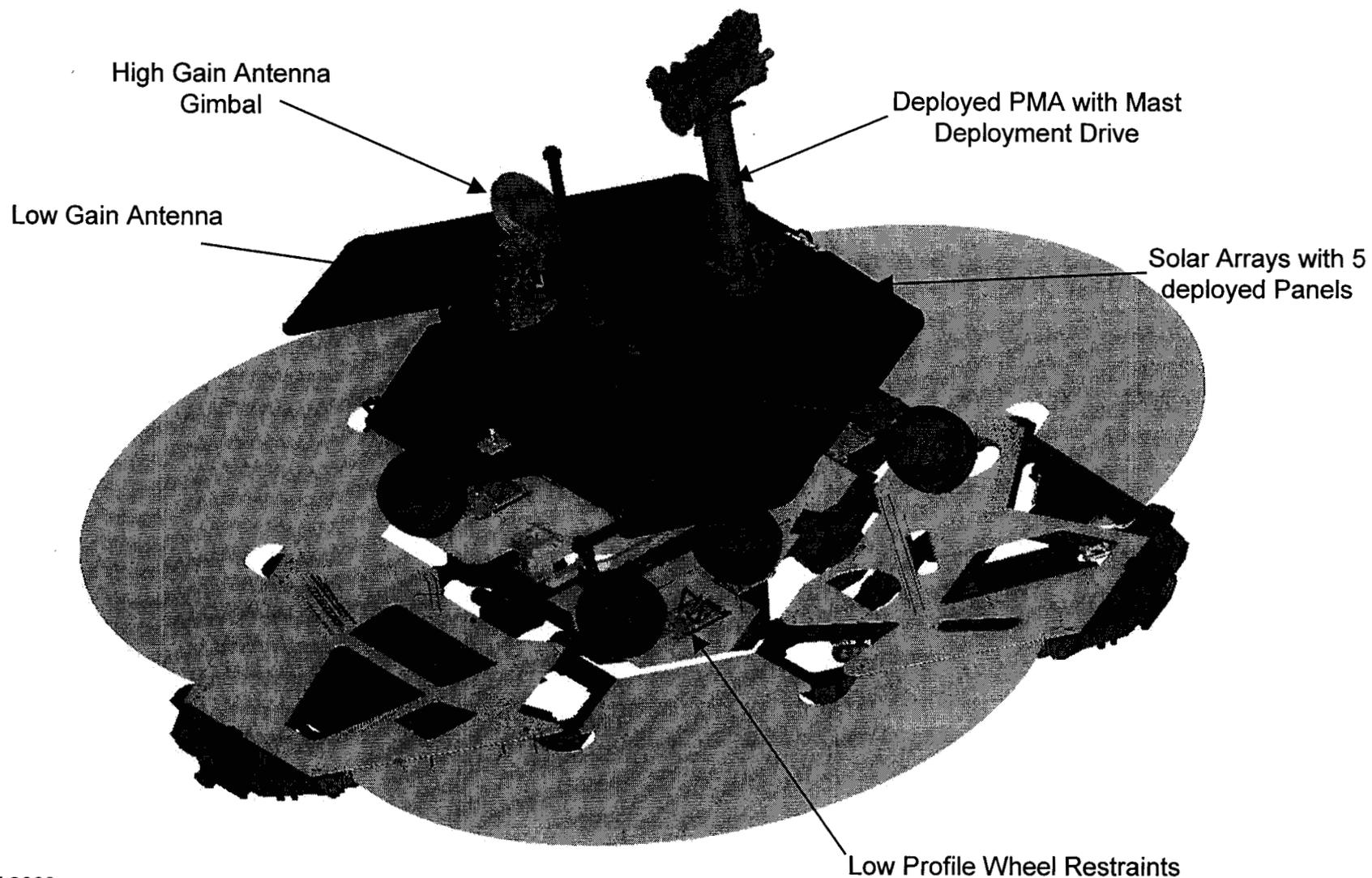


Backup Slides





I. Rover Configuration - Deployed on Lander

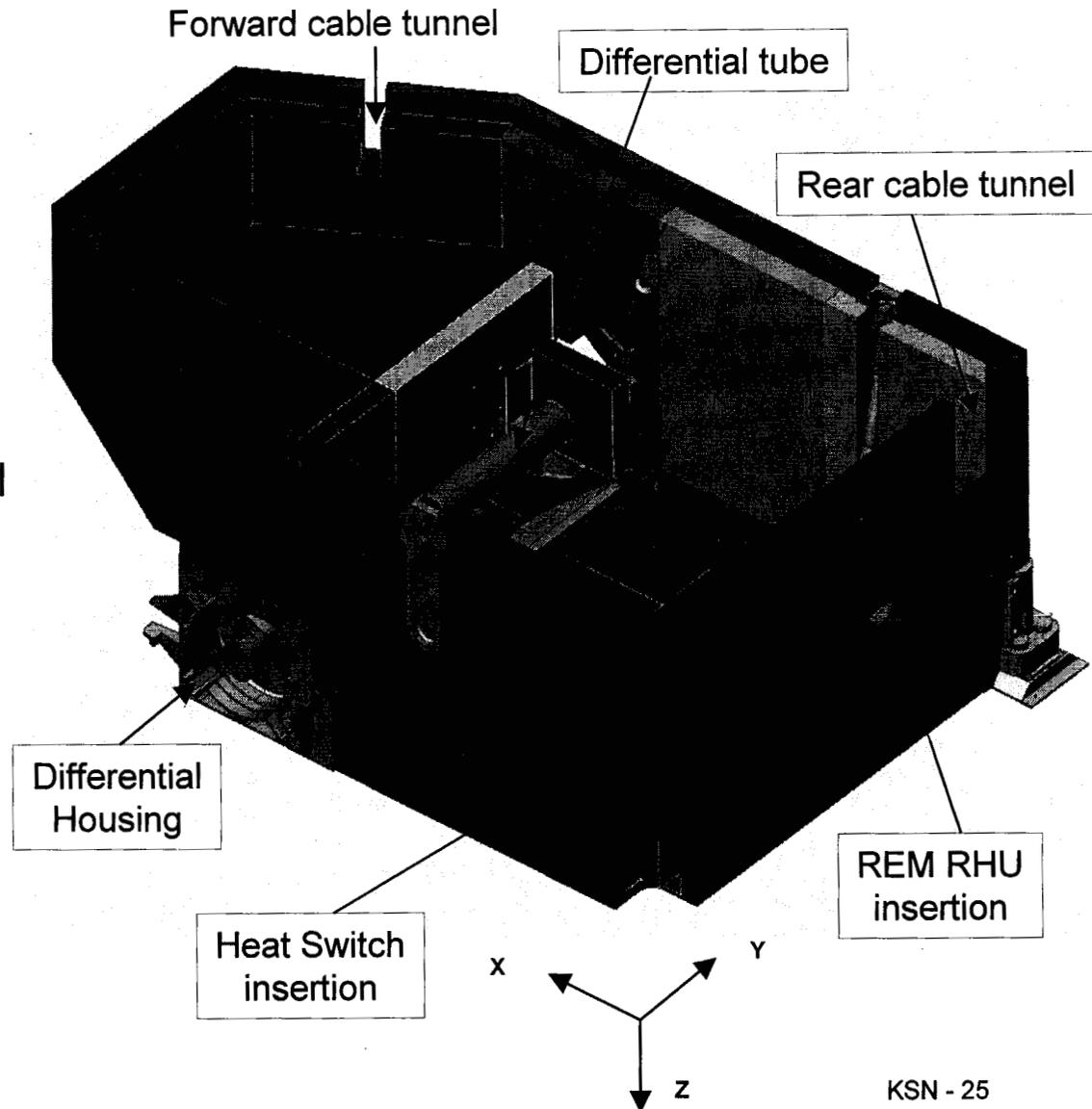




III. Thermal Design Approach - Exoskeleton WEB w/ Aerogel



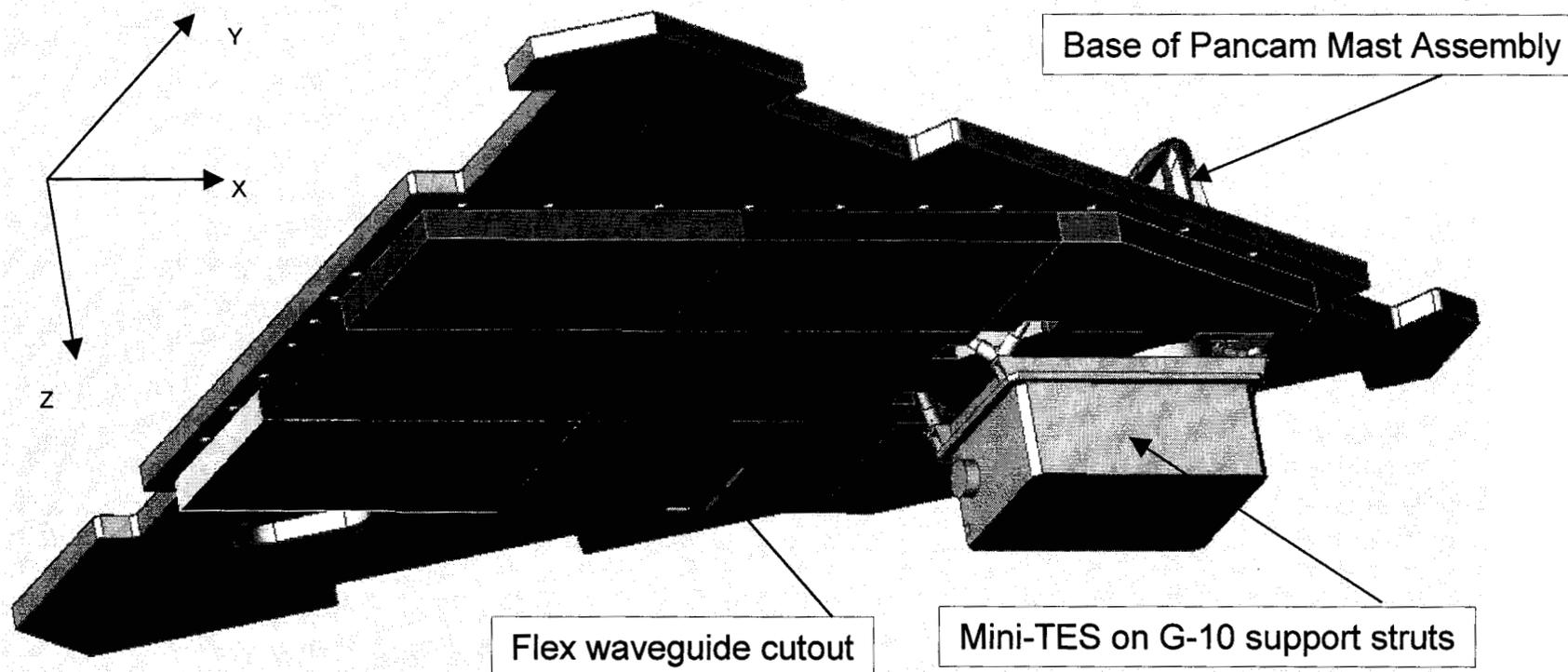
- 1mm thick M55J Carbon composite facesheets
- over 3.1 lb/ft³ 5056 Al H/C core, 13mm thick side walls, 8 mm thick on bottom wall
- 25 mm of carbon-opacified solid aerogel insulation on all walls except +Z (20mm)
- significant cutouts (6% of area) in aerogel for struts, fittings, cable tunnels, RHU insertion, heat switches
- 0.012" thick Astroquartz composite faceskin closeout on local 0.020" thick "Z" spars





III. Thermal Design Approach - RED w/ Aerogel & REM w/ Struts

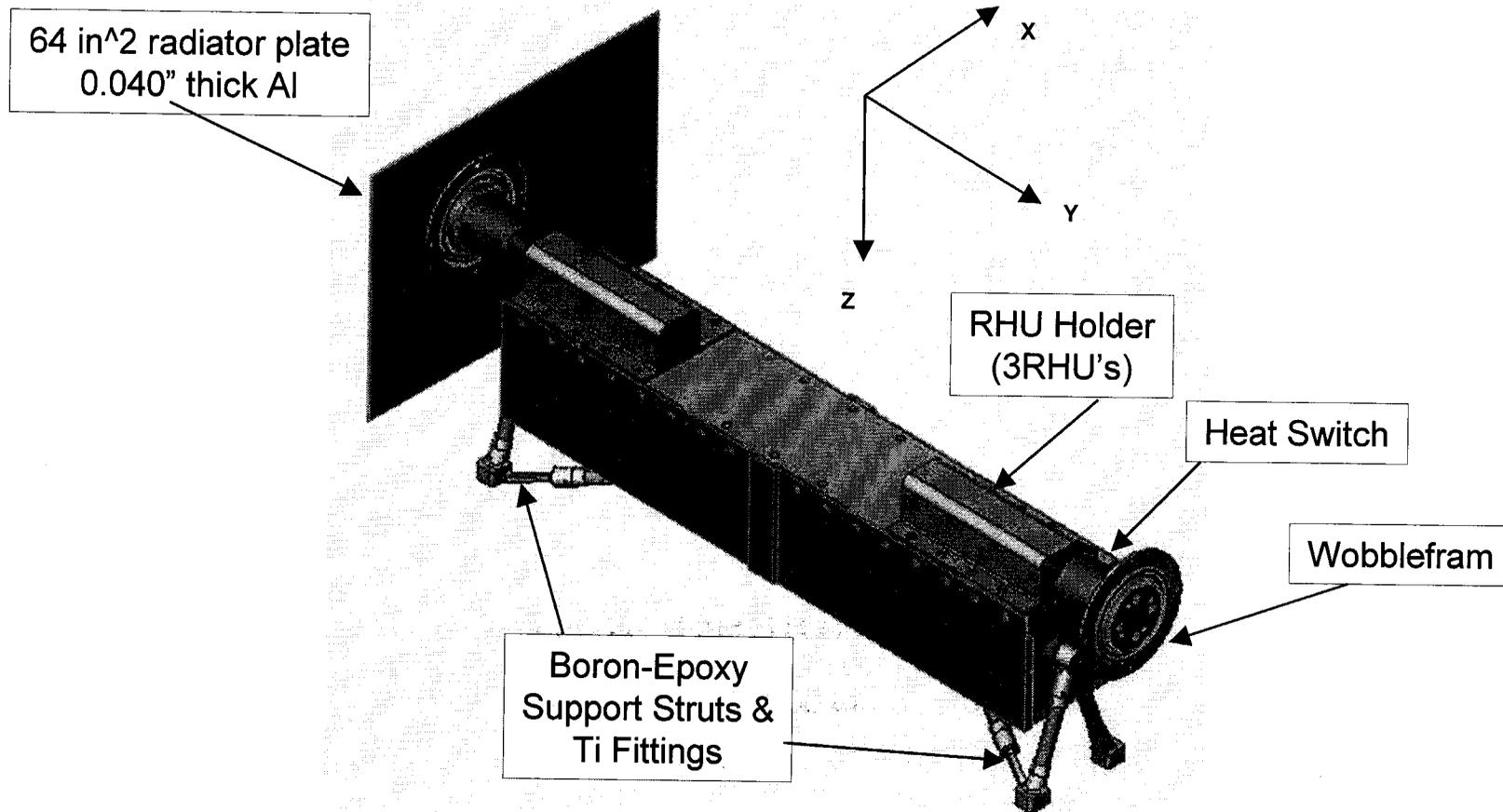
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- 25mm thick carbon-opacified aerogel
- Cutouts for MTES telescope & LGA flex waveguide



III. Thermal Design Approach - Battery Mounted on Struts



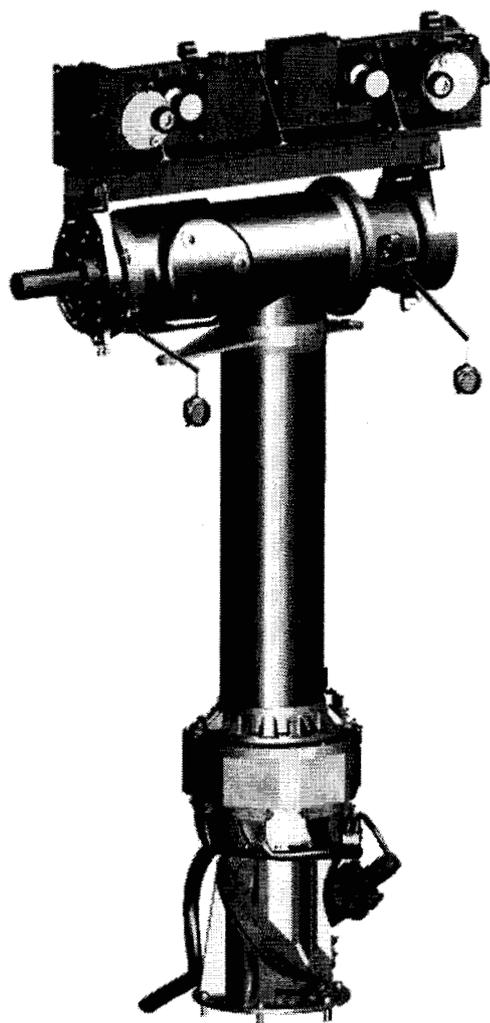


TGMM Description

PMA Cameras Configurations



Configuration 2: Hot
(45 Deg.)



Configuration 3: Cold

