

Advanced Dynamic Simulation of Lid-Latch Mechanisms under Impact Loading

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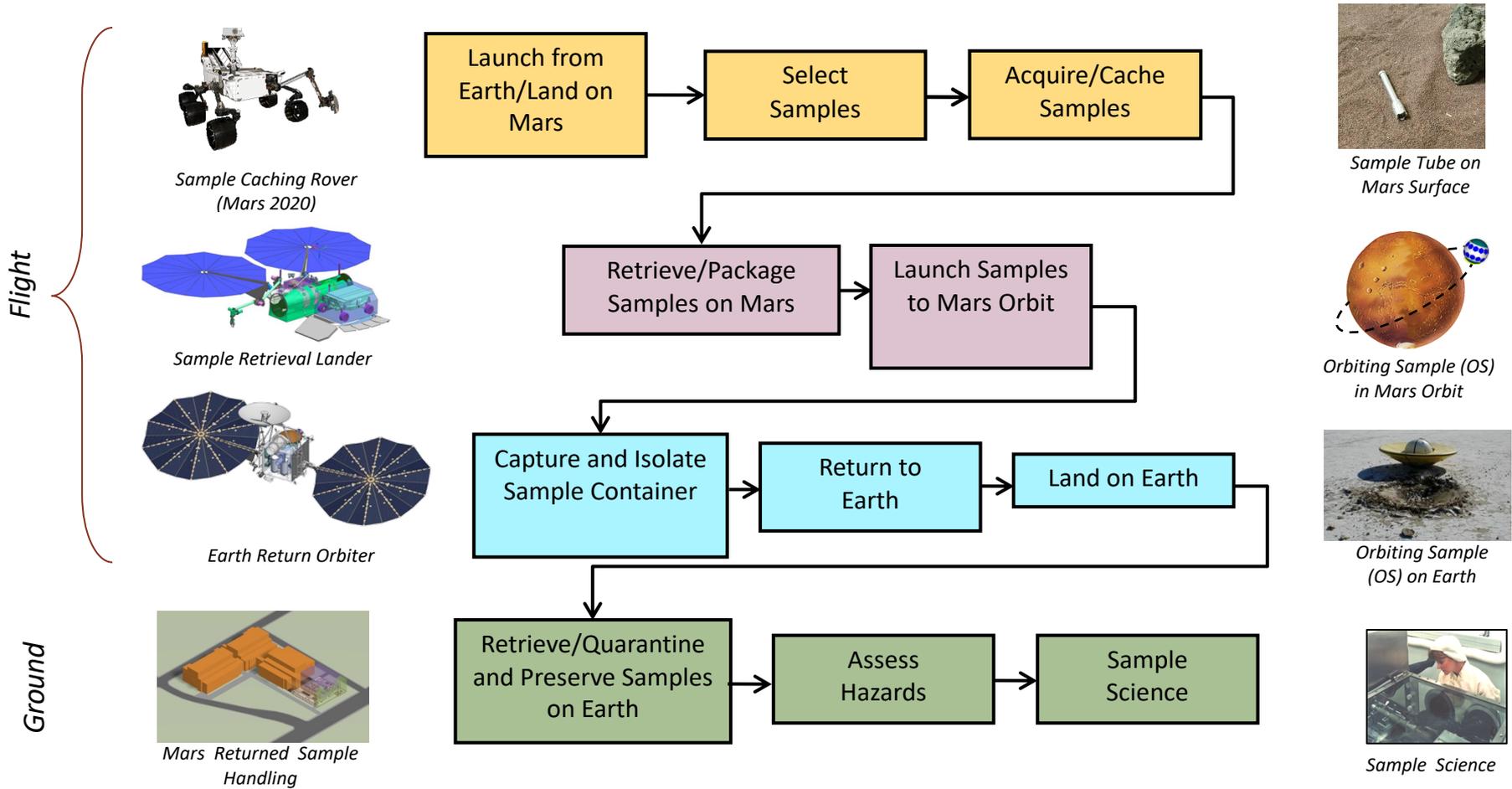
2019 Spacecraft Launch Vehicle
Dynamic Environments Workshop

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- Notional Mars Sample Return (MSR) Campaign Architecture Overview
- MSR Earth Entry Vehicle (EEV) Concept Overview
- MSR Containment Assurance Scheme
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 - Load environment and implementation
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 - LS-DYNA Analysis Examples
 - Single pawl studies
 - Piece-Part Studies of Secondary Containment Vessel (SCV)
 - Progress towards integrated, system-level model

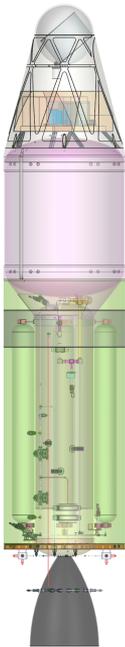
Notional Mars Sample Return (MSR) Campaign Overview



Notional MSR Key Elements of Interest

Sample Retrieval Lander

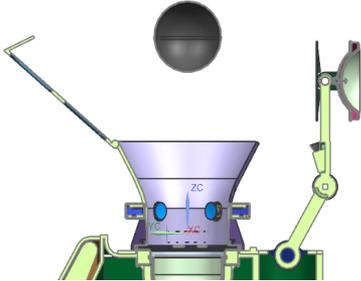
Earth Return Orbiter



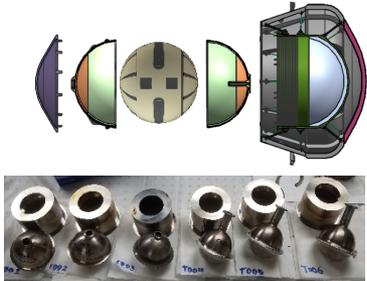
Mars Ascent Vehicle



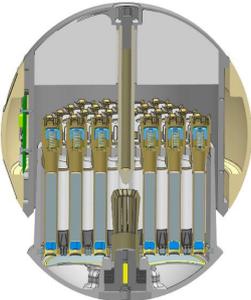
Sample Fetch Rover



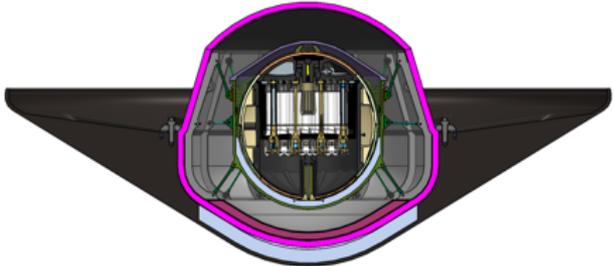
Rendezvous and Capture



Containment Assurance

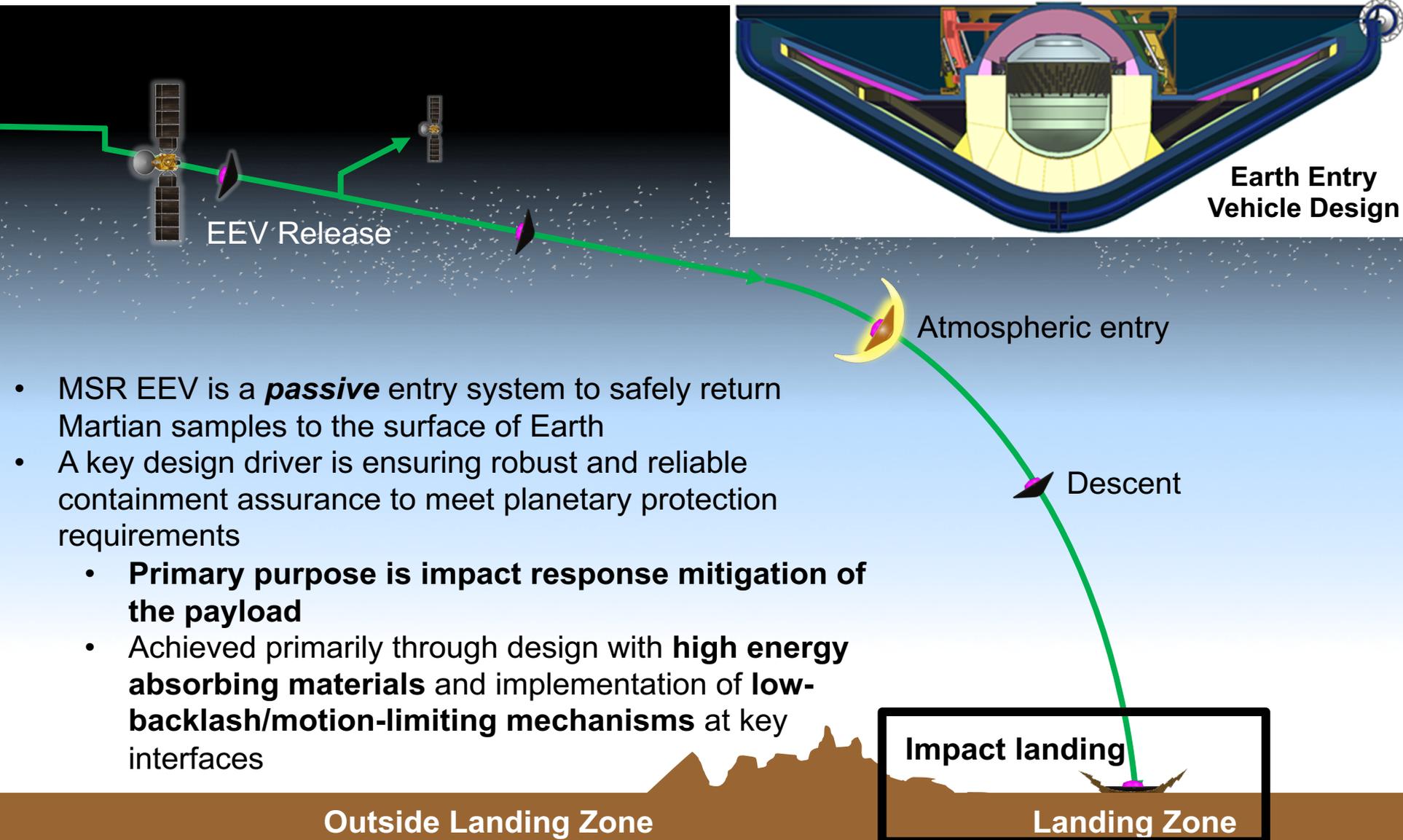


Orbiting Sample (OS) Container



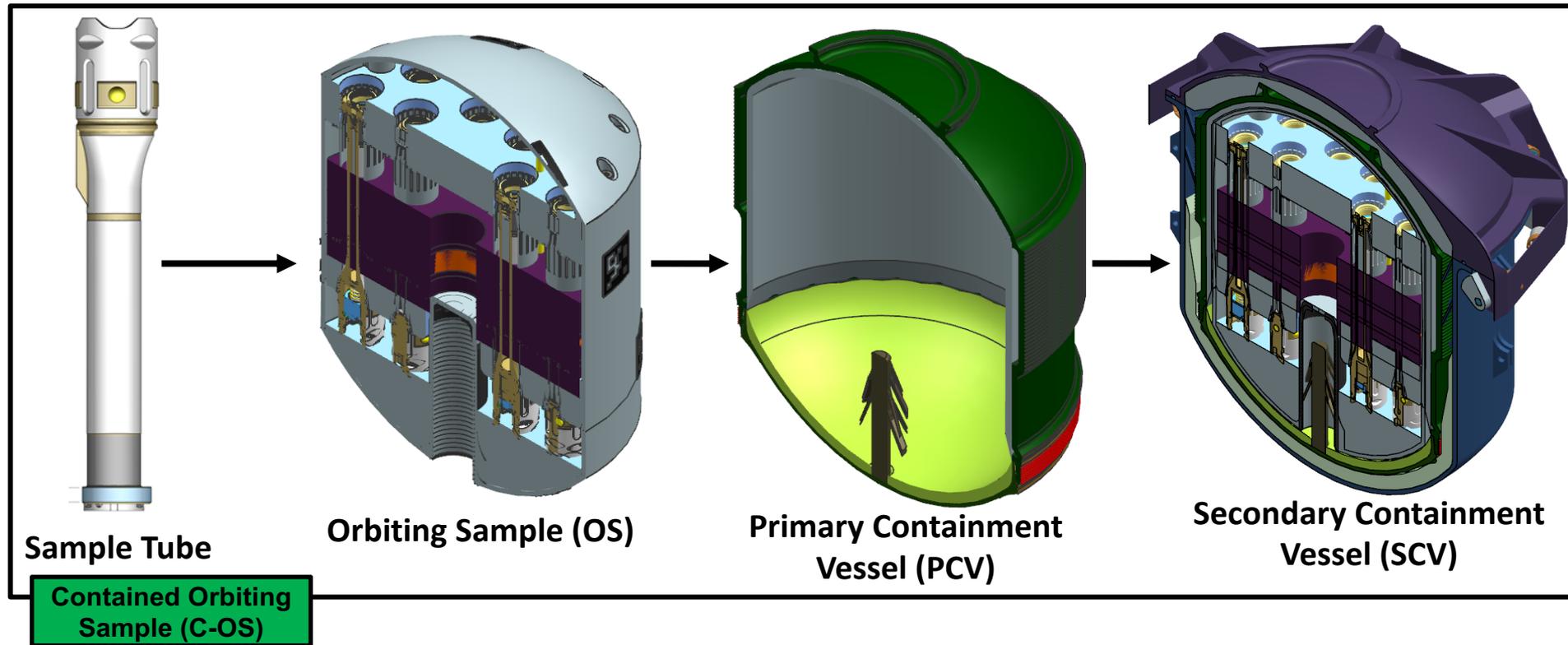
Earth Entry Vehicle

MSR Earth Entry Vehicle (EEV) Concept Overview



- MSR EEV is a **passive** entry system to safely return Martian samples to the surface of Earth
- A key design driver is ensuring robust and reliable containment assurance to meet planetary protection requirements
 - **Primary purpose is impact response mitigation of the payload**
 - Achieved primarily through design with **high energy absorbing materials** and implementation of **low-backlash/motion-limiting mechanisms** at key interfaces

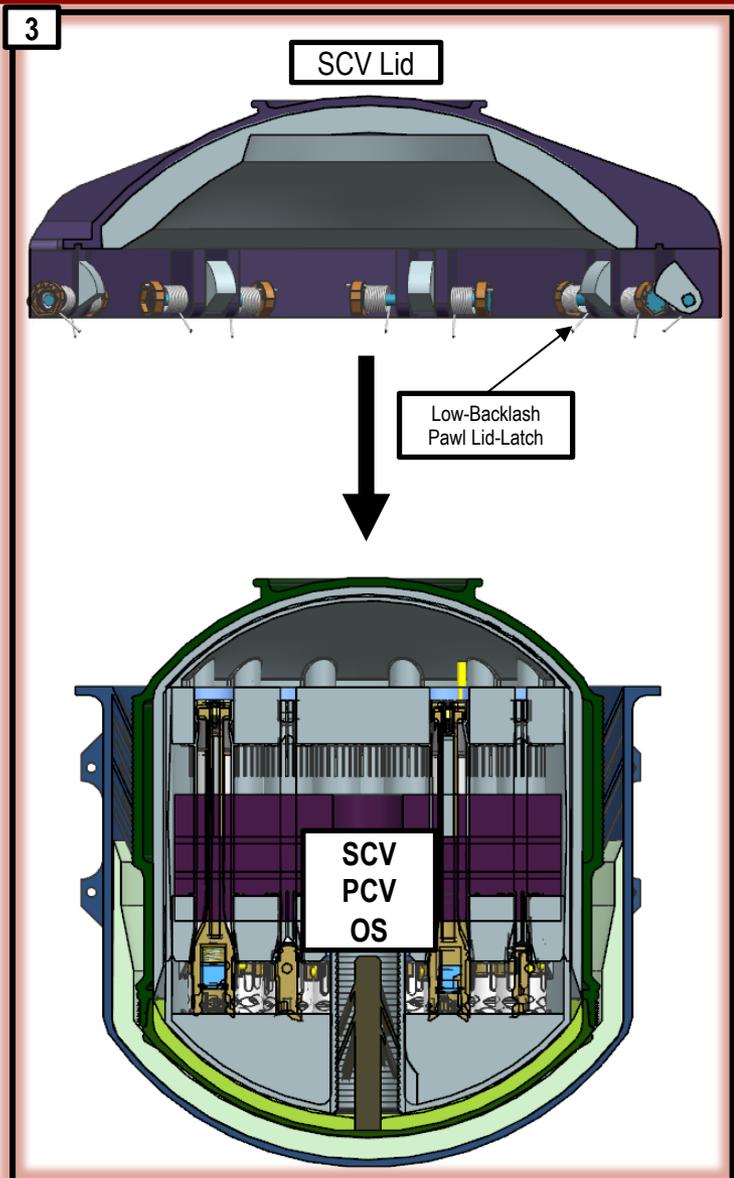
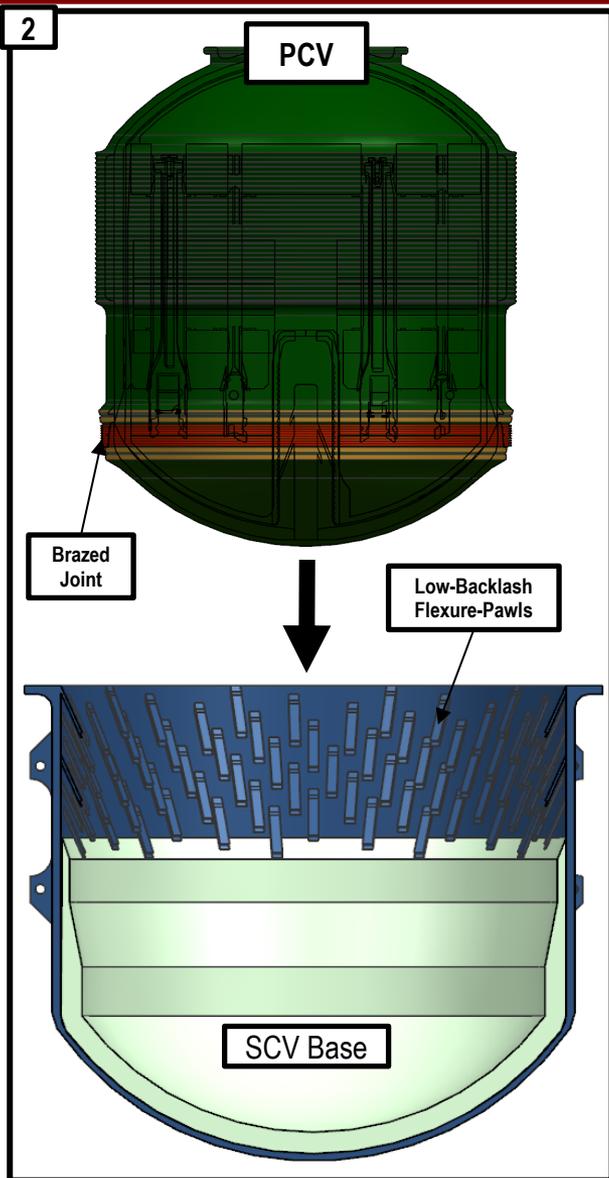
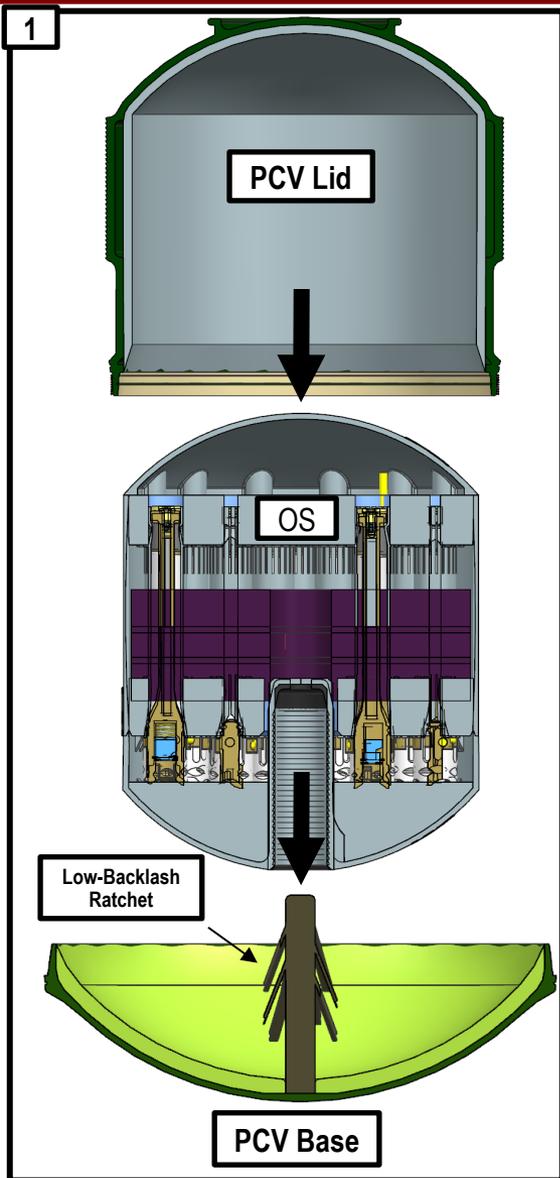
MSR Contained Orbiting Sample (C-OS)



The Contained-OS is composed of: the (1) Orbiting Sample (OS), the (2) Primary Containment Vessel (PCV), and (3) Secondary Containment Vessel (SCV)

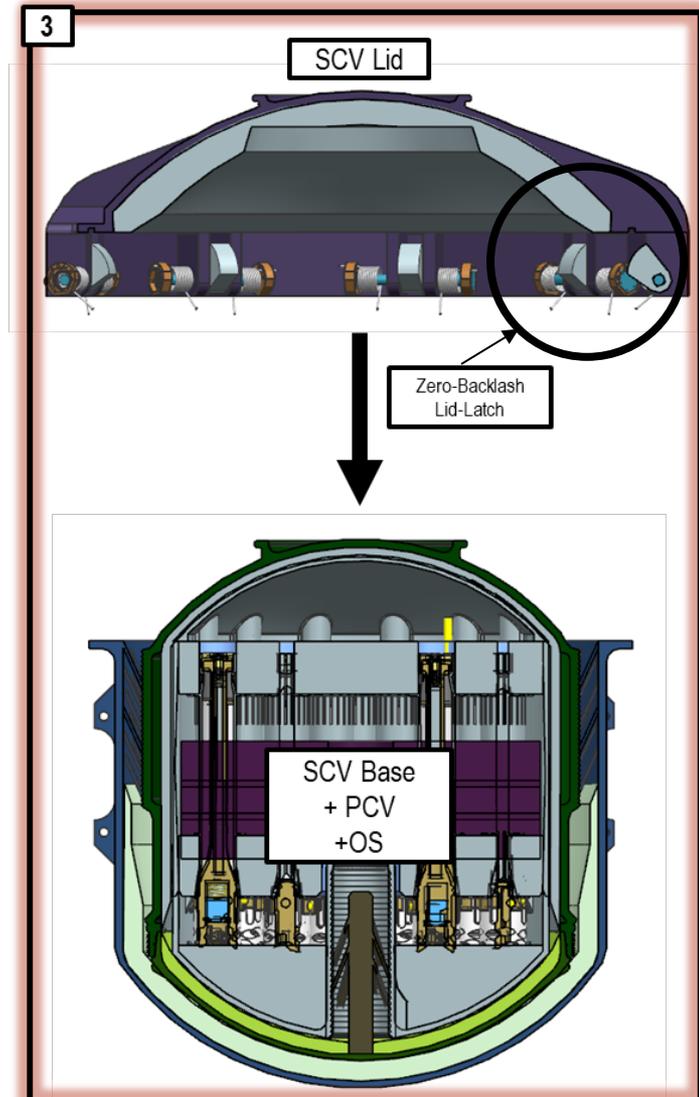
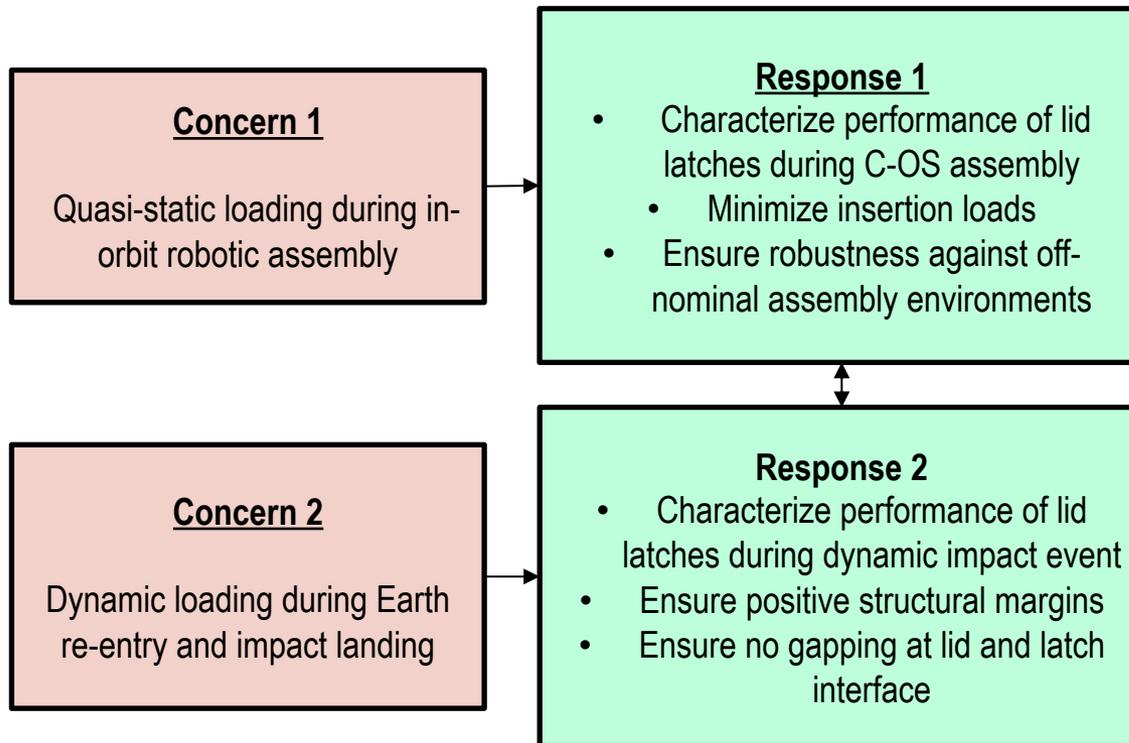
The **goal of the C-OS** is to provide returned samples with a “**redundant, fail-safe containment**” methodology able to survive Earth entry, descent, and impact landing - EEV required to provide majority of impact response mitigation during landing

Contained-OS Assembly Procedure

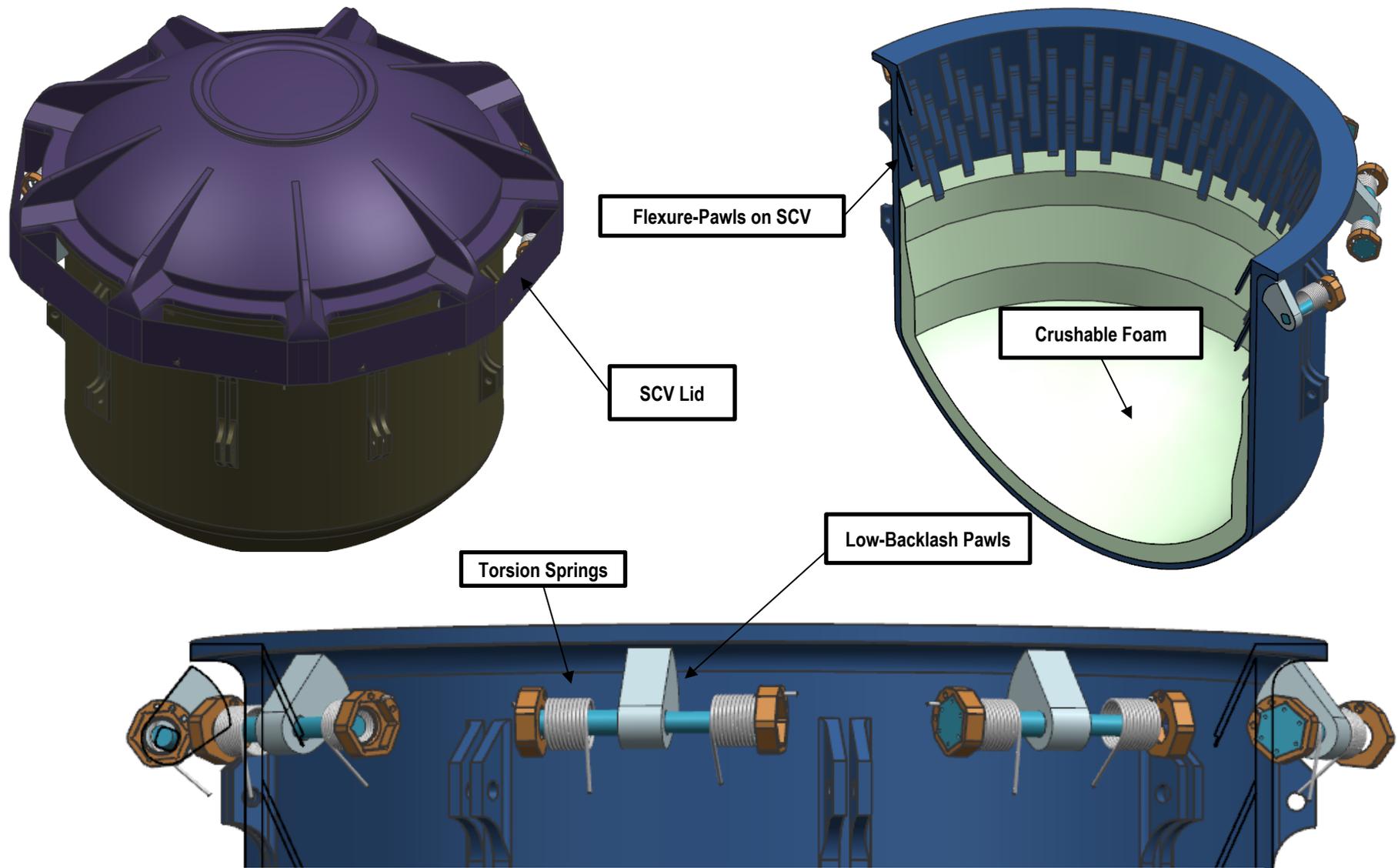


Interface Currently under Study

- Containment not assured when PCV and SCV:
 - Suffer overt structural failure (e.g. container cracks)
 - Gap/fail their seals
 - Due to deflection of the lid and/or base
 - Due to failure of the latch/closure system
- Believe that Containment Assurance currently **driven by failure of the latch system for SCV**



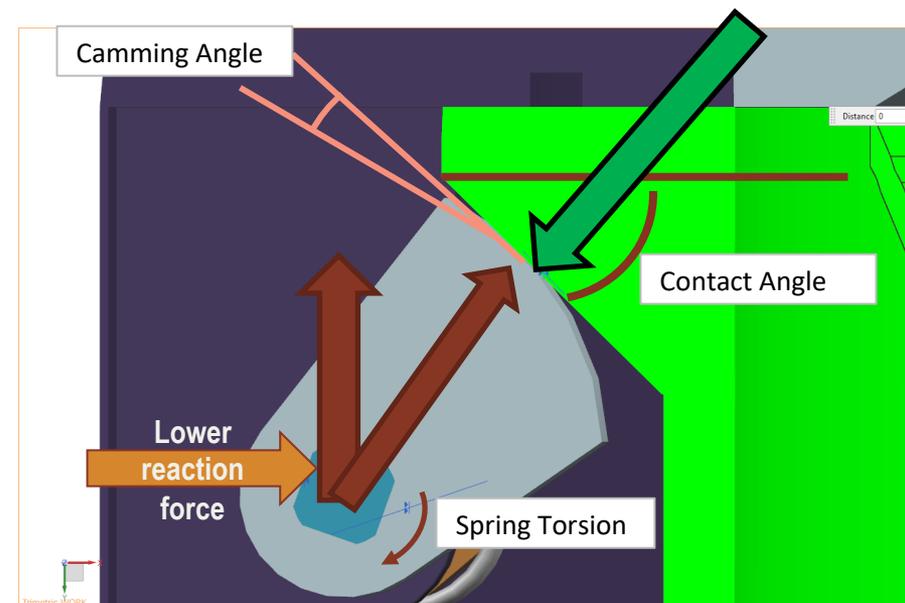
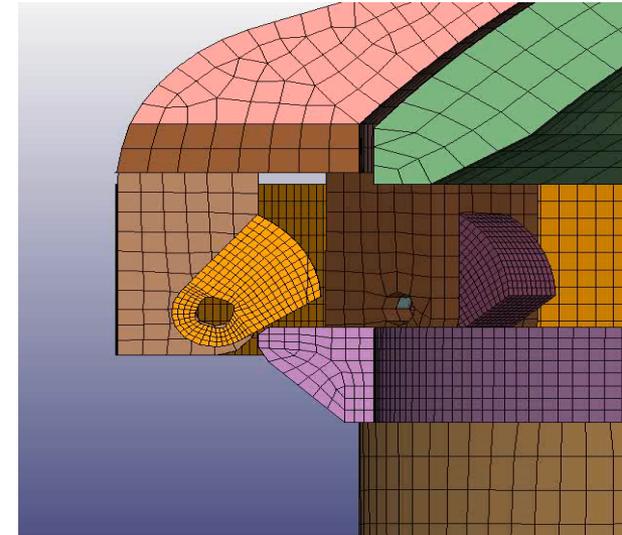
SCV Lid Latch Interface Details



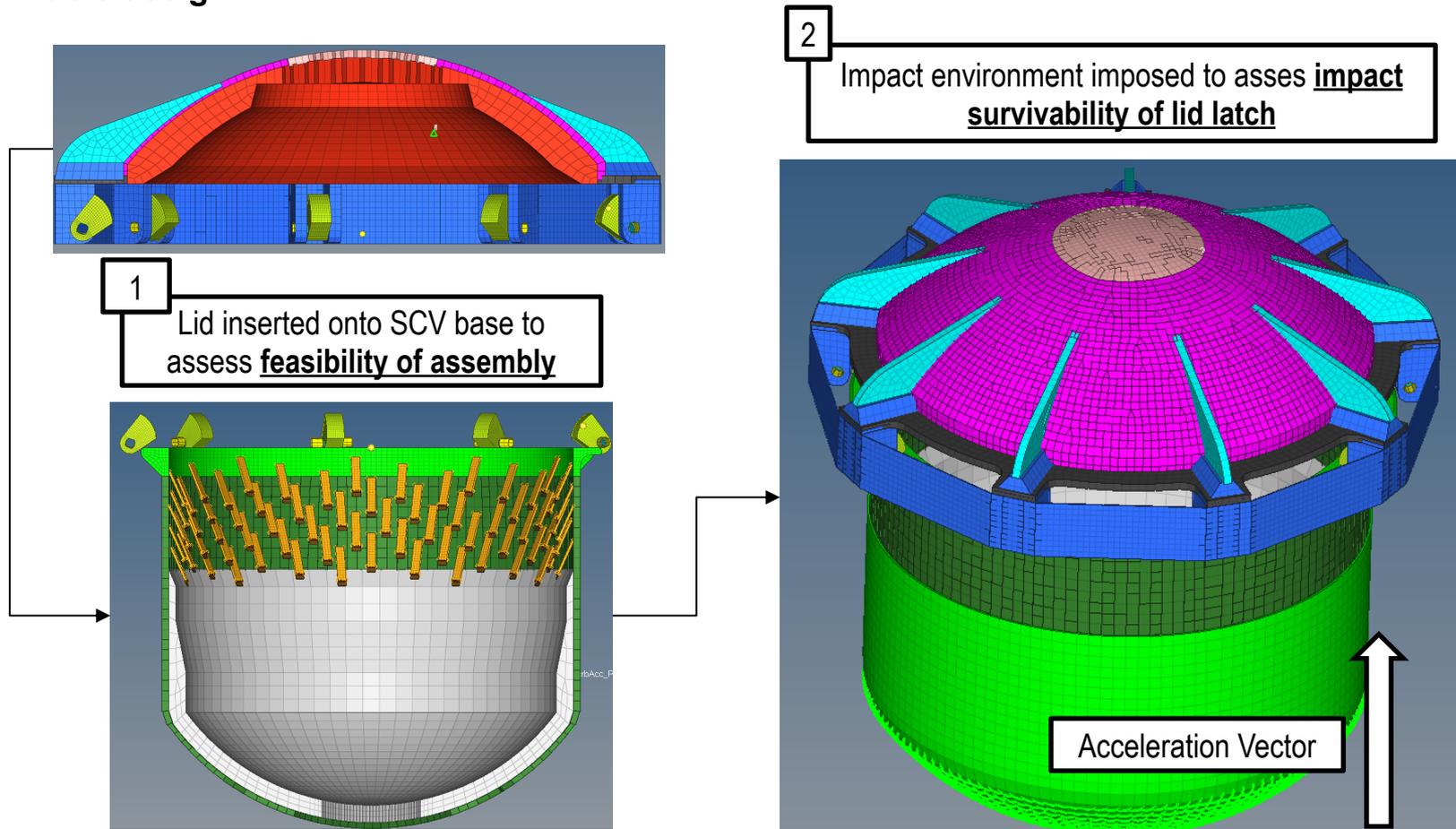
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SCV Pawl Lid-Latch Design

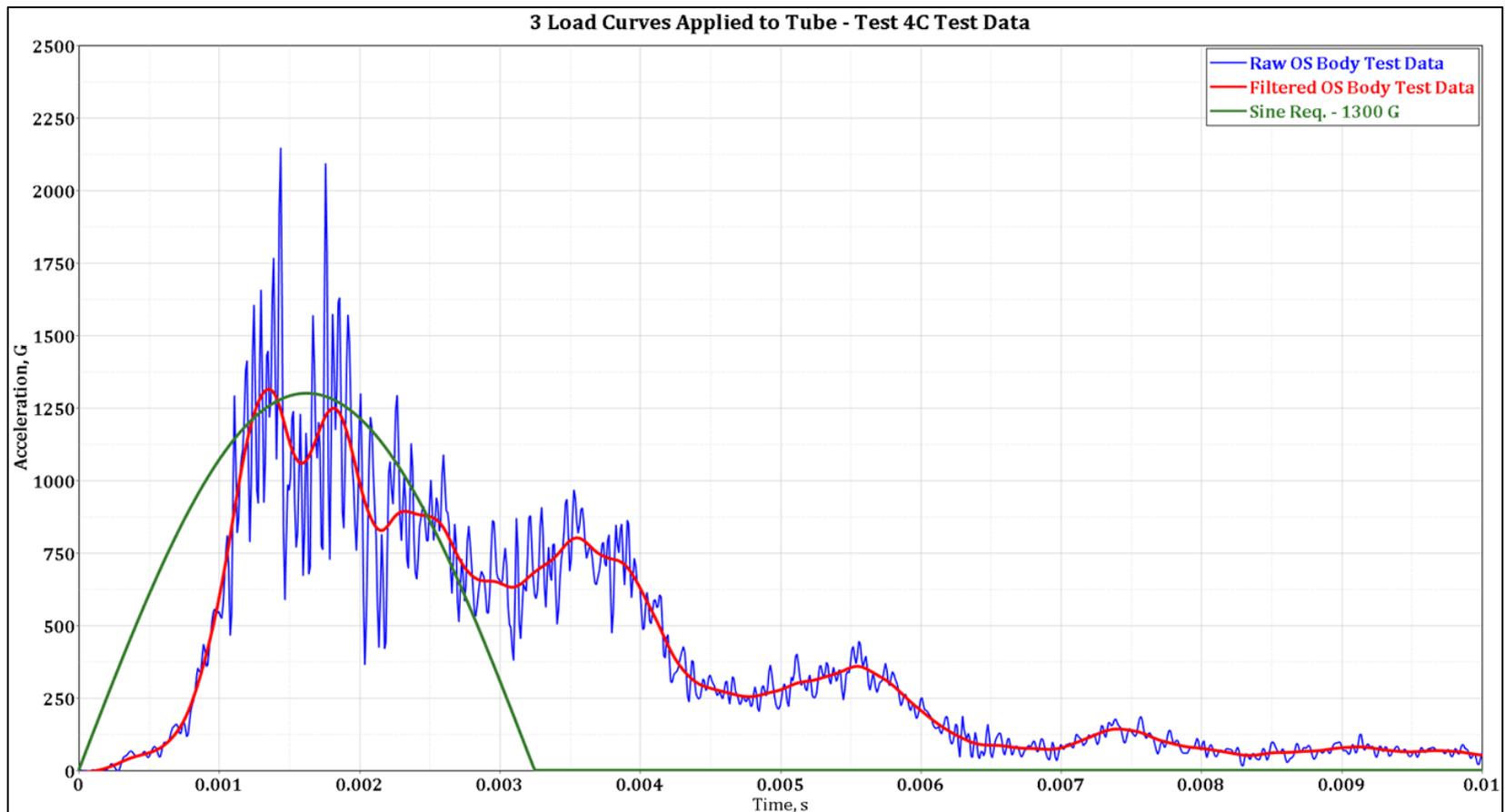
- Lid-latch is based off of a low-backlash pawl design
 - Used on MSL Remote Sensing Mast and SMAP Solar Array
- The logarithmic cam profile - prevents backlash in an impact event
 - Entry/impact forces will push lid closed, resulting in increased latch engagement
 - Torsional springs help to drive engagement
- Latch requires (very low) friction to remain engaged
- Radial forces must be reacted - overhang surface to reduce both reaction loads and contact stresses
- Success in quasi-static environment – not yet characterized in impact environment



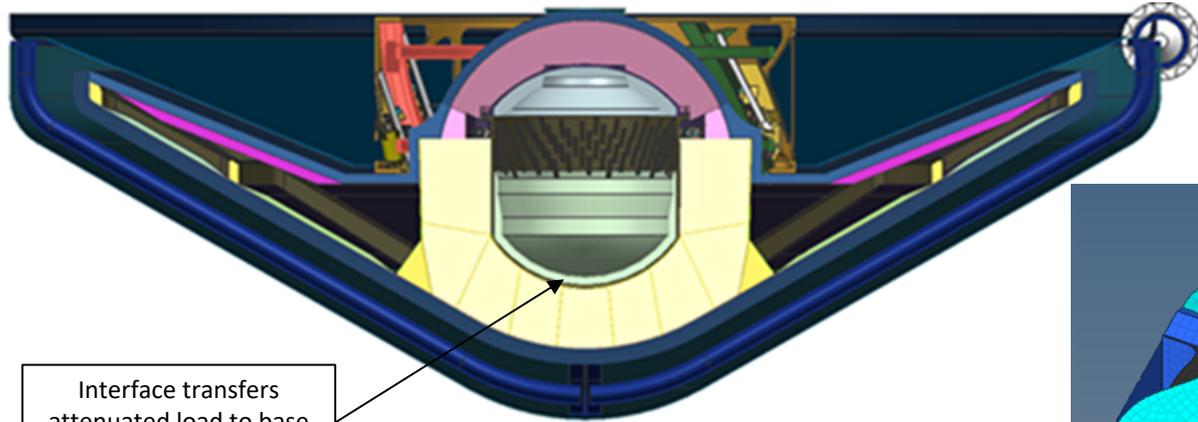
- Primary driver of Contained-OS design is **assurance of sample containment**
- All key mechanisms and interfaces must be able to structurally withstand peak dynamic load environments, while maintaining proper seal engagement at lids of containment vessels
- **Properly assessing the Contained-OS in a dynamic load environment is critical to achieving a viable design**



- Drop-tests were performed to determine the dynamic response at the C-OS during impact
- In initial simulations, the measured acceleration curves are used to approximate the load environment at the C-OS sub-assembly level
- In future simulations, full-scale system level models will be implemented in order to accurately capture load transfer from the EEV to the C-OS to the sample tubes

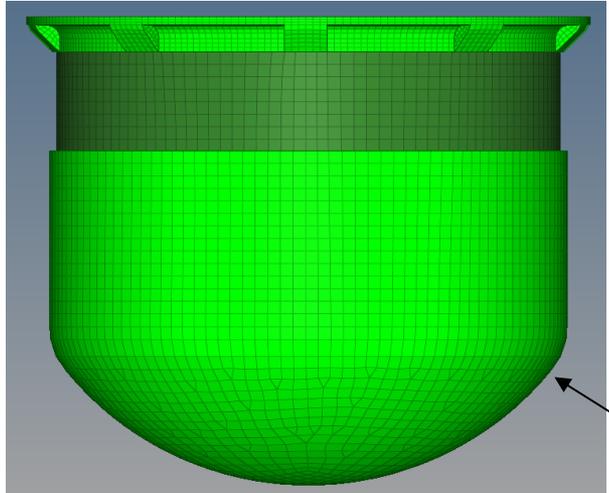


Idealization of Load Environment on C-OS

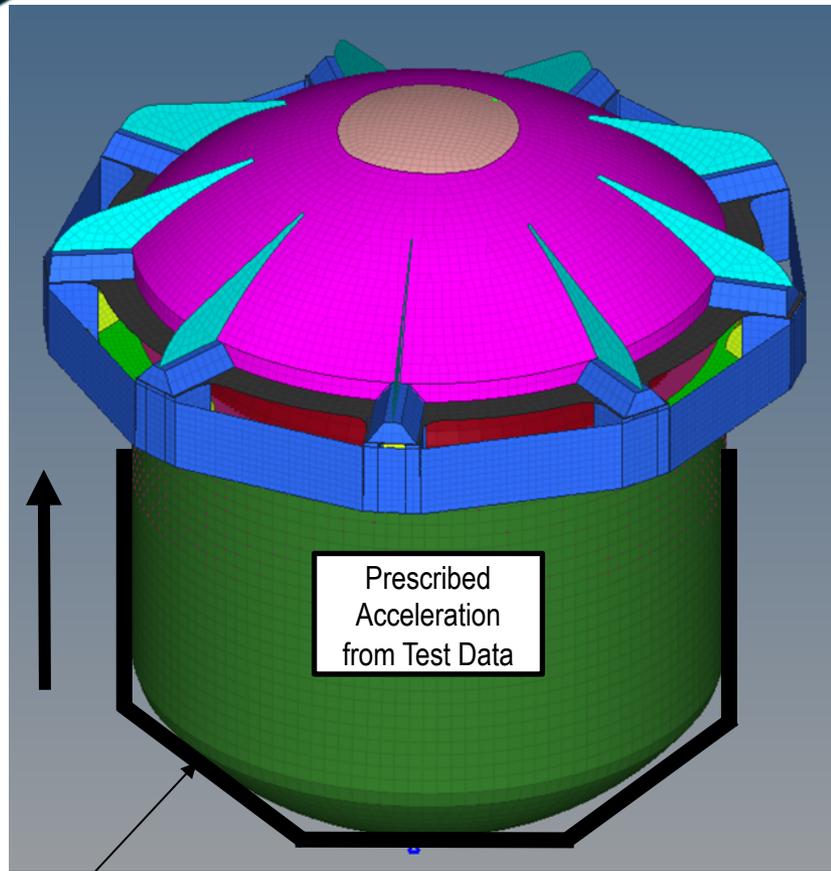


Interface transfers attenuated load to base of C-OS

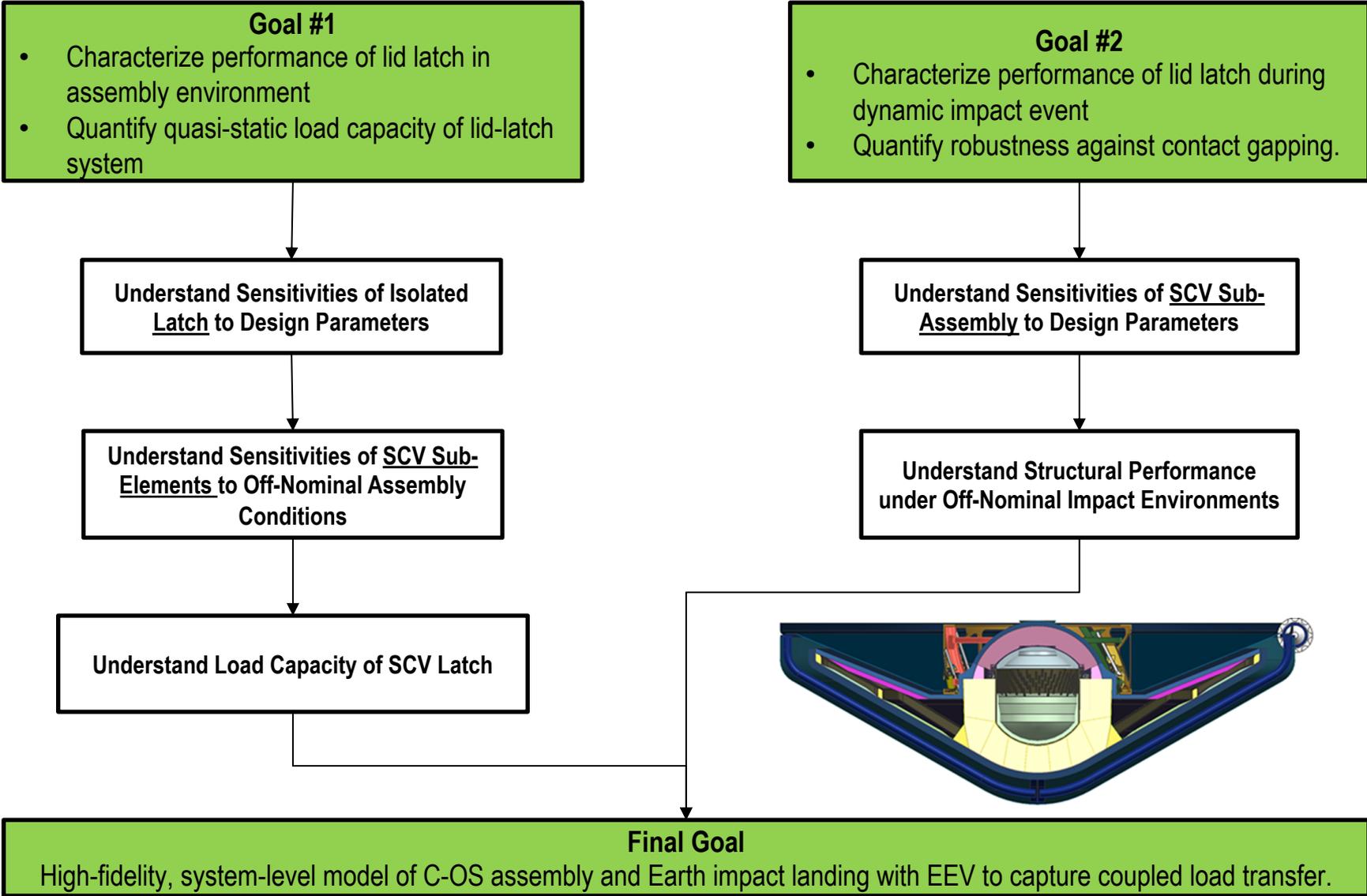
1. Encase SCV in rigid shell
2. Prescribe boundary acceleration to rigid shell
3. Load transfer from rigid shell to SCV sub-structure



Rigid Shell



Prescribed Acceleration from Test Data

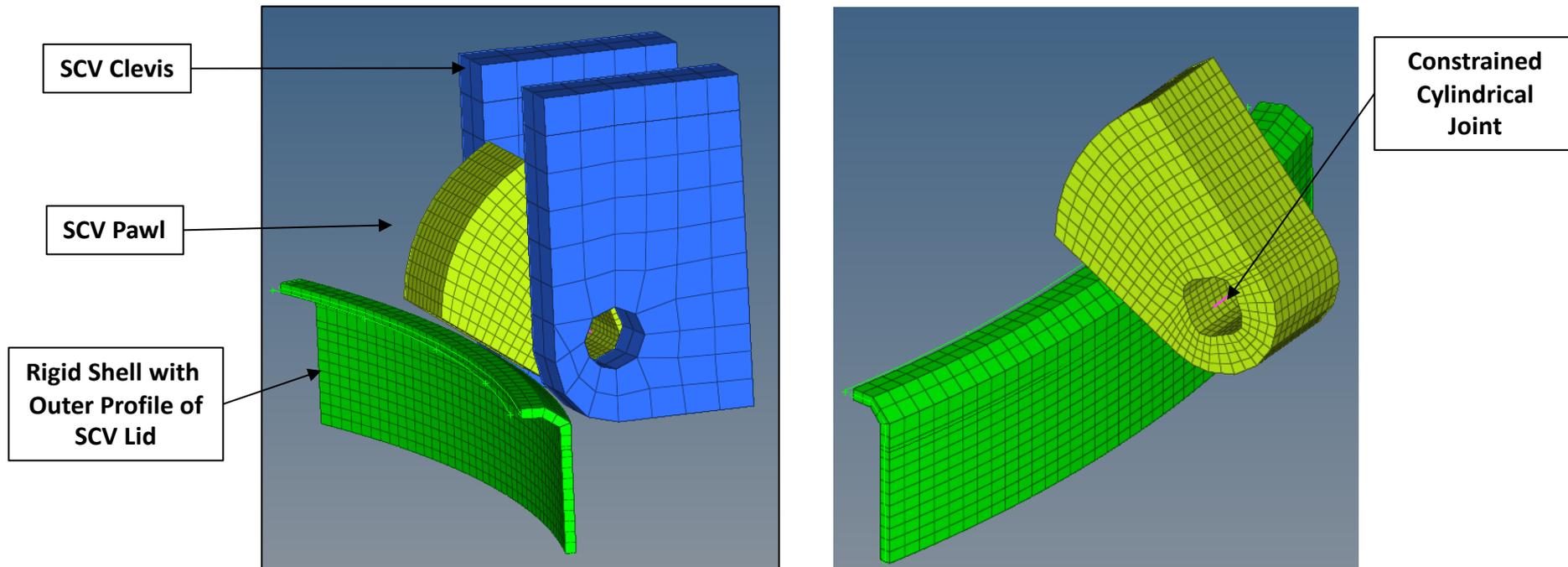


Single Pawl Characterization Studies

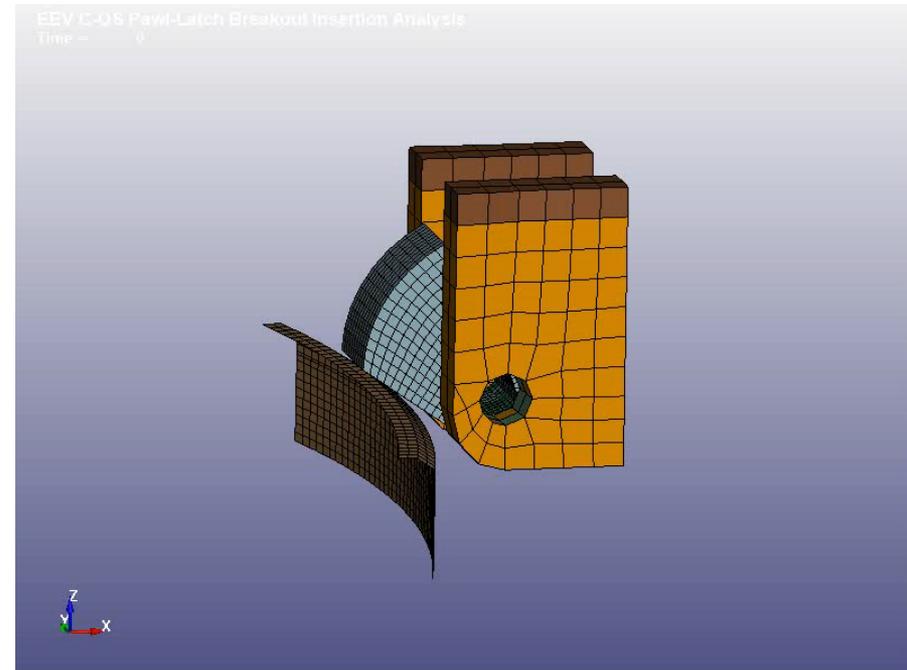
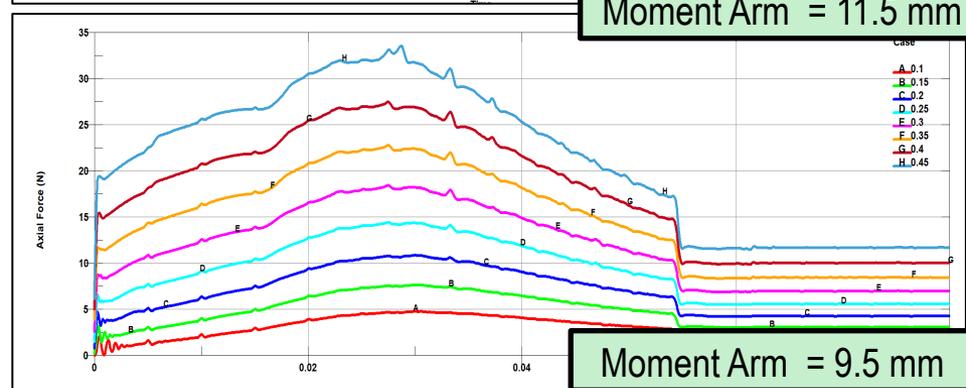
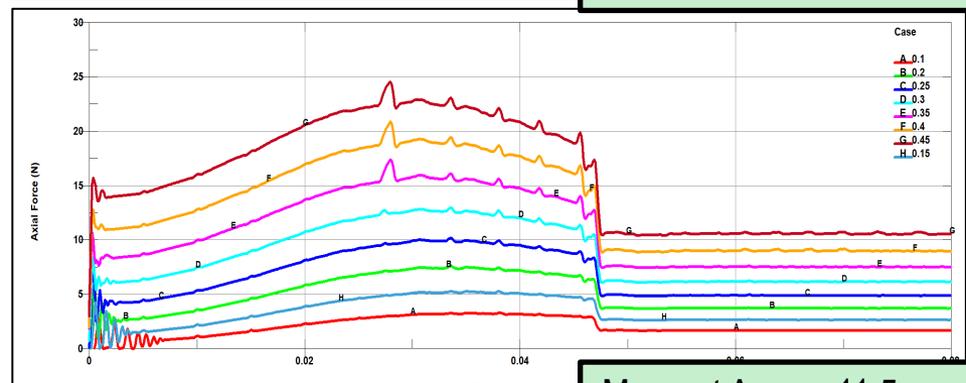
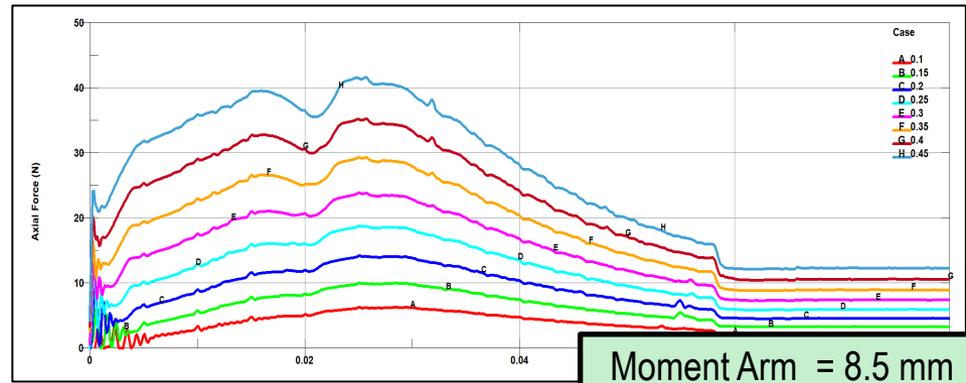
Goal: Characterize performance of pawl during assembly under varying spring stiffness and geometric conditions

Method: Generate rigid-body, single-pawl model to define design space and to verify behavior of *CONSTRAINED_JOINT element in LS-DYNA

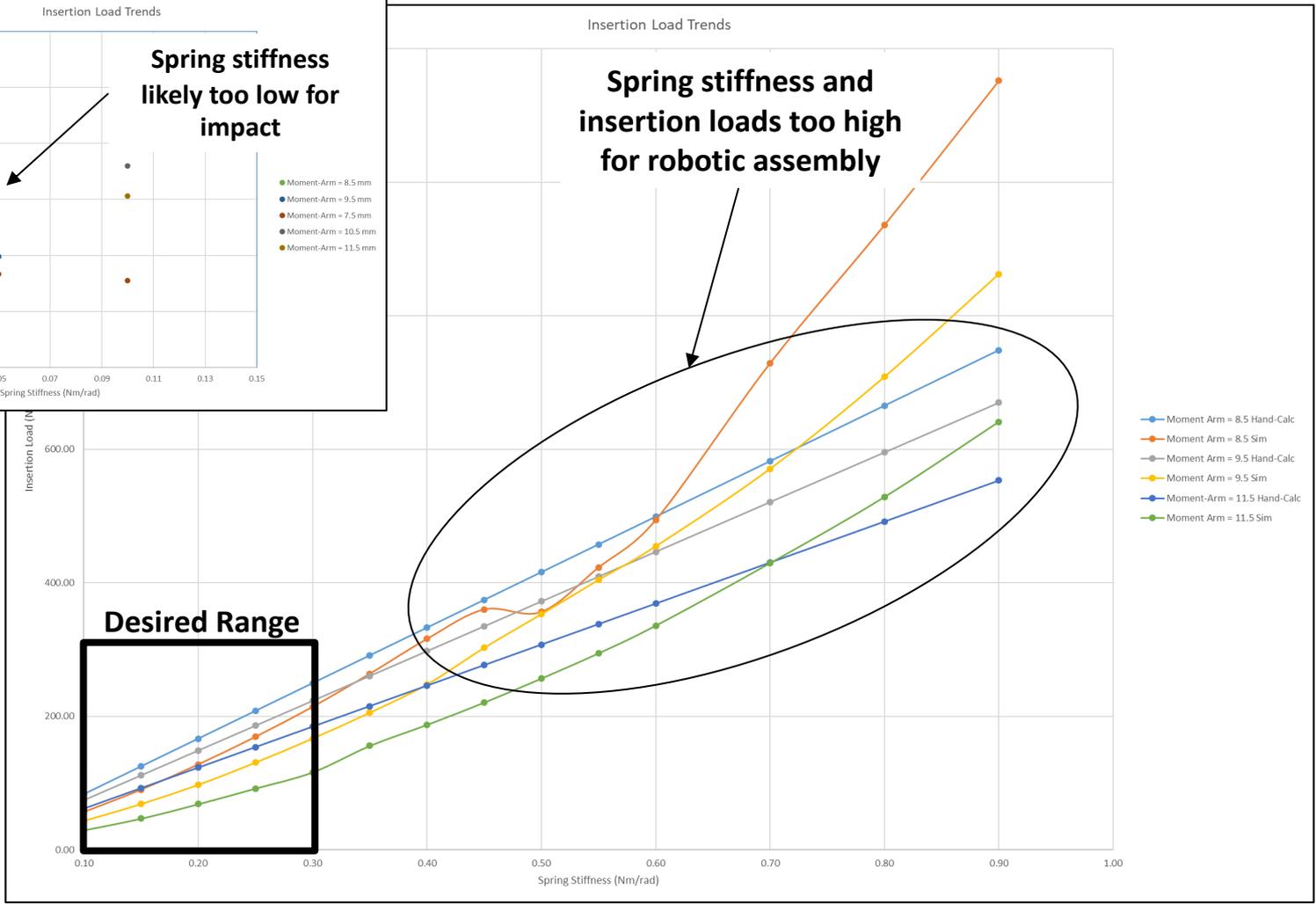
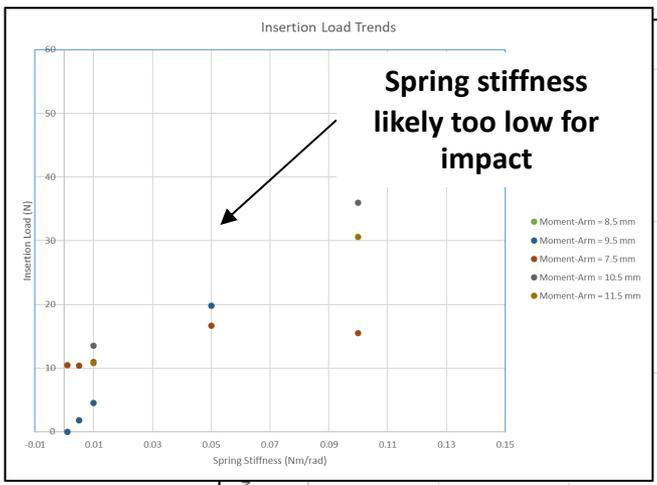
Assumptions: All components rigid, all rotational and in-plane translational DOFs constrained on shell, reduced density of pawl material (to attenuate unrealistic transient effects of pawls due to short simulation time)



Axial Contact Force on Pawl



Initial Simulation-Based Design Space



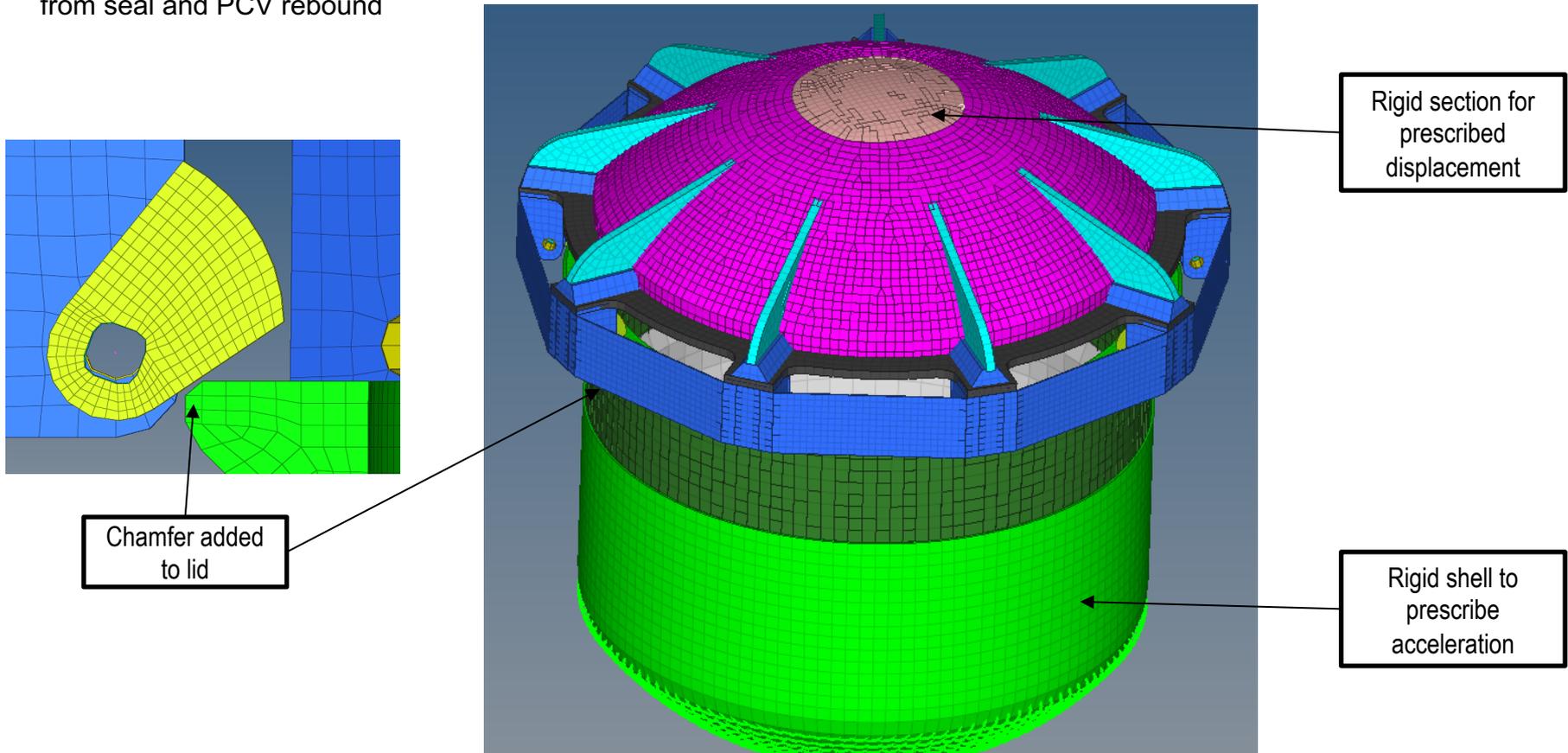
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SCV Sub-Assembly Model

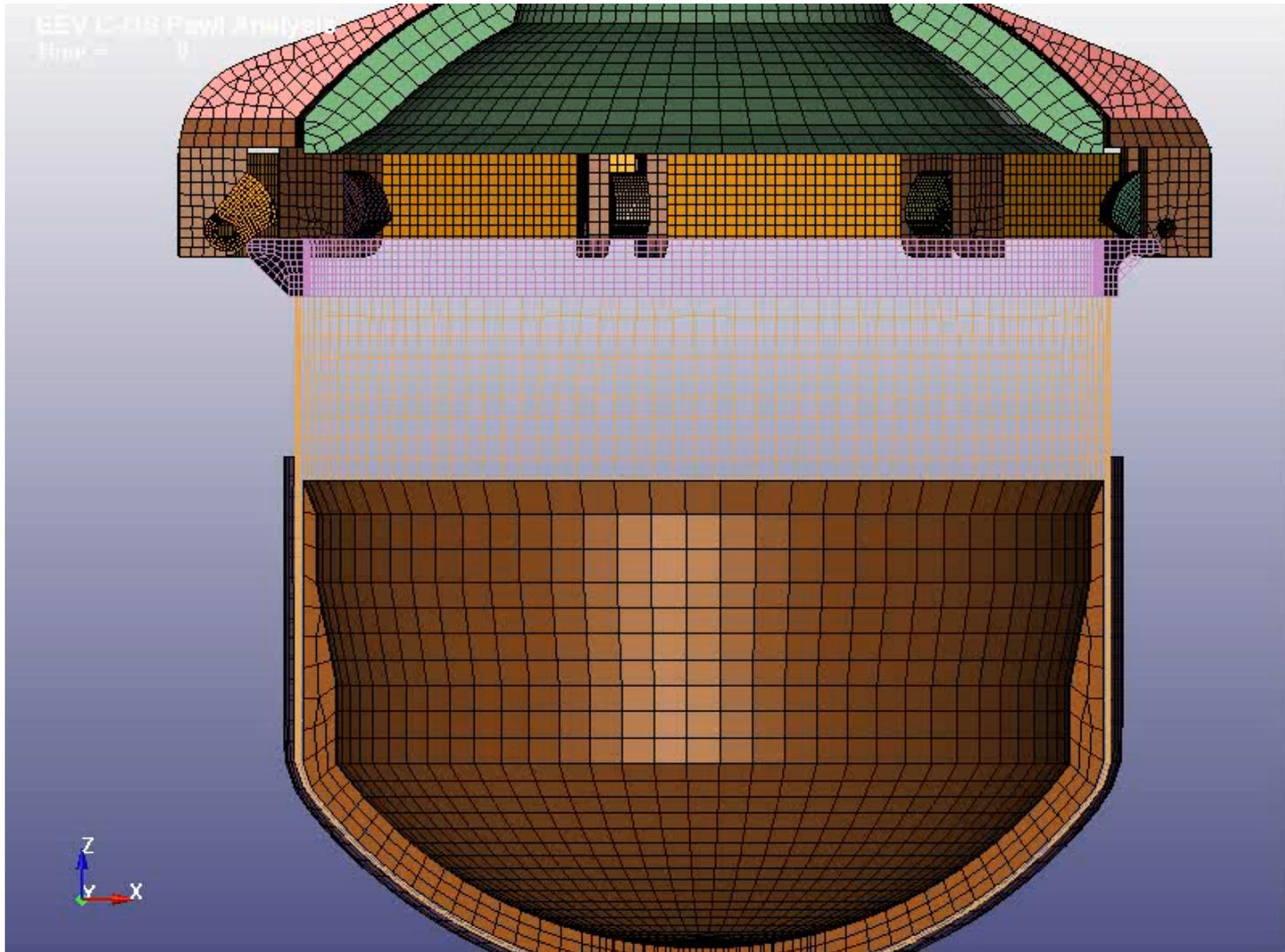
Goal: Characterize performance of SCV latch during SCV lid insertion, retention, and dynamic load environments

Method: Generate break-out model that includes isolated SCV hardware, pawls, and bonded foam – vary parameter space using Hyperstudy

Assumptions: Pawls rigid, chamfer added to lid, base nodes of SCV tied to rigid shell, foam tied to lid, no load contribution from seal and PCV rebound

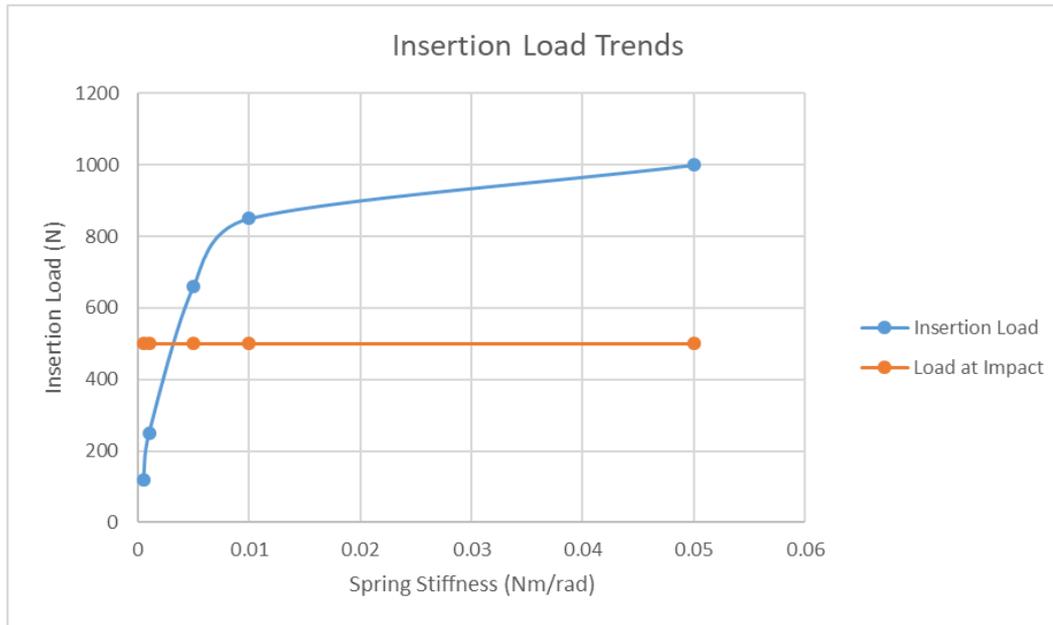


Animation of Simplified System



Pre-Decisional Information – For Planning and Discussion Purposes Only

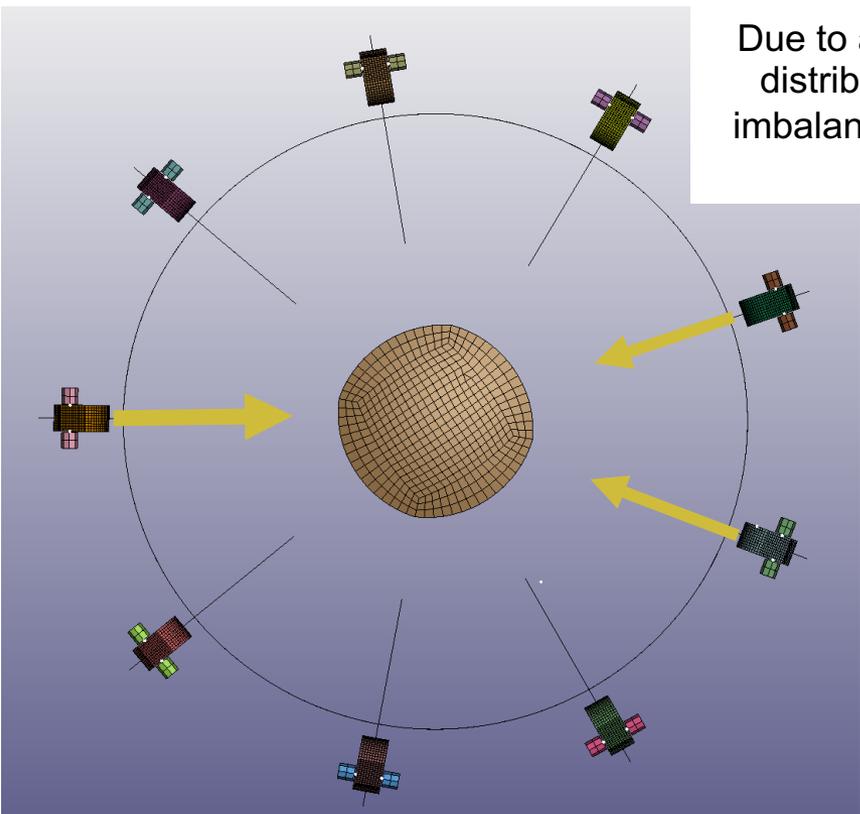
Axial Insertion Loads at SCV Latch



Insertion, Impact, and Extraction Loads		
Stiffness (Nm/rad)	Insertion Load (N)	Load at Impact (N)
0.05	1000	500
0.01	850	500
0.005	660	500
0.001	250	500
0.0005	120	500

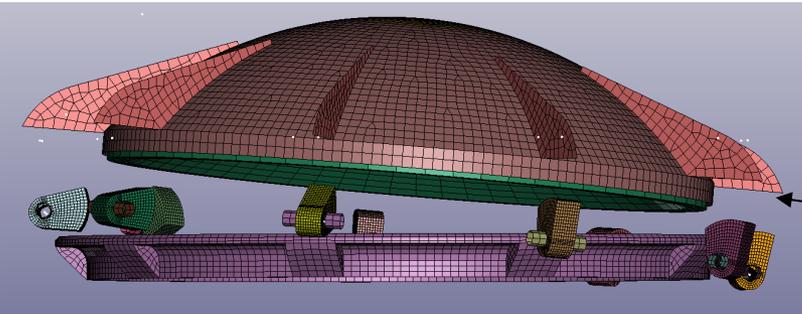
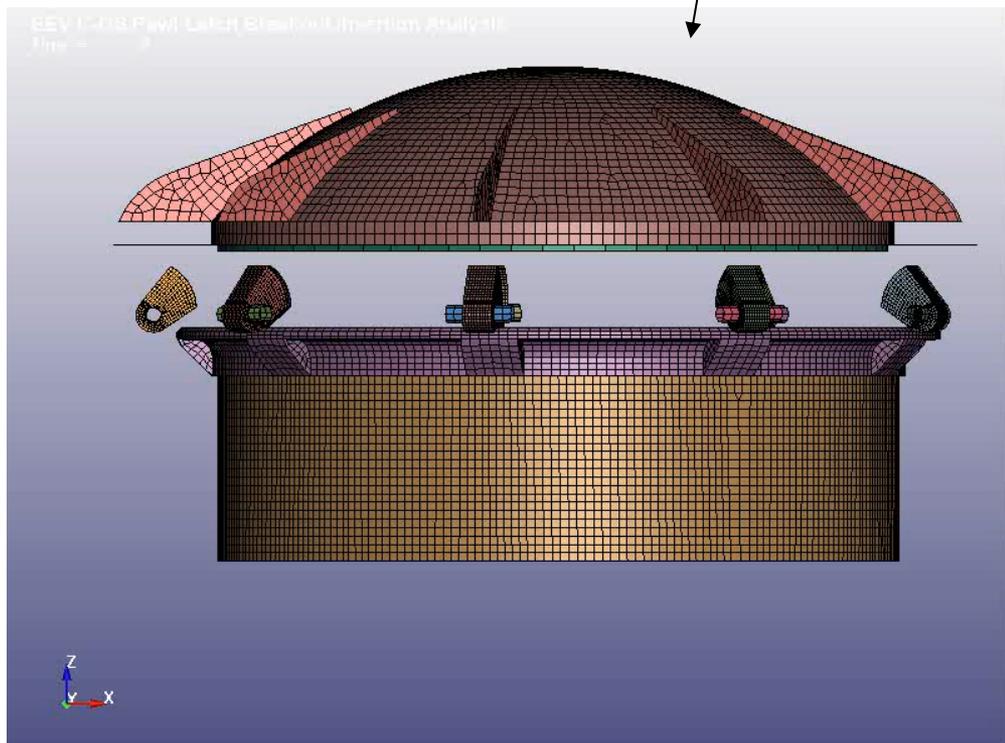
- As spring stiffness increases, insertion load increases
- Extraction loads are consistent over spring stiffness range –**material failure occurs prior to latch failure**
 - Material deflection that produces gapping at lid more likely failure mode than latch failure
- Contact force at lid interface remains non-zero during impact, preliminarily indicating that **no (global) gapping occurs during impact**
 - Local gapping could occur due to lid deflection

General Behavior of Lid Latch



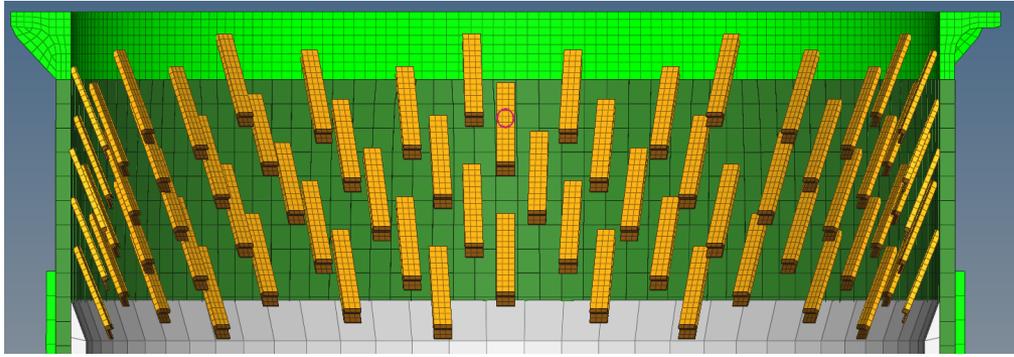
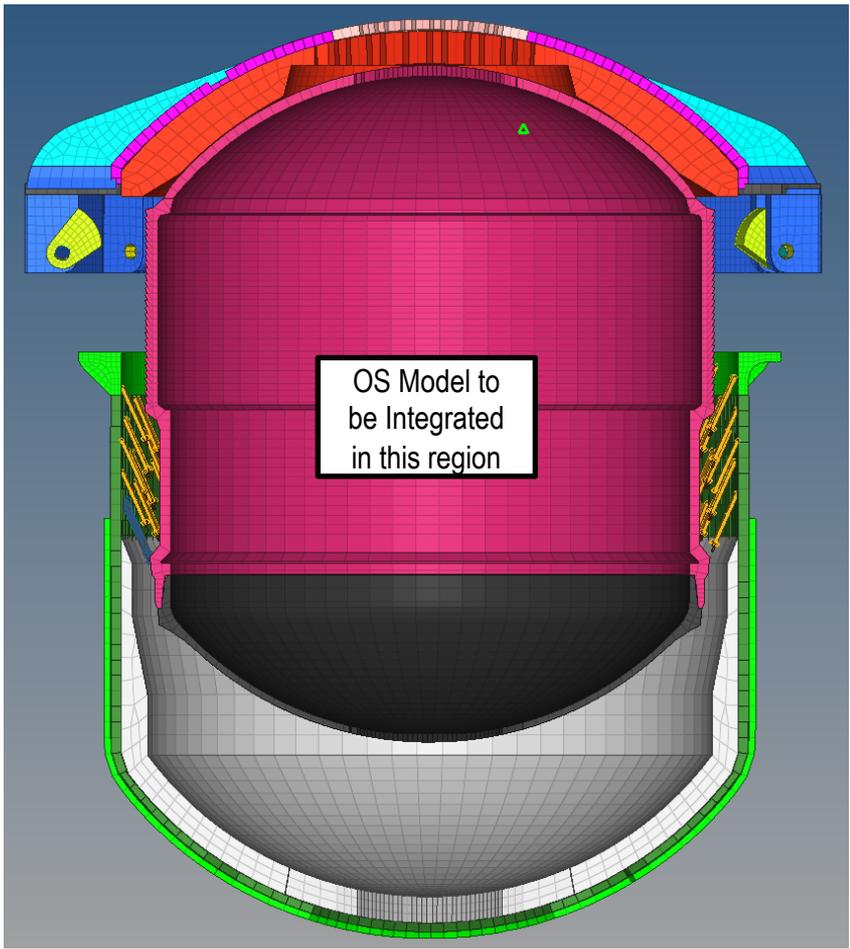
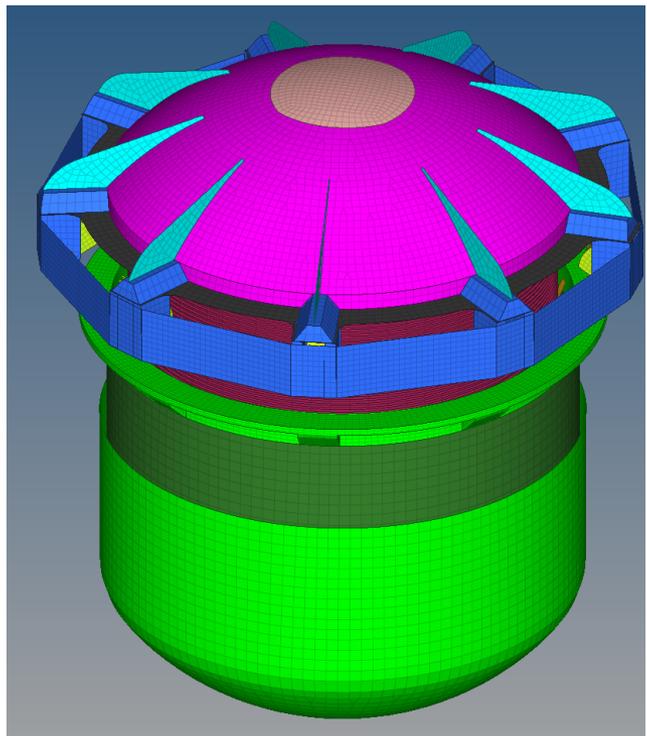
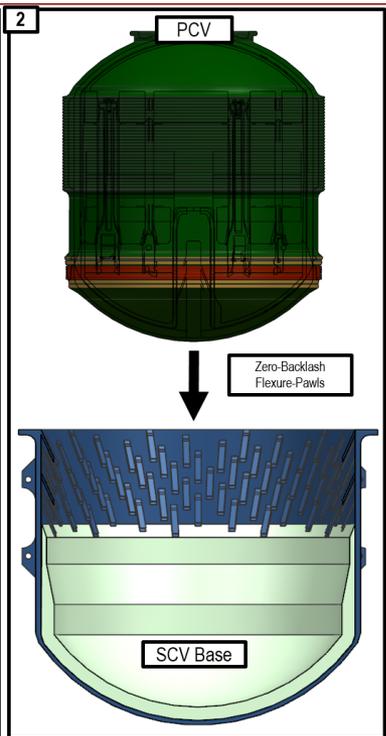
Due to asymmetry in pawl distribution, lateral load imbalance occurs on initial insertion

Mechanism allows for self-alignment in off-nominal case



When rotational DOF constraints on lid removed during insertion, lateral load imbalance causes instability

SCV and PCV Assembly Model

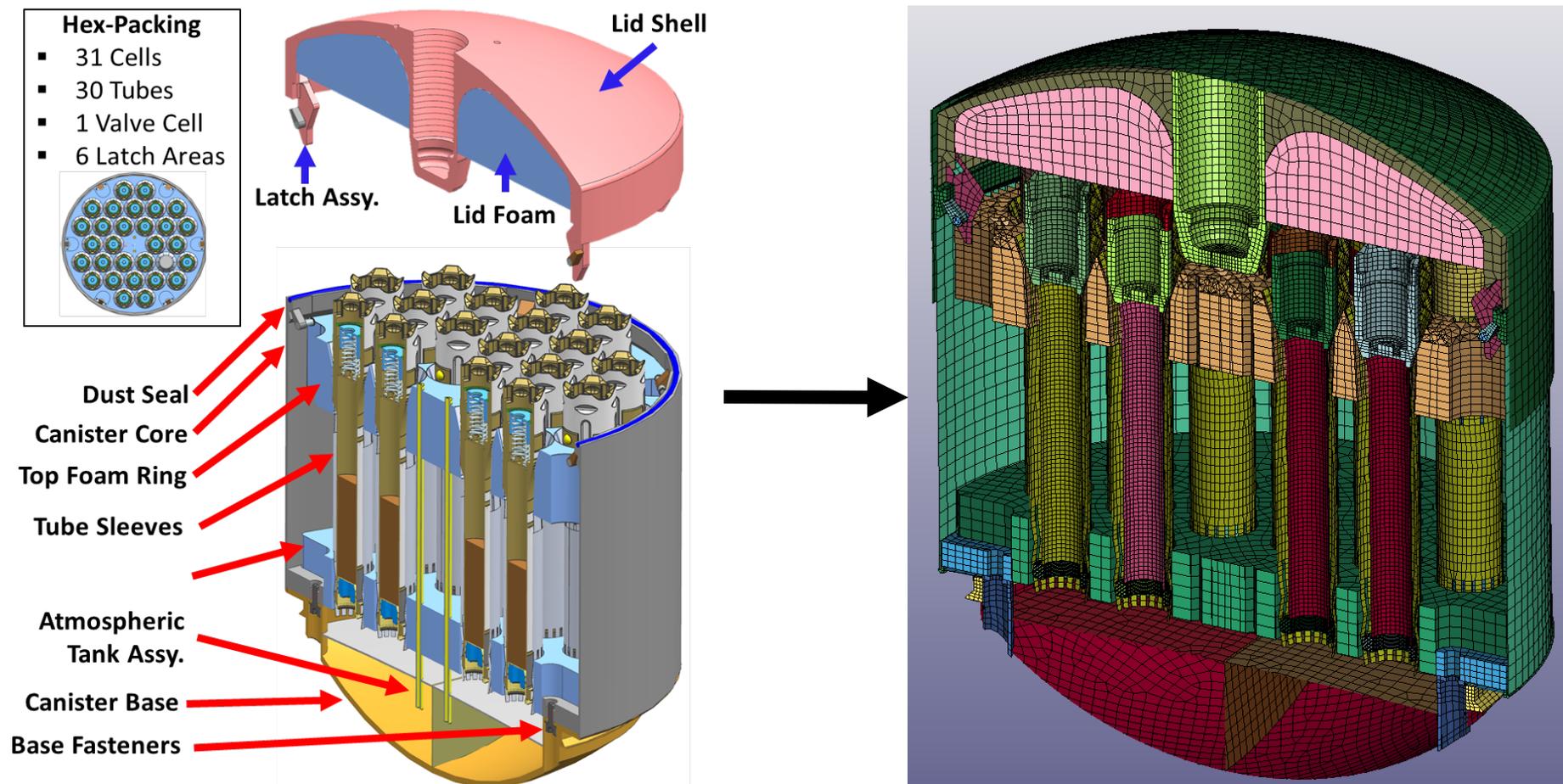


- Simulation and analysis and performance characterization of lid latch designs is currently underway – will be verified with testing
- In conjunction, simplified sub-system level models are being used for understanding behavior and sizing – will be verified with testing
- Sub-system level models and lid latch models will be integrated into a single C-OS system-level model to quantify coupled performance of mechanisms under impact
- C-OS system-level model will be integrated into EEV model to simulate entire Earth impact landing event
- Analysis will eventually be verified with an extensive test program that includes:
 - Material test campaign
 - PCV impact, SCV impact, PCV/OS impact, C-OS impact testing
 - Soft and hard EEV impact testing

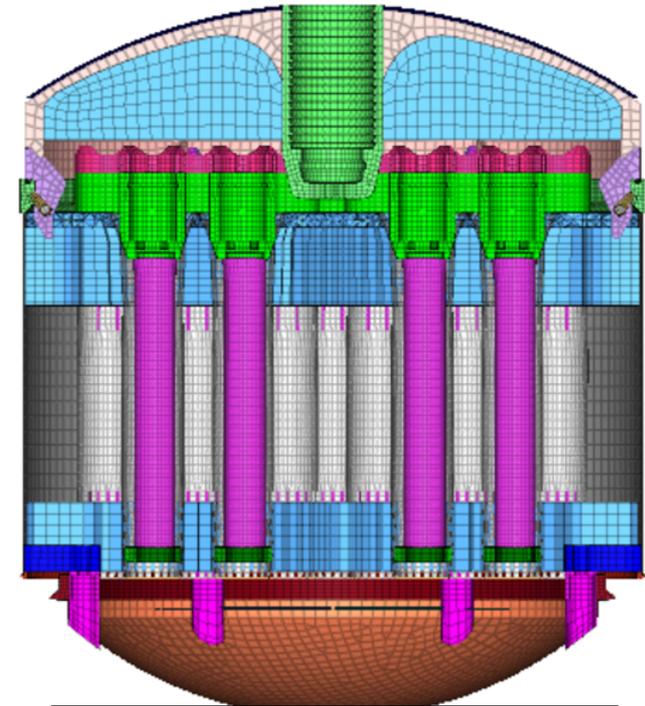
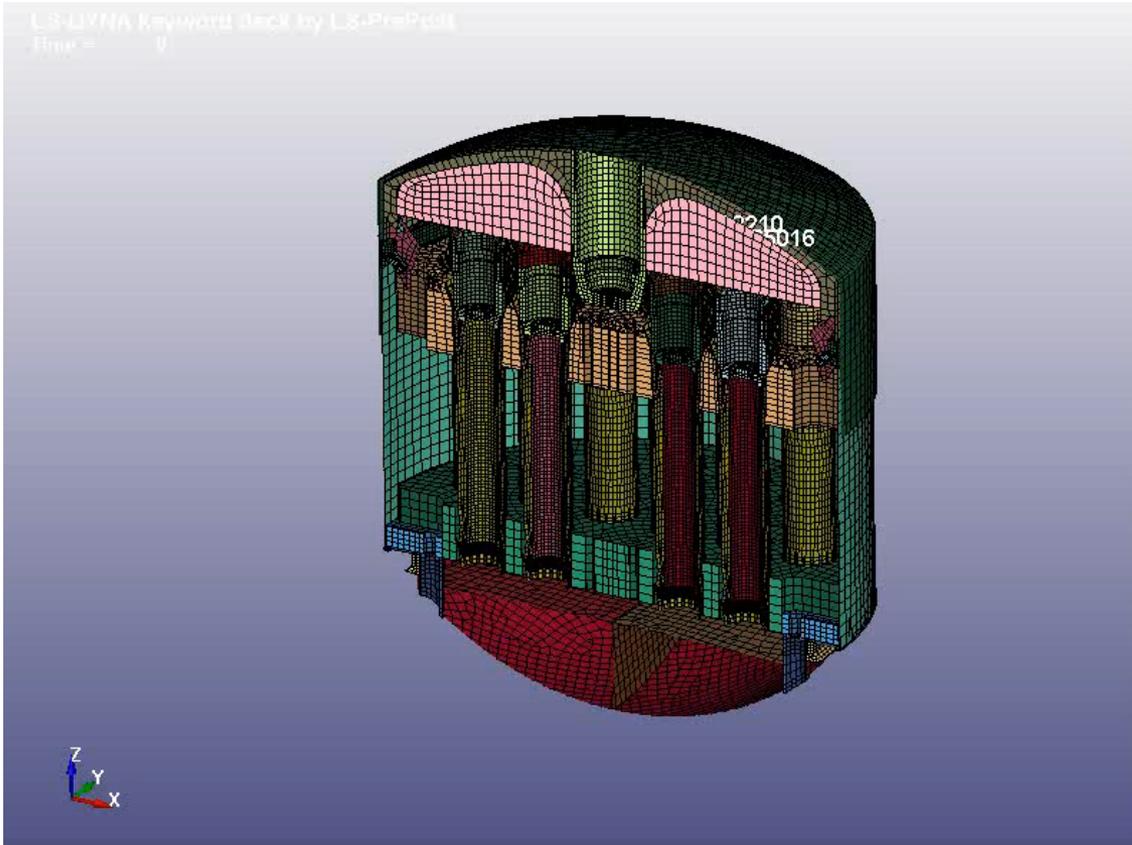
Back-Up: Path Forward to System-Level Model

Non-Spherical OS Idealized FEM

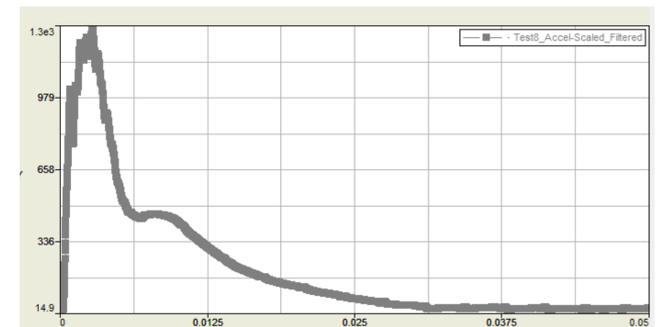
Idealized OS model used to verify positive structural margins for hardware sizing verification – all interfaces tied and no mechanisms explicitly modeled



OS Behavior under Impact

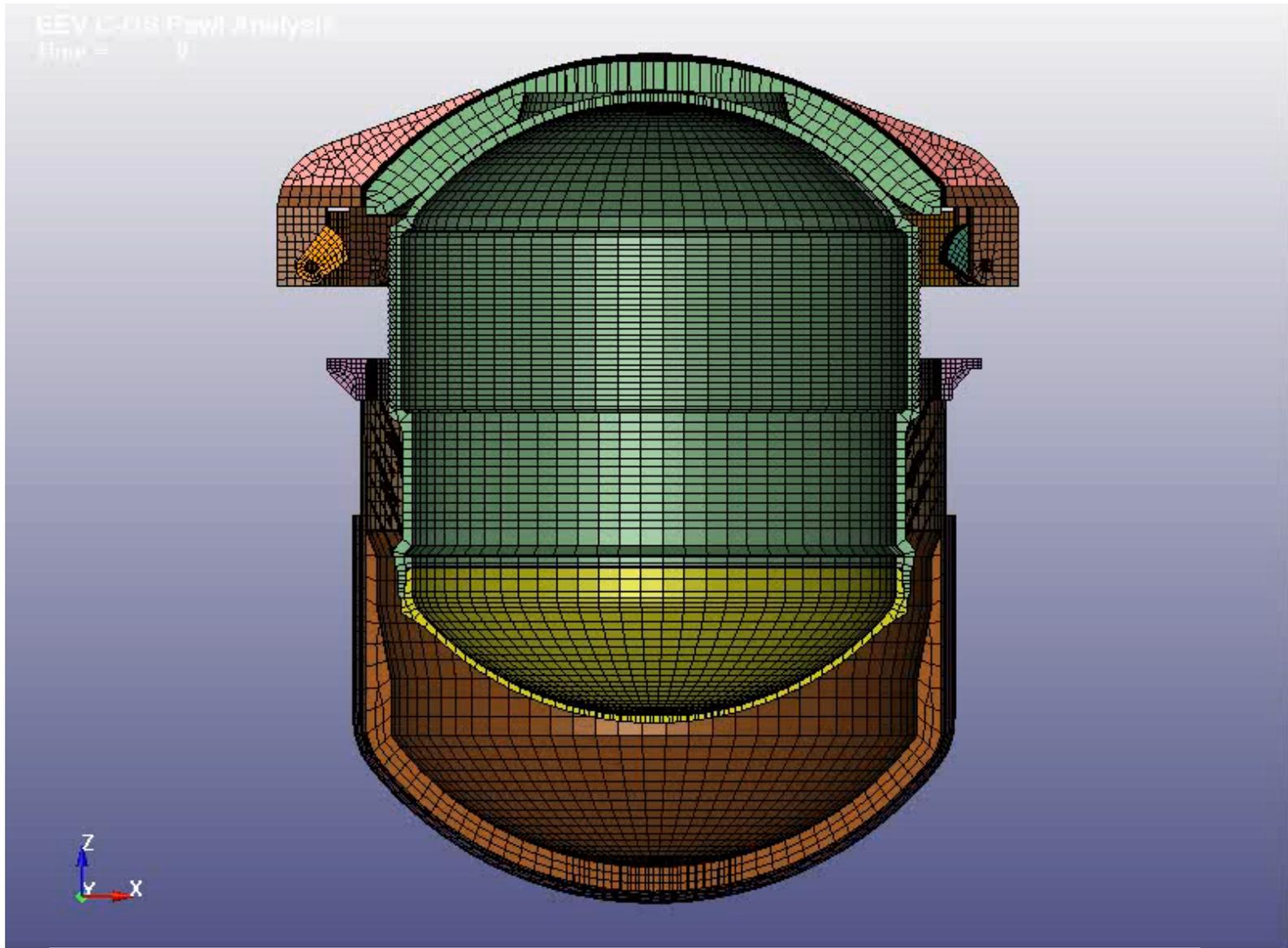


Prescribed acceleration applied to rigid shell



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Animation of Assembly



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