



InSight Attitude Control System Thruster Characterization and Calibration for Successful Navigation to Mars

Jill Seubert, Eric Gustafson, Allen Halsell, Julim Lee, Sarah
Elizabeth McCandless

Jet Propulsion Laboratory, California Institute of Technology

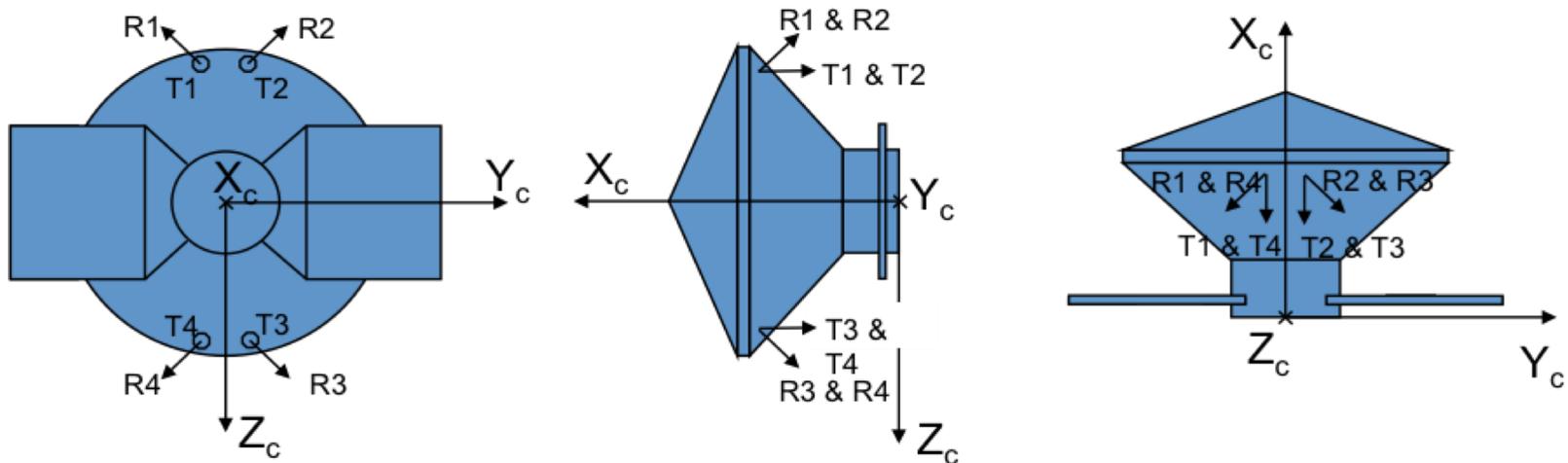
AAS/AIAA Space Flight Mechanics Meeting, AAS 19-222

January 15, 2019

- InSight carried significant heritage from 2007 Phoenix Lander – including unbalanced Reaction Control System (RCS) thrusters used for attitude control
- Proper in-flight characterization of thruster firings (small forces) historically significant for Mars exploration
 - e.g. 2001 Mars Odyssey, 2005 MRO, 2007 Phoenix Lander
 - Loss of 1999 MCO
- Accumulation of ~ 29,000 RCS thruster firings over 7 month cruise significant impacted spacecraft trajectory
 - Accurate reconstruction and prediction of RCS thruster firings was crucial for successful delivery to atmospheric entry point

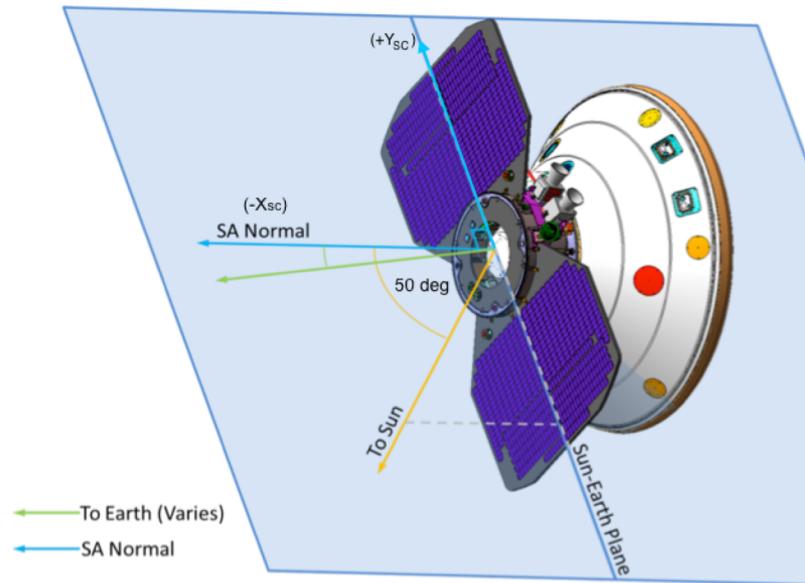
Attitude Control System (ACS)

- Attitude control provided via an unbalanced thruster system
 - 4 Reaction Control System (RCS) thrusters fire in pairs for 3-axis stabilization & slew to/from TCM attitudes
- 4 Trajectory Correction Maneuver (TCM) thrusters execute main burns
- RCS/TCM thrusters mounted onto lander & extended through backshell
 - Scarfed to backshell contour
 - Each RCS thrust vector had non-zero component in all 3 axes

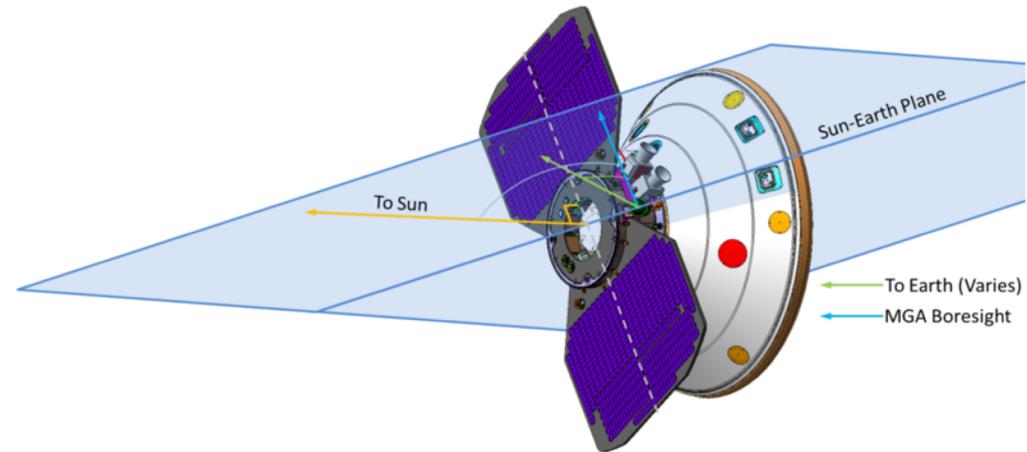


- Two attitude profiles designed to balance power, communications, and thermal constraints throughout cruise

Early Cruise: Launch to July 12



Late Cruise: July 12 to Entry



- Early cruise: 3-axis RCS ΔV due to off-Sun pointing
- Late cruise: Y and Z nominally balanced, RCS ΔV in X direction
 - In reality, thrusters not perfectly balanced, small ΔV s in Y and Z also

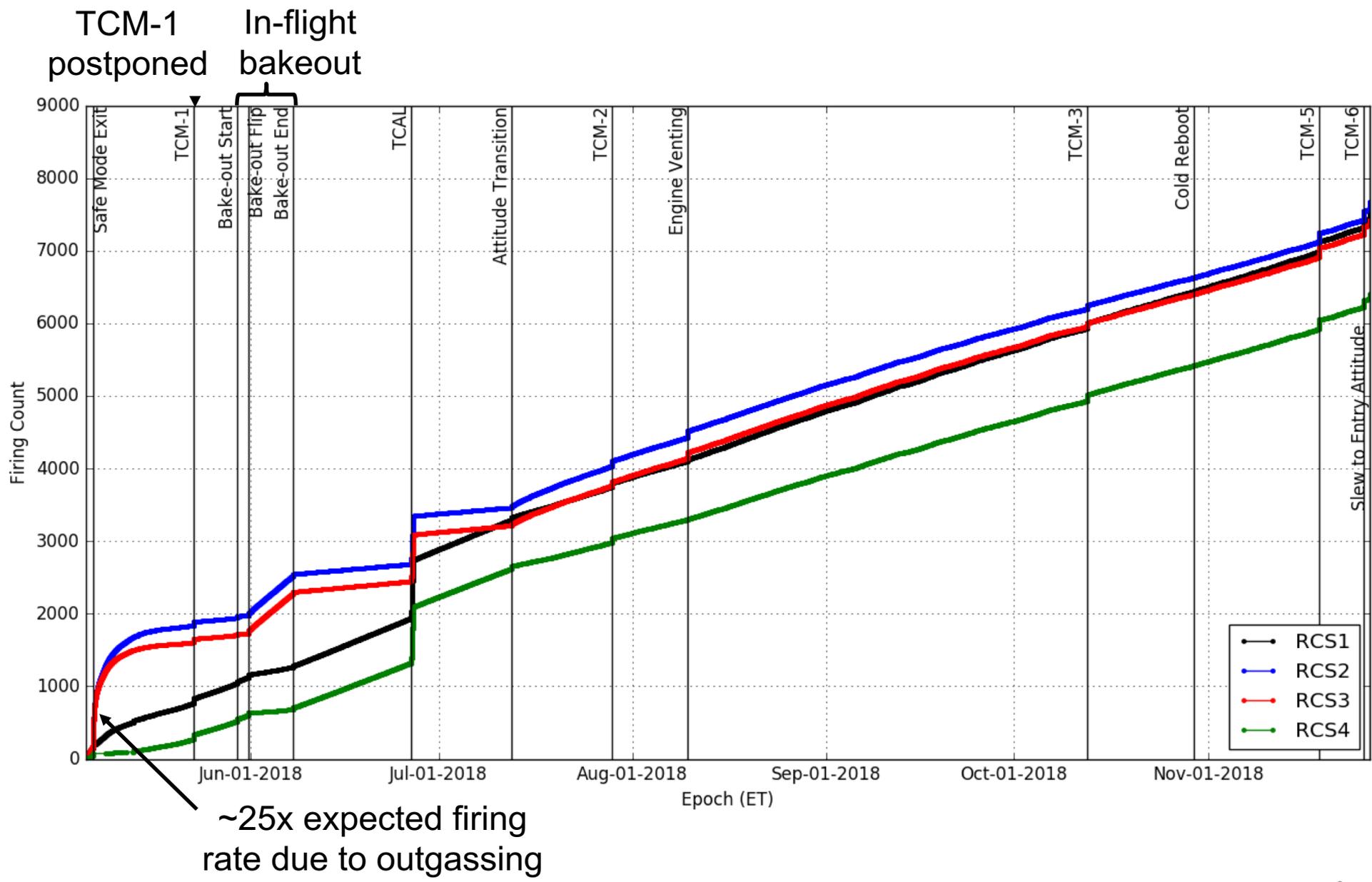
- Nominal cruise attitudes maintained via deadbanding
 - Attitude allowed to drift through 3-D deadband
 - RCS thrusters fired when a deadband limit was reached

- Early and late cruise deadbands defined to cover Earth/Sun/Spacecraft geometry variation
 - Tighter deadband constraints resulted in more frequent thruster firings
 - Imparted ΔV increased after late cruise transition

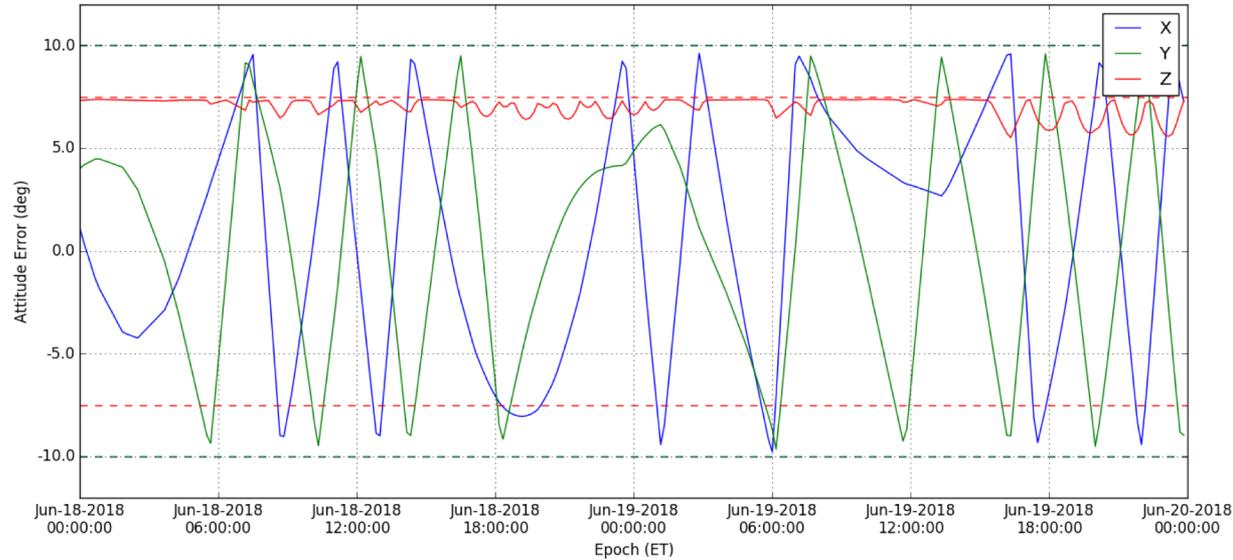
Table 1. Spacecraft Attitude Deadband Definitions (Spacecraft-Fixed Frame)

Cruise Phase	X	Y	Z
Early Cruise (May 5, 2018 to July 12, 2018)	10°	10°	7.5°
Late Cruise (July 12, 2018 to November 26, 2018)	4°	4°	4°

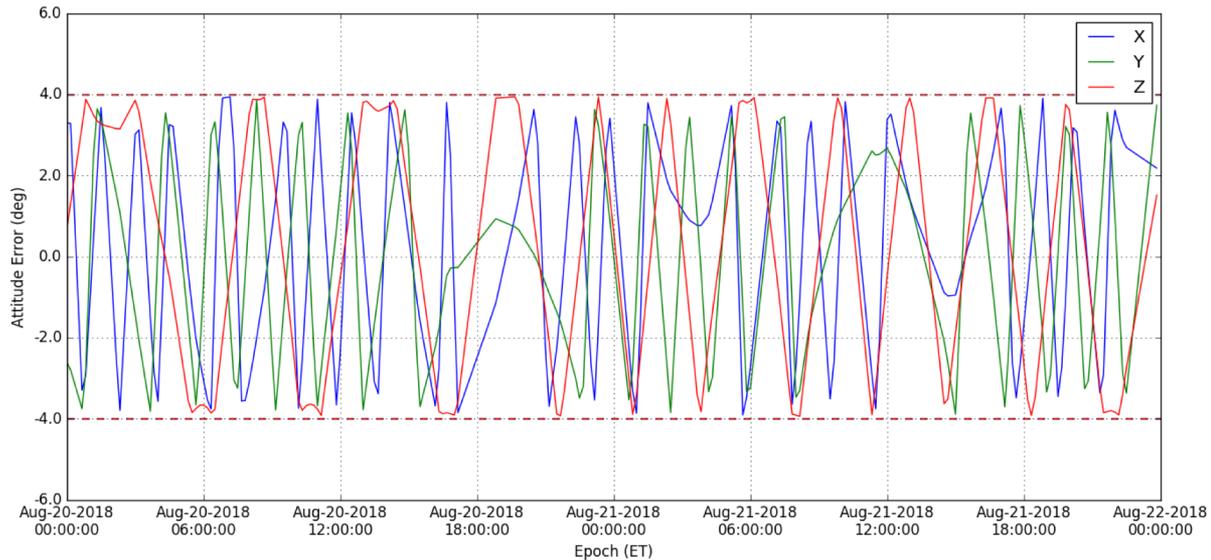
- Attitude knowledge via star trackers, MIMUs, Sun sensors (backup)
- Raw telemetry packet recorded with every RCS/TCM thruster pulse
 - Thruster on time
 - Pulse length
 - Thruster number
 - On-board estimated ΔV & quaternions at time of firing
- Raw telemetry used to construct *a priori* models of small forces and attitude for orbit determination (OD) and trajectory prediction
- On-board filtered telemetry used during Thruster Calibration analysis



- Early cruise:
 - Solar torque due to off-Sun pointing pinned spacecraft against +Z deadband
 - Drifts between $\pm X$ and $\pm Y$ limits

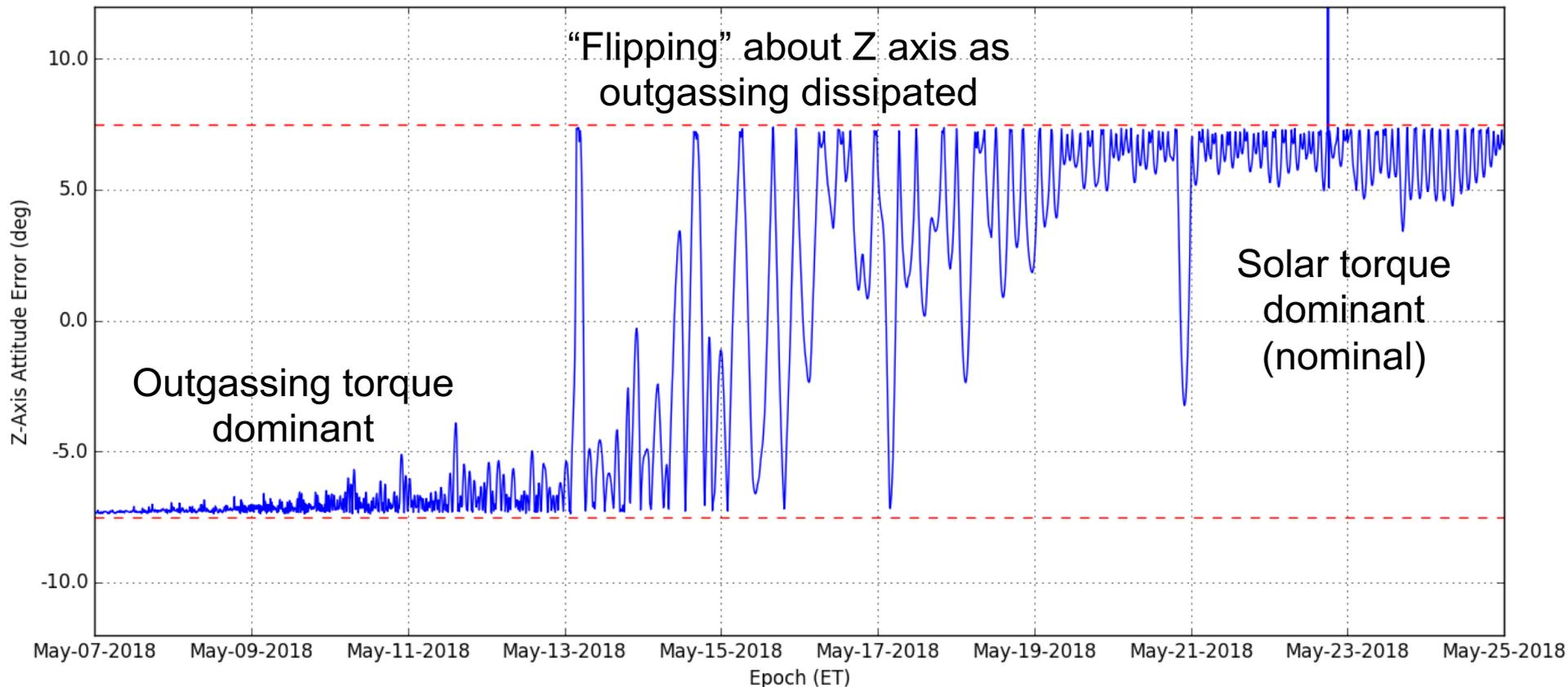


- Late cruise:
 - Solar torque balanced as solar arrays ~ Sun-pointed
 - Drifts between $\pm X$, $\pm Y$, $\pm Z$ limits



Attitude Errors During Heavy Outgassing (May 2018)

- Outgassing torque pinned spacecraft against the -Y, -Z deadbands
- Outgassing and solar pressure torques acted in opposite directions
 - Solar torque effect not observable until outgassing dissipated



- OD strategy accounted for errors in small force telemetry
 - Reconstructed behavior of each individual RCS thruster
 - Improved upon Phoenix strategy (estimated accumulative effect of all RCS thrusters combined)
- ACS on-board telemetry used to model *a priori* attitude and ΔV at the time of each RCS thruster firing
 - Effective thrust vectors and imparted ΔV per firing based on:
 - Pre-TCAL: pre-launch models
 - Post-TCAL: estimated values
- Filter configured to estimate corrections to thruster models

Table 2. Baseline Small Force Estimation Strategy

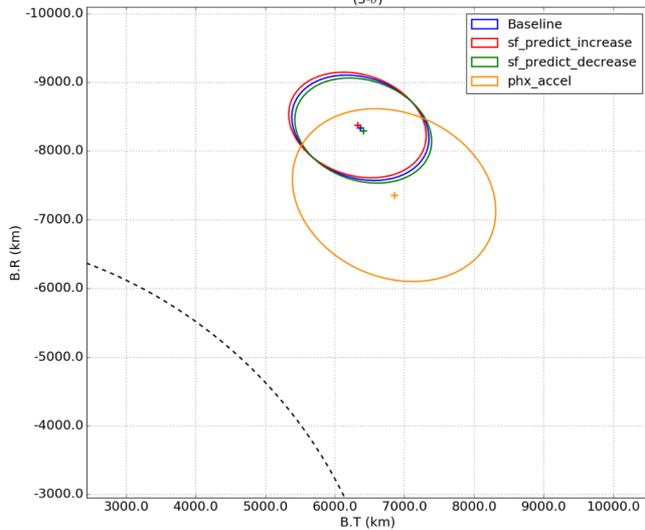
Estimated Parameter (Per Thruster)	Model	<i>A Priori</i> Value	<i>A Priori</i> Uncertainty
Thrust Direction Y Offset	Bias	0°	3°
Thrust Direction Z Offset	Bias	0°	3°
ΔV Magnitude	Bias	0%	3%
ΔV Magnitude	White Noise Stochastic	0%	15%

- Propagation of OD solution from data cut off to entry interface point included predictions of future small force behavior of each RCS thruster
 - Average acceleration empirically-determined via linear fit to recent firing counts
 - Linear firing rate computed for each thruster, converted to average acceleration using nominal thruster models
 - Nominal ΔV magnitude corrected based on estimated ΔV scale factor
- Effectively, on-going thruster characterization of short-term deadbanding behavior in response to varying astrodynamics conditions

- Various predictive models compared throughout cruise to assess suitability of baseline approach
- Impact of small force prediction proportional to “time to go”

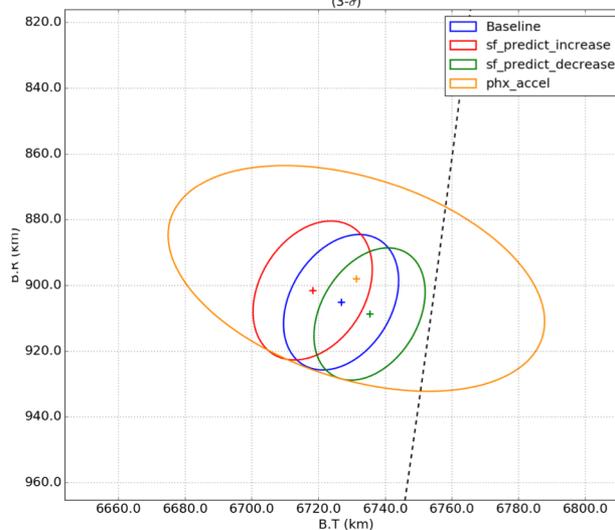
TCM-2 DCO
Entry-142 days

Insight B-Plane Plot
MARS MEAN EQUATOR IAU NODE OF DATE INERTIAL IAU_2000
(3- σ)



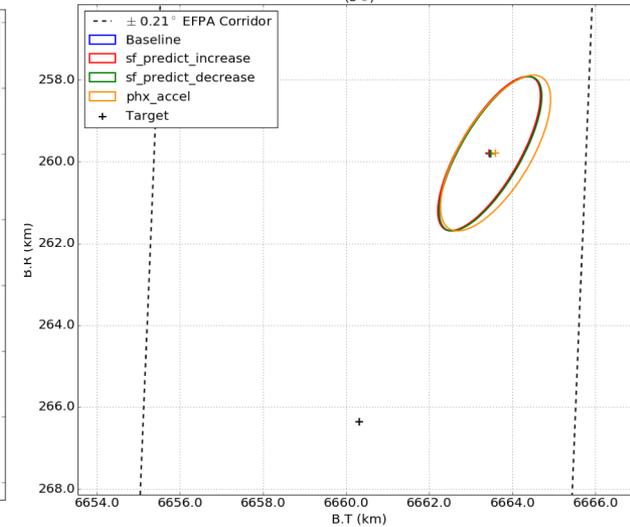
TCM-3 DCO
Entry-50 days

Insight B-Plane Plot
MARS MEAN EQUATOR IAU NODE OF DATE INERTIAL IAU_2000
(3- σ)



TCM-6 DCO
Entry-48 hrs

Insight B-Plane Plot
MARS MEAN EQUATOR IAU NODE OF DATE INERTIAL IAU_2000
(3- σ)

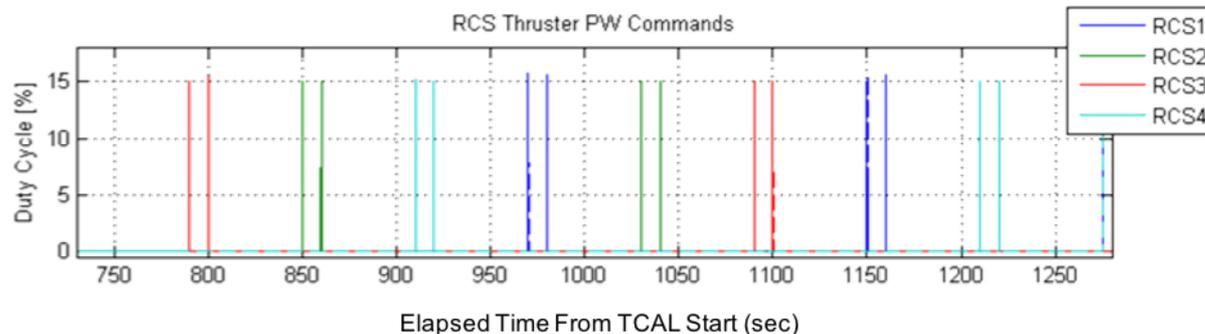


- Solution uncertainty driven by data uncertainties
- Phoenix model $> 3\sigma$ away from baseline

- Solution uncertainty driven by small force model
- $\pm 5\%$ acceleration shifts solution by 1σ

- Short propagation time renders models indistinguishable

- Attempt to calibrate RCS thrusters in cruise environment via Thruster Calibration (TCAL)
 - Spacecraft rotated through four attitudes, sequence of thruster pulses (“pulse train”) executed at each attitude
 - Pulse train executed 9x per attitude, attitude reset between executions
 - Attitudes selected to maximize line-of-sight observability, within safety constraints
- Pulse trains not representative to nominal deadbanding behavior
 - Thrusters fired much more frequently
 - Temperature-driven variations affect both direction and magnitude of thrust vector



- Objective: estimate linear impulse vector (\vec{p}) imparted by each thruster
- Multiple data streams utilized to enhance TCAL quality
 - Quaternion telemetry – 5 Hz
 - Angular rate ($\Delta\omega$) telemetry – 5 Hz channelized, 50 Hz via MIMU
 - Doppler data - 1 Hz (data calibrated with OD solution to remove other dynamic/measurement errors)
- Data filtered to include only minimum impulse bit firings, to be more representative of nominal deadbanding
- Each pulse train filtered separately, combined in statistical batch sense

First constraint: angular momentum equation $\rightarrow \Delta\vec{H} = I\Delta\vec{\omega} = \vec{r} \times \vec{p} = S(\vec{r})\vec{p}$

Second constraint: linear momentum equation $\rightarrow \vec{p} = m\Delta\vec{V}$

$$\begin{bmatrix} S(\vec{r}) \\ \vec{l}^T \end{bmatrix} \vec{p} = \begin{bmatrix} I\Delta\vec{\omega} \\ m(\vec{l} \cdot \Delta\vec{V}) \end{bmatrix} \rightarrow \text{Fully-determined system to estimate } \vec{p}$$

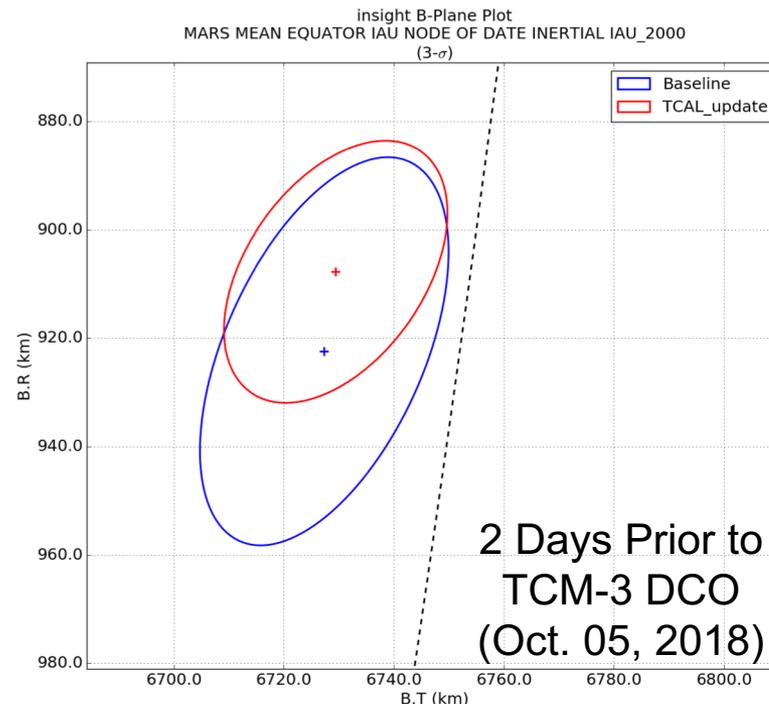
- Large offsets in thrust direction and magnitude scale factors estimated for each RCS thruster
 - Substantially larger than pre-launch uncertainties (3 degrees, 3%)

Table 4. Estimated Thruster Magnitude Scale Factor and Direction ([X, Y, Z])

	RCS1	RCS2
Nominal Direction	[0.3404, 0.7411, 0.5786]	[0.3652, -0.7571, 0.5417]
Estimated Direction	[0.4722, 0.7642, 0.4394]	[0.3610, -0.8002, 0.4790]
Estimated Direction Offset	11.08°	4.367°
Estimated Scale Factor	0.6738	0.7525
	RCS3	RCS4
Nominal Direction	[0.3707, -0.7661, -0.5251]	[0.3308, 0.7493, -0.5736]
Estimated Direction	[0.5176, -0.6997, -0.4925]	[0.4922, 0.7713, -0.4036]
Estimated Direction Offset	9.434°	13.52°
Estimated Scale Factor	0.6536	0.6900

- Applying estimated values to *a priori* OD filter models improved estimation of thrust magnitude, but not thrust direction
 - Filter still adjusts *a priori* directions by significant amount

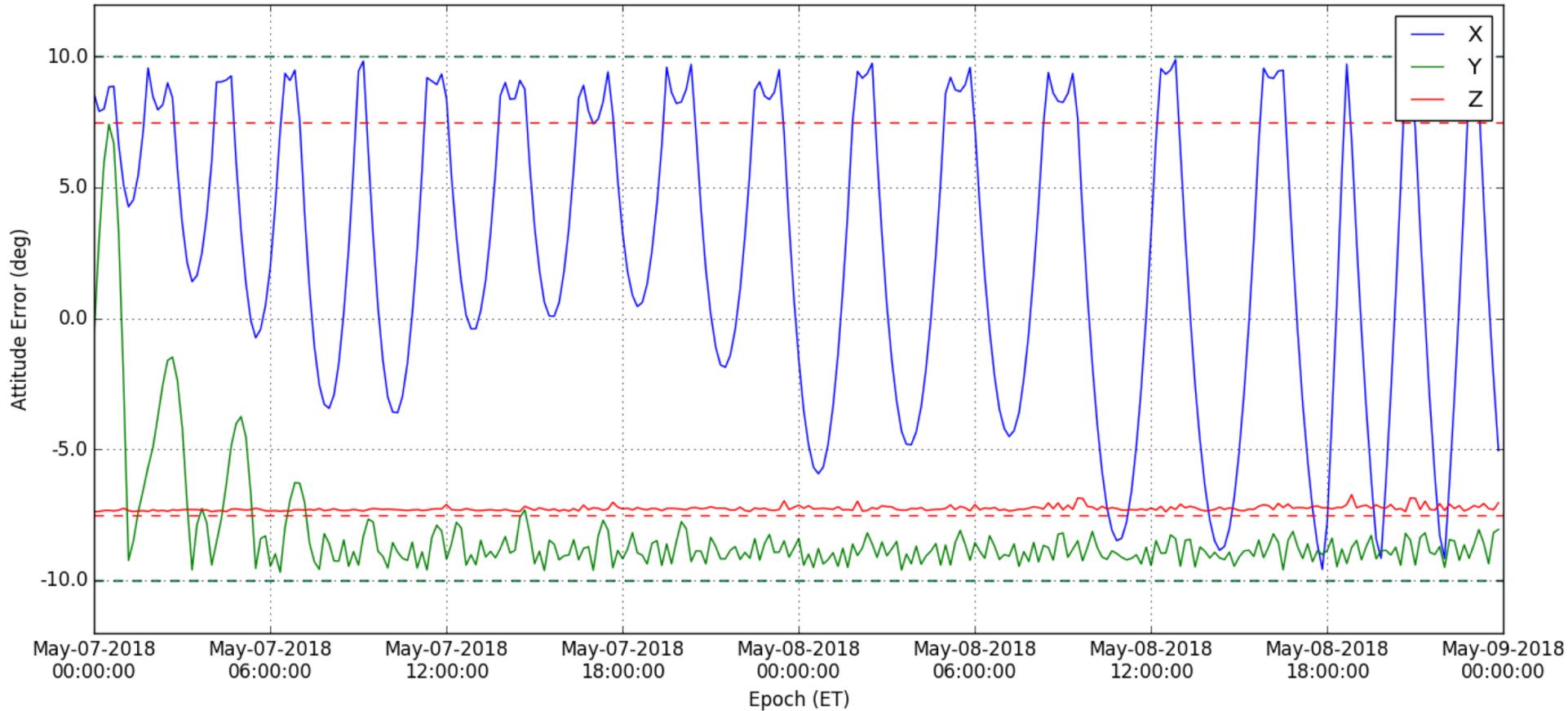
- *A priori* thruster models updated from pre-launch to estimated values prior to TCM-3 DCO
 - No change to OD filter configuration
- *A priori* model change resulted in a 1σ shift in entry interface point, significant reduction in propagated solution uncertainty
 - Uncertainty proportional to estimated thrust magnitude scale factors



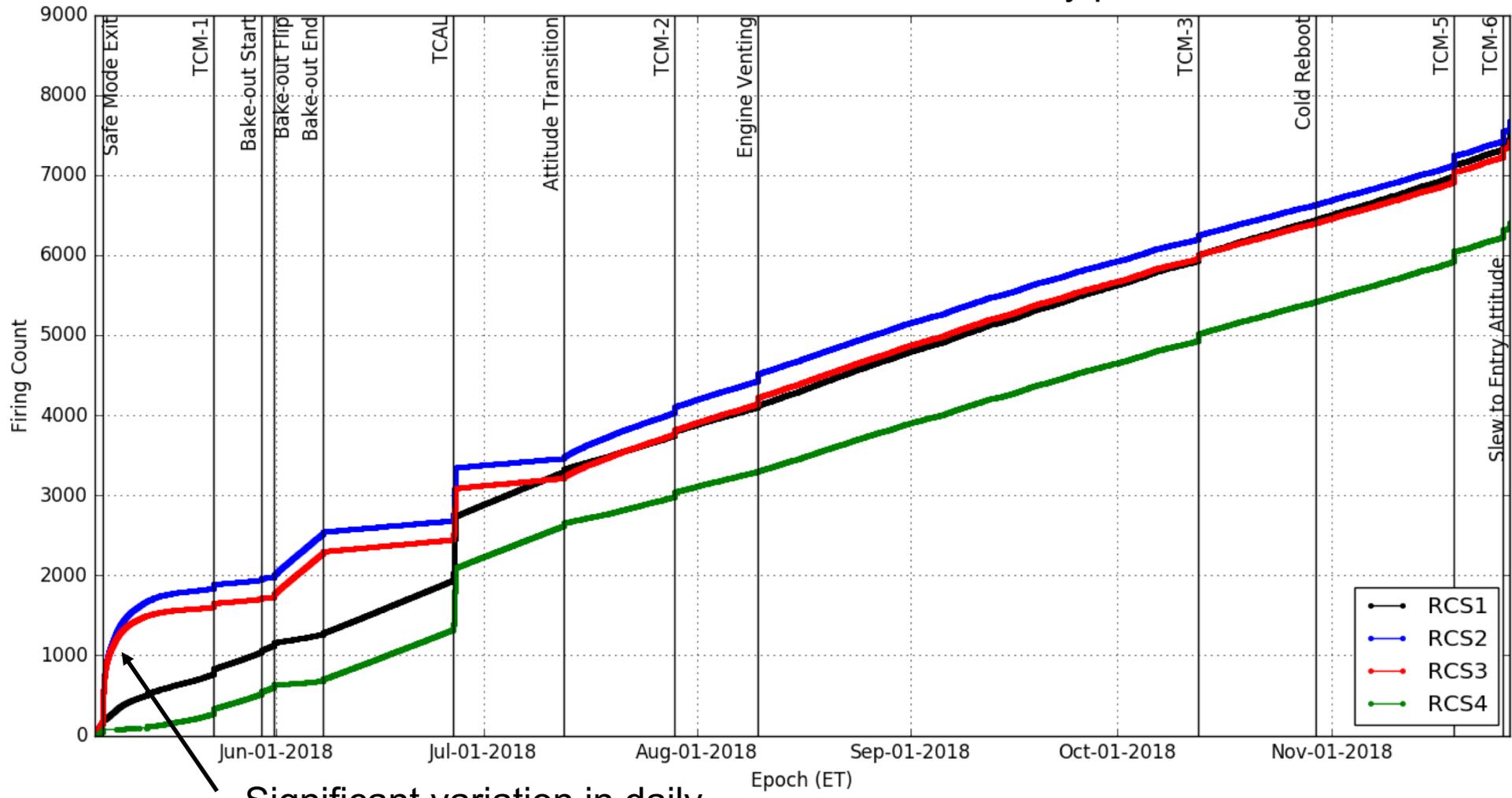
- Proper characterization of unbalanced RCS thrusters paramount to successful landing
- TCAL designed to optimize full thrust vector observability, but pulse trains not representative of nominal cruise deadbanding
 - Improved knowledge of thrust magnitude
 - Limited utility in thrust vector offset determination
- Empirical trending to recent small force telemetry combined with estimated corrections to nominal thruster models:
 - Produced stable and statistically consistent OD solutions
 - Predicted spacecraft trajectory exceptionally well

- Thank you to:
 - The entire InSight Navigation and Guidance and Control teams for all their hard work. Special thanks to Tom Kennedy, Dale Howell and Dave Eckart of the G&C team.
 - The JPL Navigation Advisory Group for their guidance and advice.
- Special thanks to Tim McElrath (JPL) for sharing his expertise and experience in dealing with the small forces.
- The work described in this paper was carried out at the Jet Propulsion Laboratory, California Institute of Technology, under a contract with the National Aeronautics and Space Administration.
- © 2019 California Institute of Technology. Government sponsorship acknowledged.

Backup - Attitude Errors During Heavy Outgassing

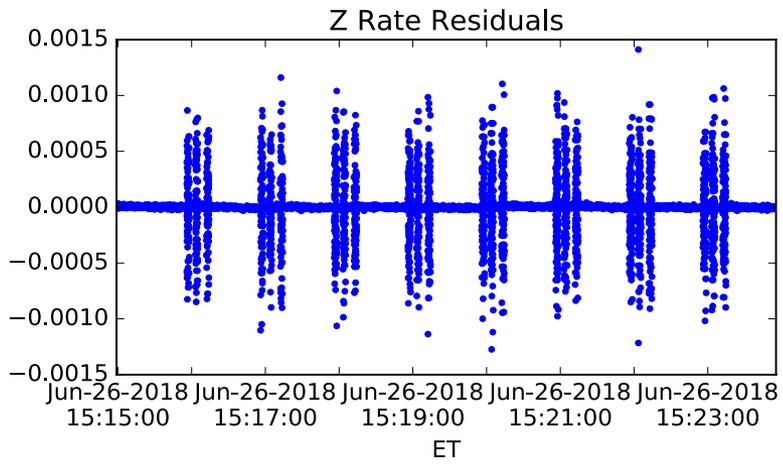
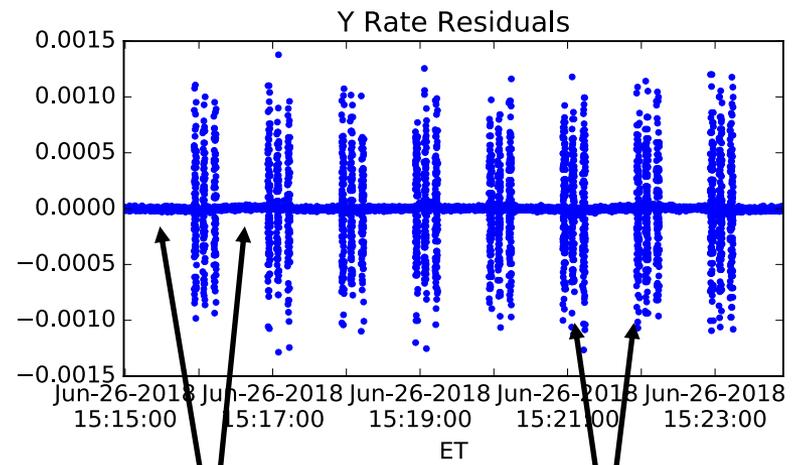
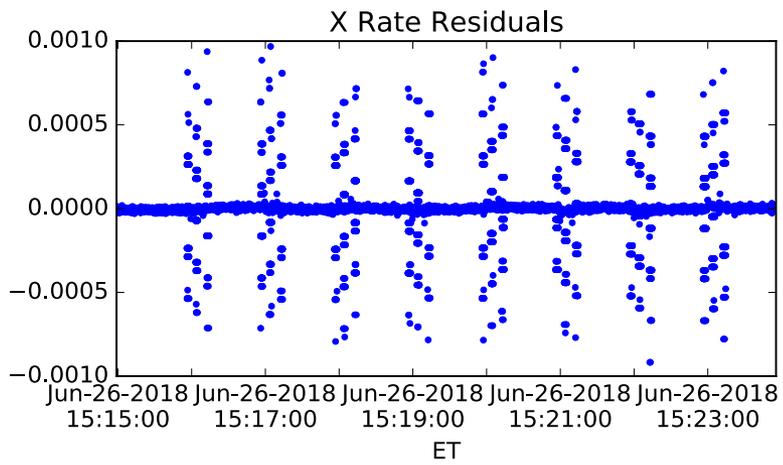


Daily variation < 0.5 mm/sec
over 1 day prediction



Significant variation in daily predictions due to outgassing

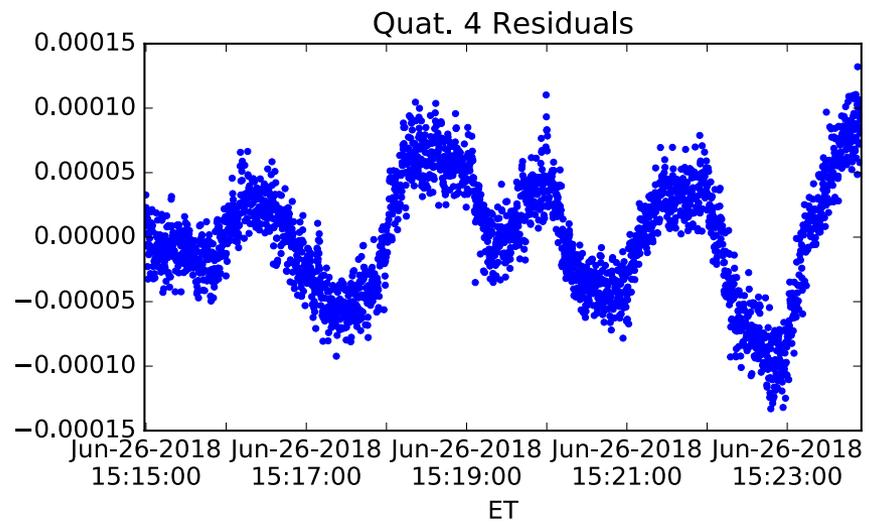
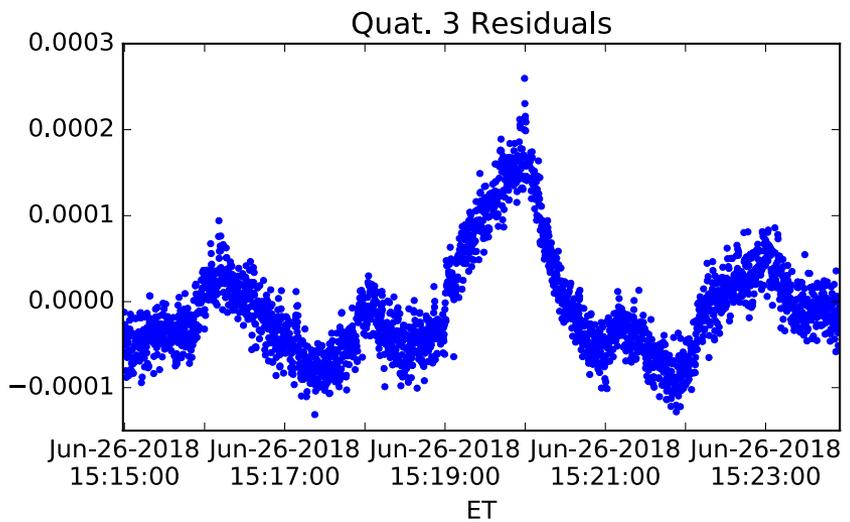
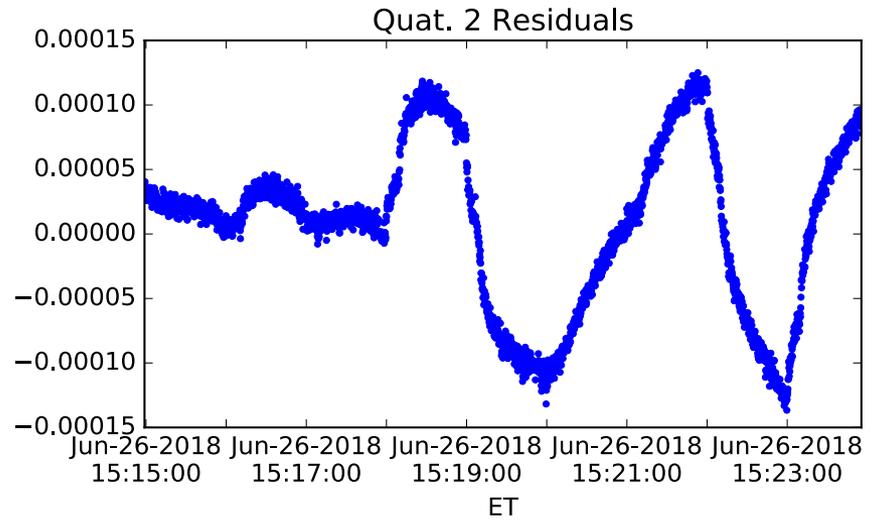
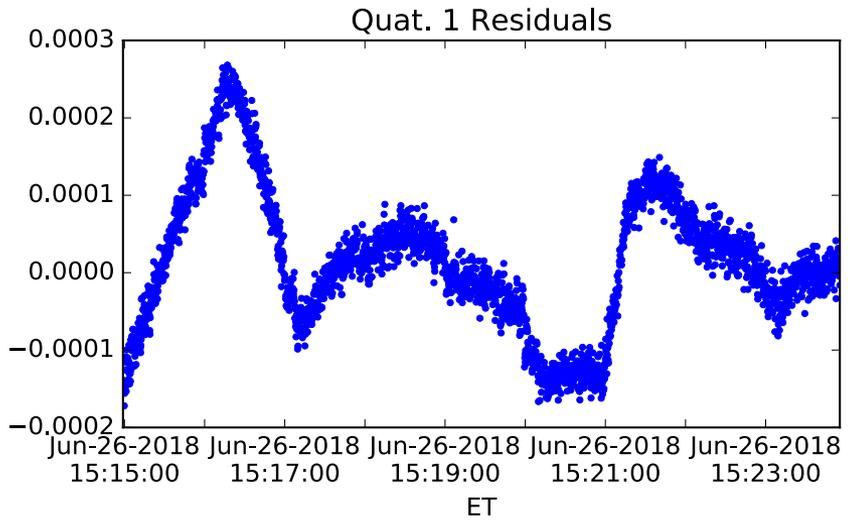
Backup: TCAL Results – Angular Rate Postfit Residuals



Low-rate
channelized
telemetry

High-rate
MIMU
telemetry

- Systematic trends consistent with star tracker measurement errors



- Statistically consistent with 2-way X-band Doppler

