

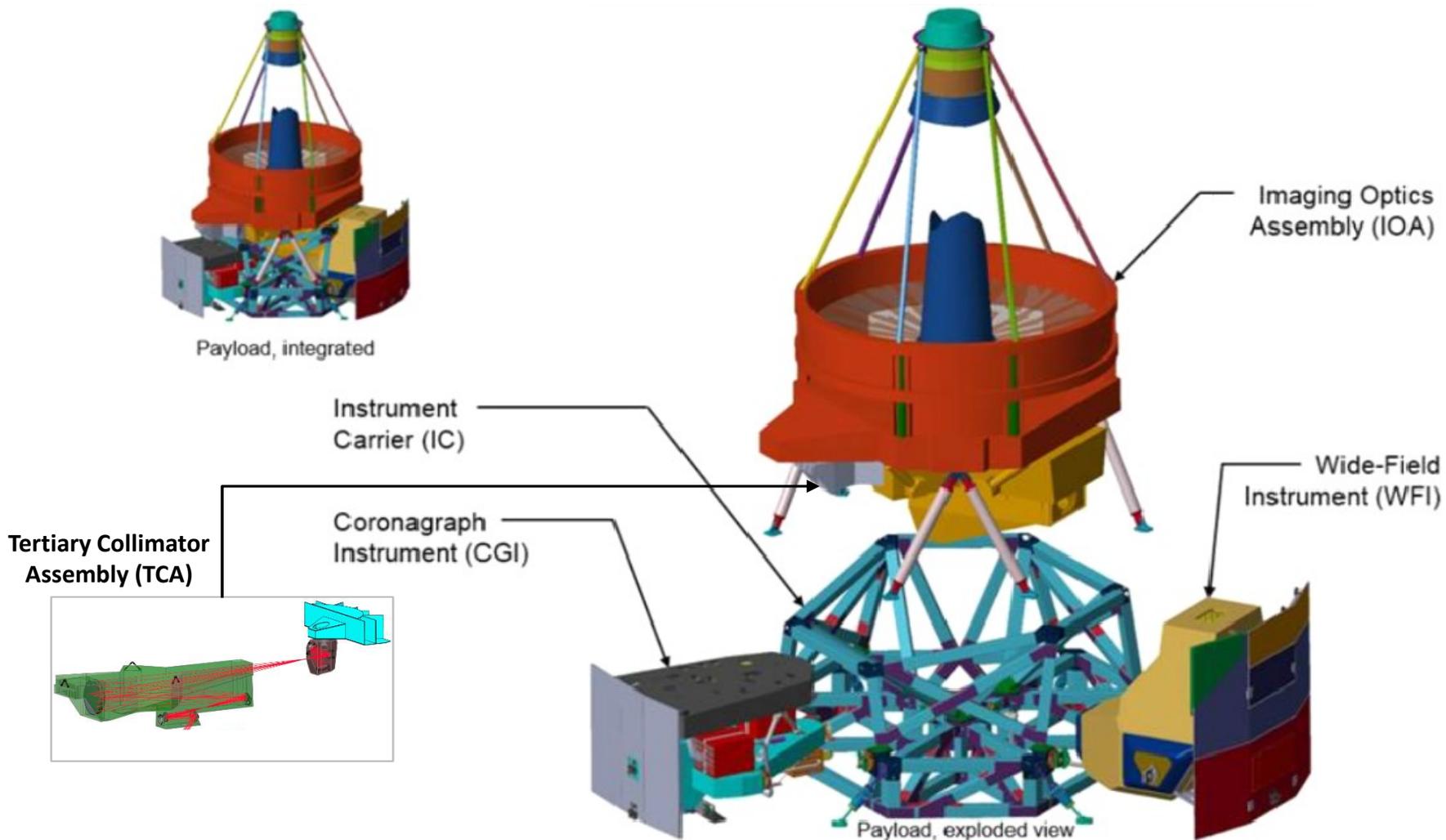


The WFIRST Coronagraph Instrument Optical Design Update

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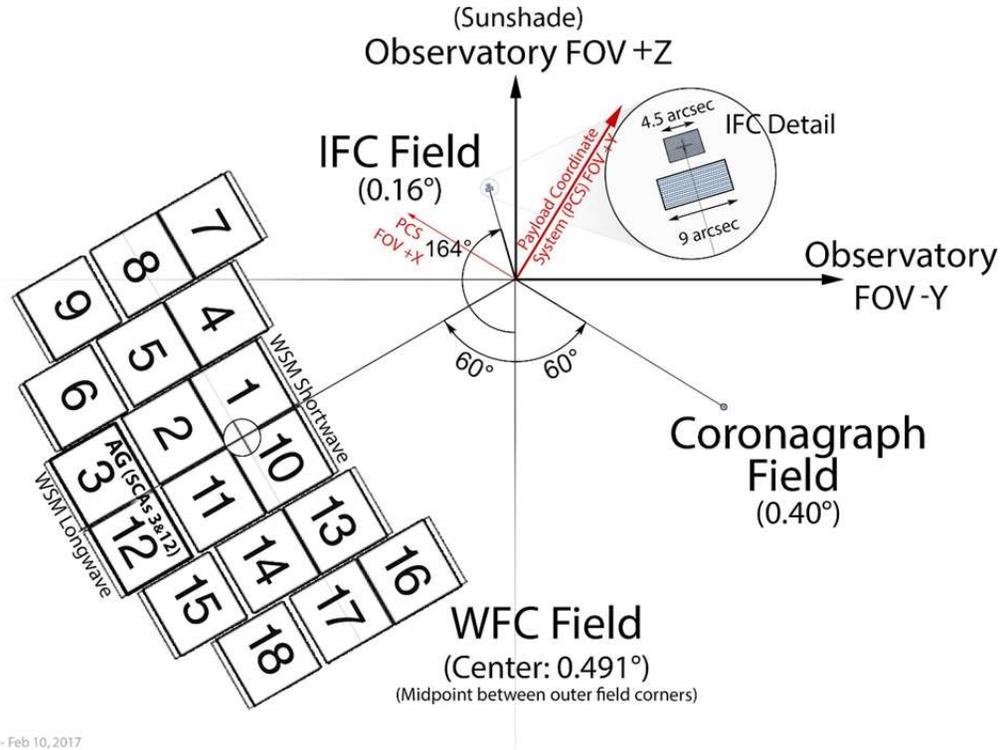
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August 8, 2017

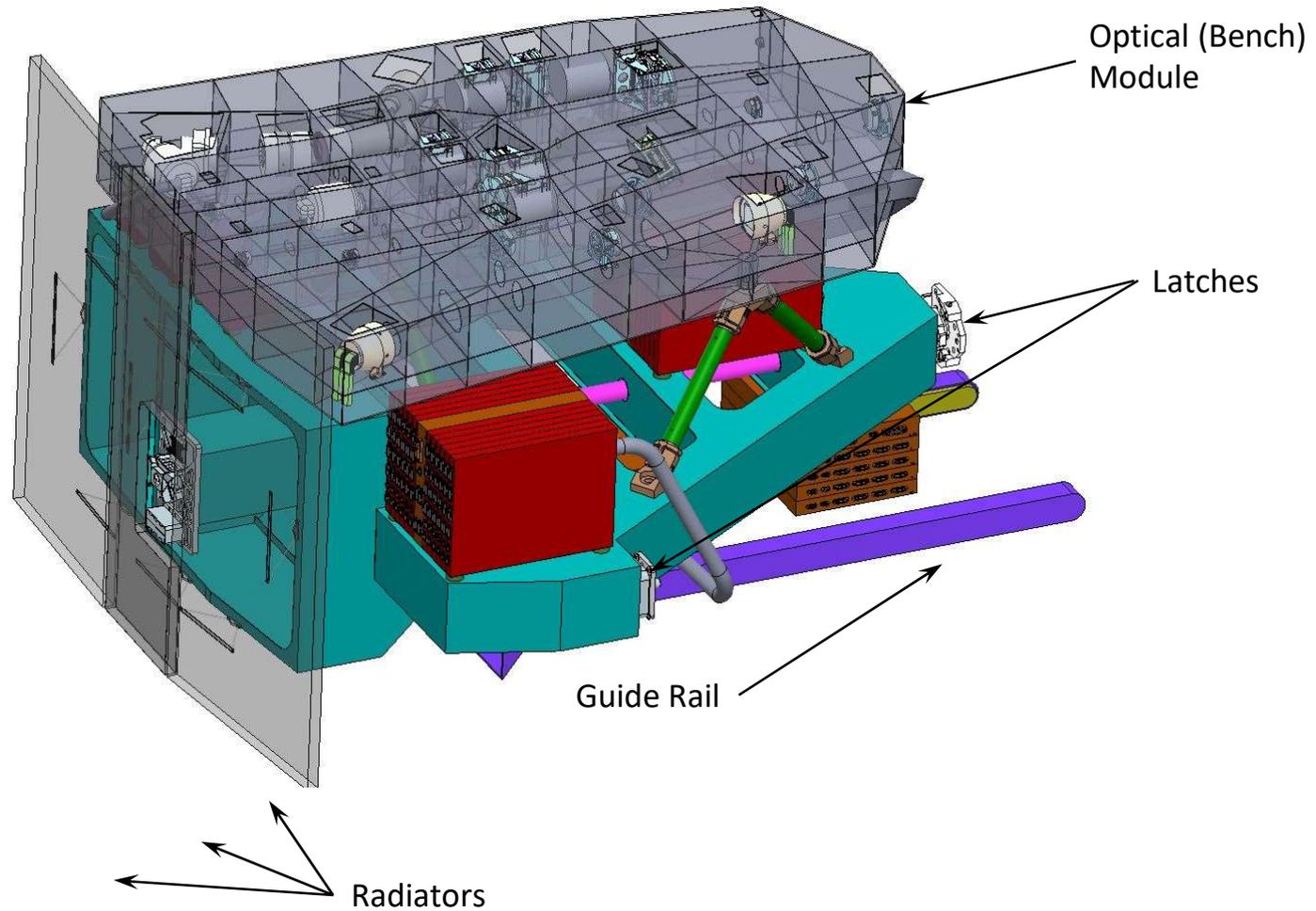




WFIRST Instrument Field of View Layout Sky Projection Phase-A SRR Design (v.7.6.8)



bap - Feb 10, 2017

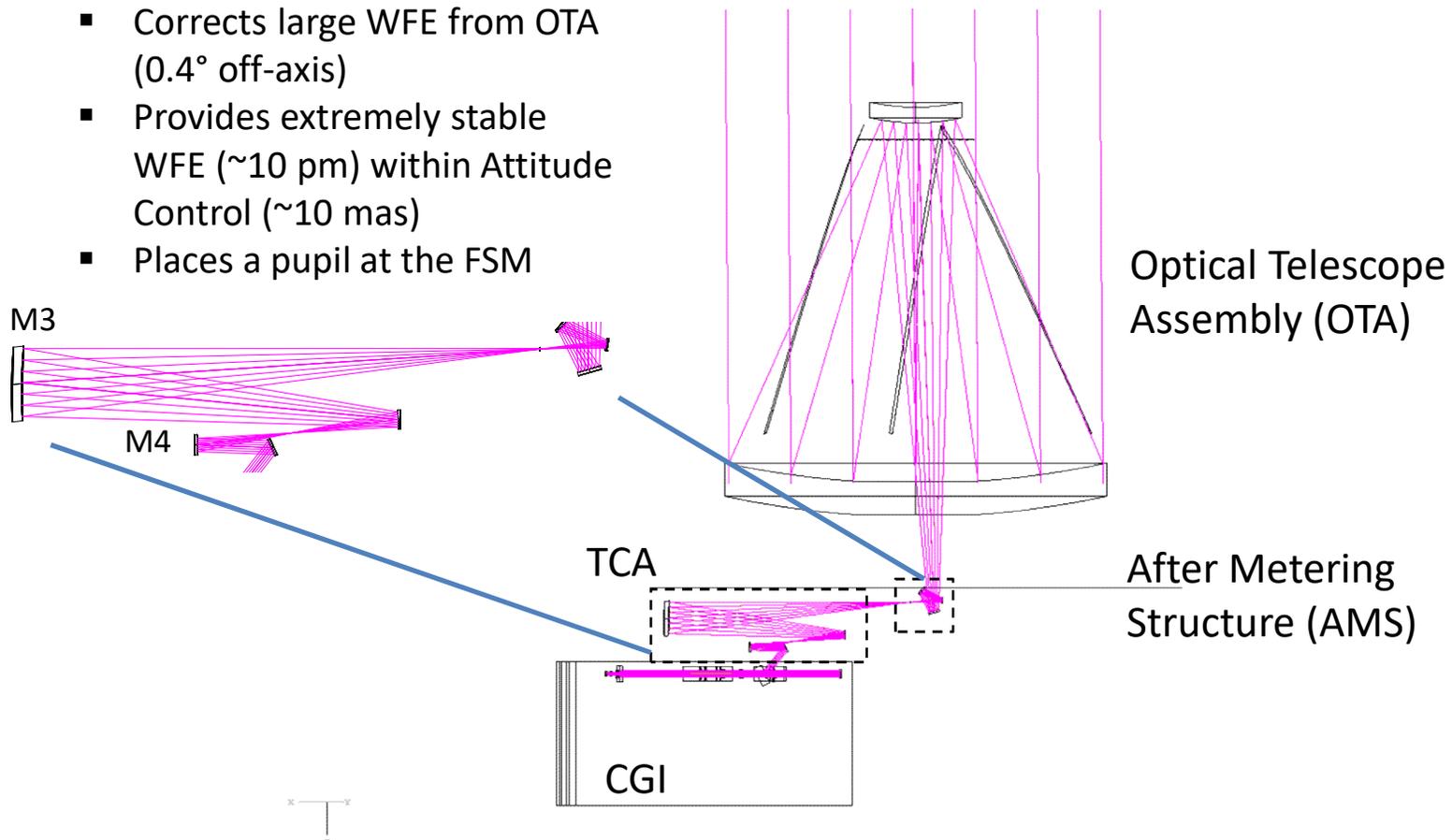


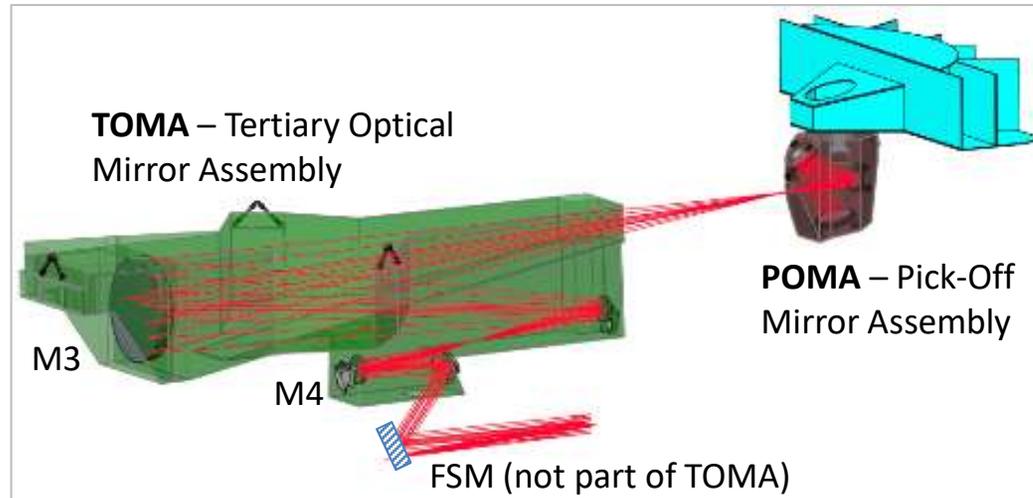


Tertiary Collimator Assembly (TCA)

Tertiary Collimator Assembly - TCA

- Corrects large WFE from OTA (0.4° off-axis)
- Provides extremely stable WFE (~10 pm) within Attitude Control (~10 mas)
- Places a pupil at the FSM

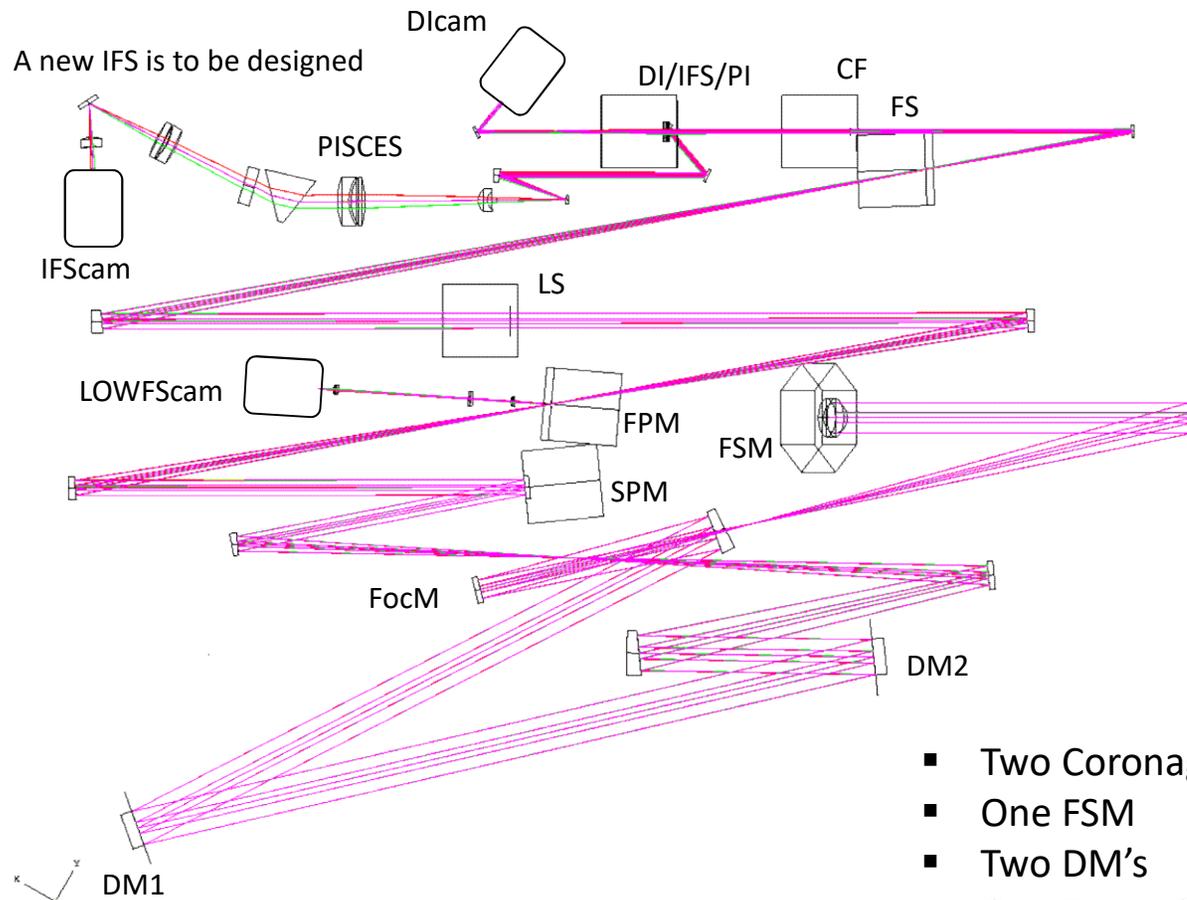




- TCA splits into two assemblies, POMA and TOMA
- TOMA and POMA are attached to After Metering Structure (AMS) of the Optical Telescope Assembly (OTA)
- Coronagraph pick-off mirrors increases from two to three (as a result of Wide Field Instrument's M3/F1 trade)
- M3 and M4 are re-optimized to simple conic surfaces
- Exit pupil is 40 mm (was 46 mm), more margin for FSM optic
- Exit pupil extends to FSM (was 200 mm short of it)



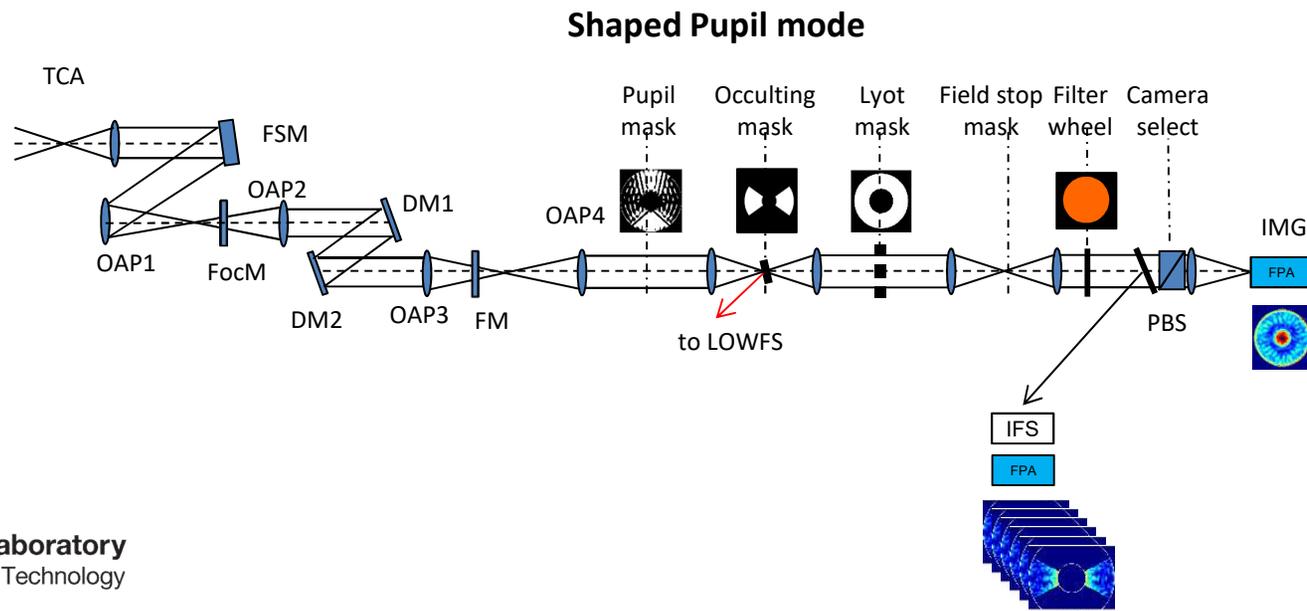
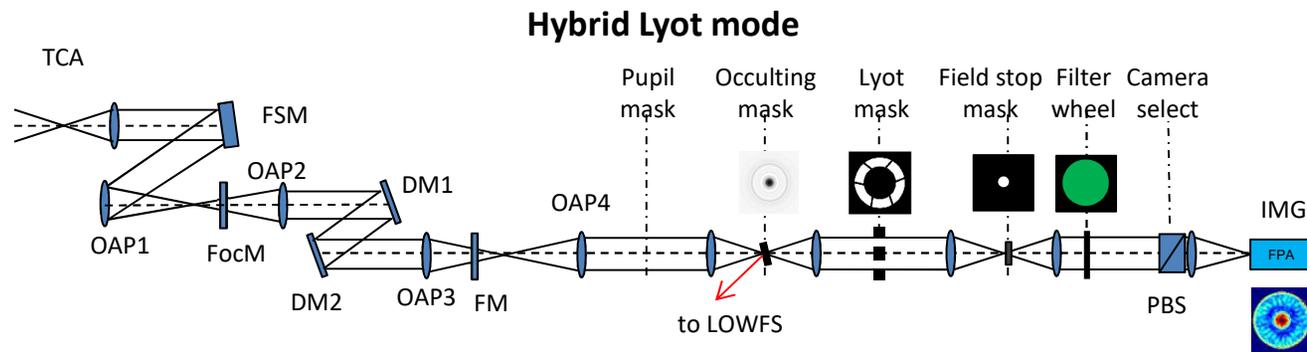
CGI Optical Layout



- Two Coronagraph Architectures
- One FSM
- Two DM's
- One Focus Correction Mirror
- Six wheel mechanisms
- Three CCD cameras



Operation Modes

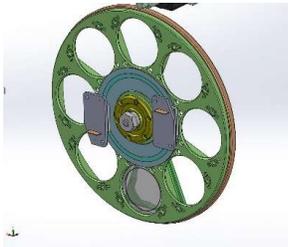




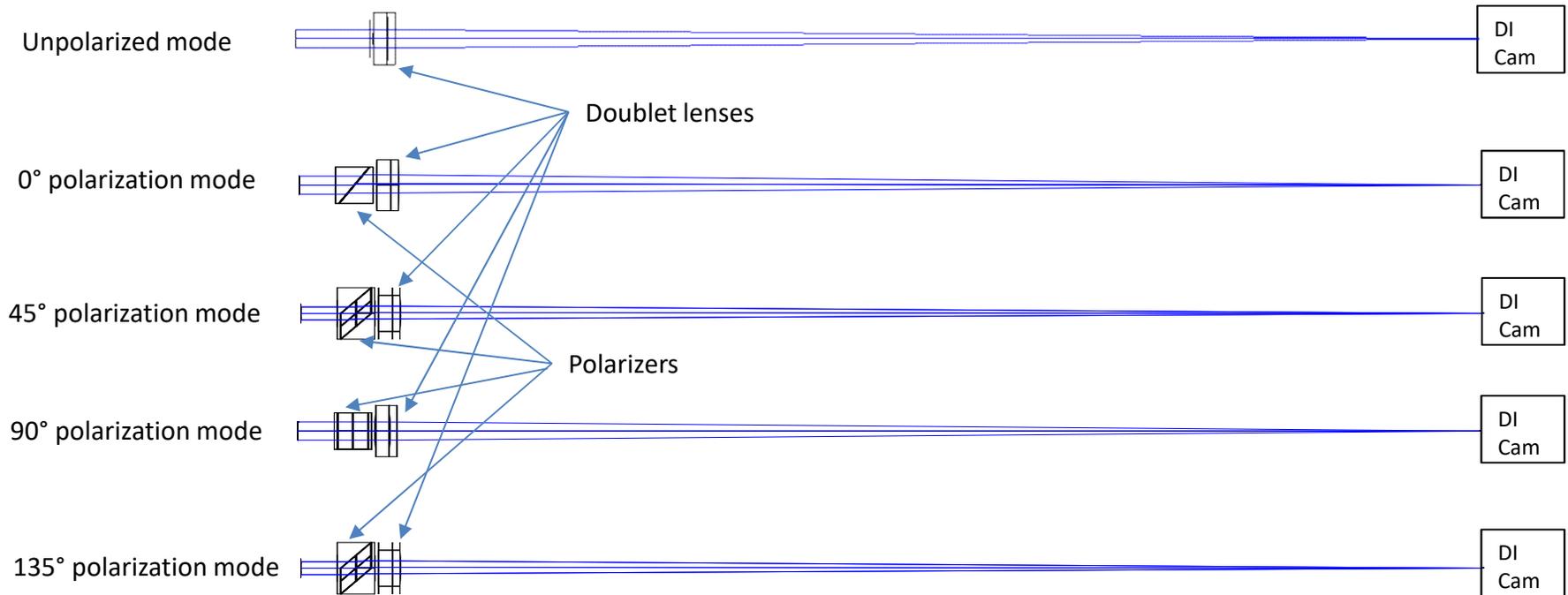
- CGI starts from FSM
- Eliminates several fold mirrors, only one remains
- Adds un-polarized mode in Direct Imaging Channel
- Added 45° and 135° polarized imaging modes
- PISCES is serving as a place holder for IFS
 - An IFS is being designed in Phase A according to L2/L3 Requirements



Lenses and polarizer/lens subassemblies on Camera Select wheel (DI/IFS/PI)



- Un-polarized image
- Linearly polarized images (0°, 45°, 90°, 135°)
- Pupil image (not shown below)
- Four defocused images (not shown below)

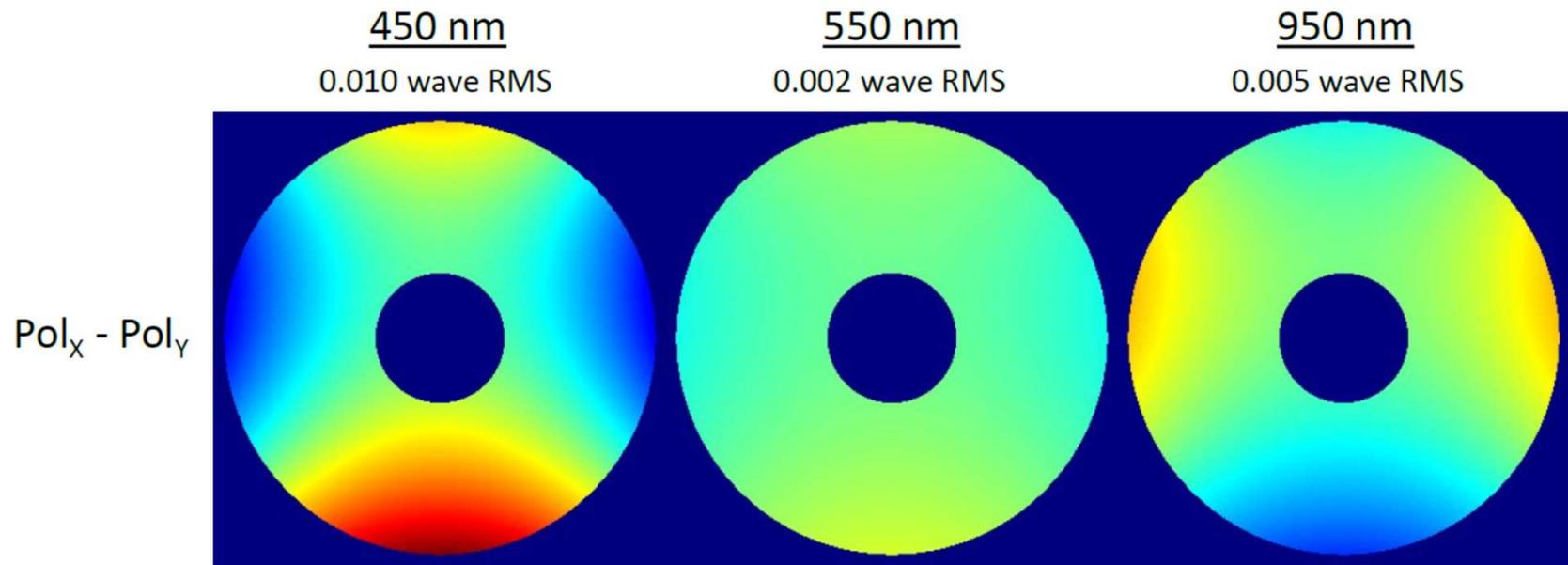




Design Specifications		Value	Unit
WFE (on CGI axis)	After SM	6380	nm (rms)
	After M4	7	
	At FPM	7	
Δ WFE (100 mas off CGI axis)	After M4	30	pm (rms)
Imaging pixel plate scale		0.02	arcsec
Imaging FOV (full)	without masks	10	arcsec

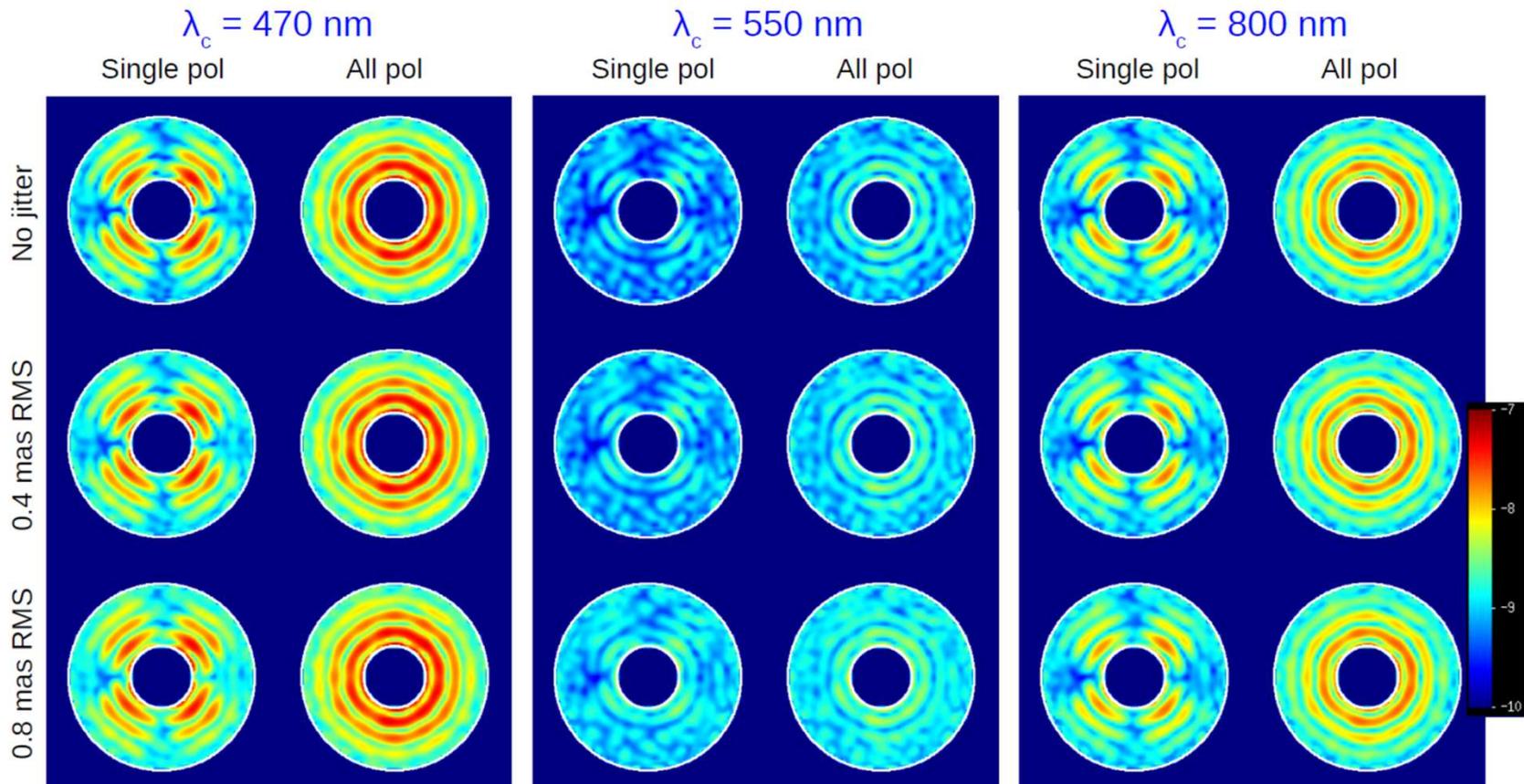


Polarization-Induced Phase Errors: Differences



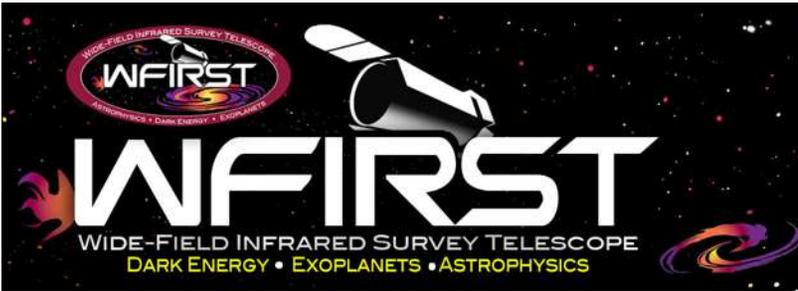
- Linearly polarized light was input to the telescope at -45° and $+45^\circ$ to represent unpolarized light
- Light from each angle was analyzed with X and Y linear polarizers at the pupil, producing 4 maps: $Pol_{X,-45^\circ}$, $Pol_{X,+45^\circ}$, $Pol_{Y,-45^\circ}$, $Pol_{Y,+45^\circ}$

HLC with Polarization, Jitter & 1 mas Star



“All pol” mode provides sufficient contrast and $\sim 2x$ gain in throughput except at 470 nm, so we added an un-polarized imaging mode.”

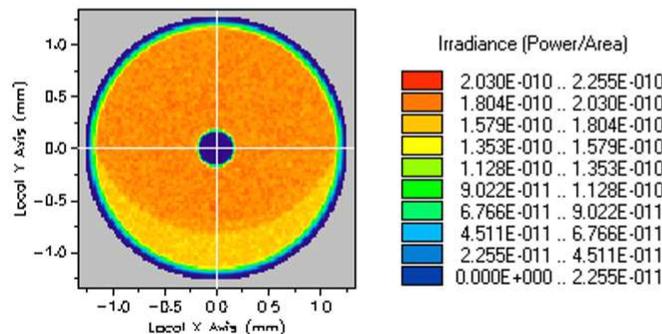
Stray Light Analysis for OMC Testbed



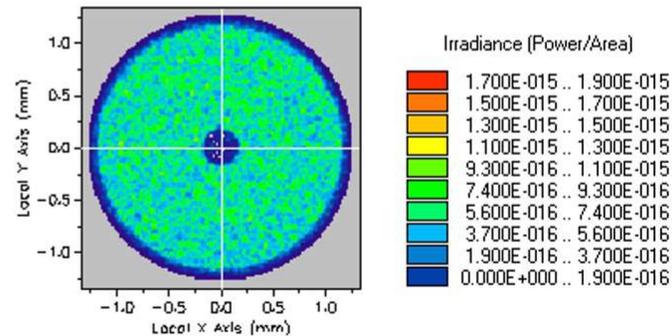
- Single level optical surface scatter is the principal source of stray light for rays with an OPD less than 5.5 μm
 - The small opening in the field stop mask means that only scattered rays with propagation directions very near the source specular rays reach the detector.
- Second level scatter events introduce path errors in excess of 5.5 μm .

Coherent

$|\text{OPD}| \leq 5.5 \mu\text{m}$
Integrated Flux: $8.35\text{e-}9$



$|\text{OPD}| > 5.5 \mu\text{m}$
Integrated Flux: $2.85\text{e-}15$



Incoherent
 $2.85\text{e-}15 / 0.055 = 5.2\text{e-}14$

Mask/apertures in use:

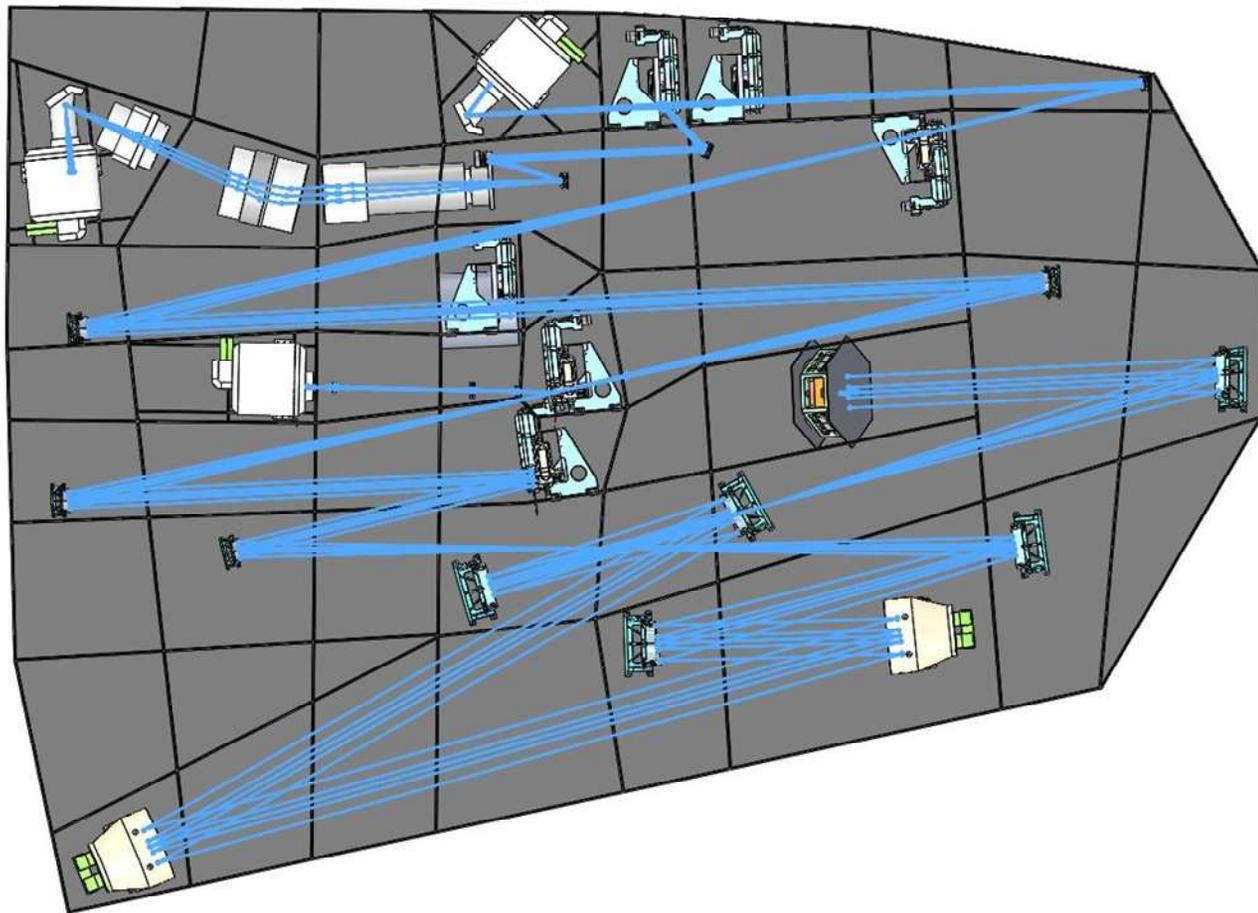
- Pupil mask, lyot stop mask, occulting disk, field stop aperture
- There are no direct or ghost-only paths to the detector



- TCA (POMA + TOMA) attached to AMS for stable interface with OTA
- Conic surfaces for M3 and M4
- Pupil at FSM
- Smaller beam print at FSM
- Only one fold mirror
- Un-polarized imaging of higher throughput
- Four polarized imaging modes
- Stray light from optical surfaces not an issue

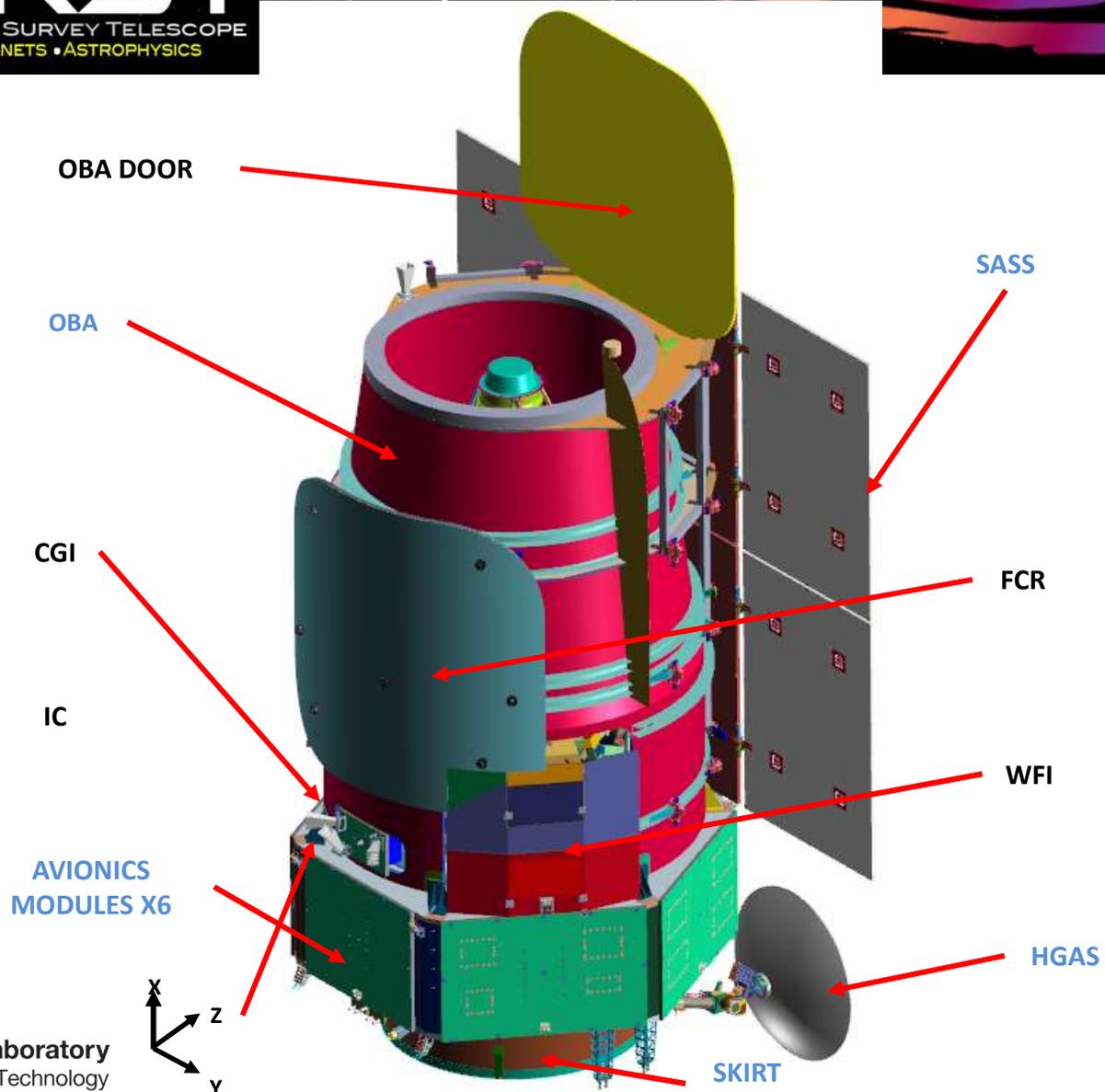


- Backup Slides

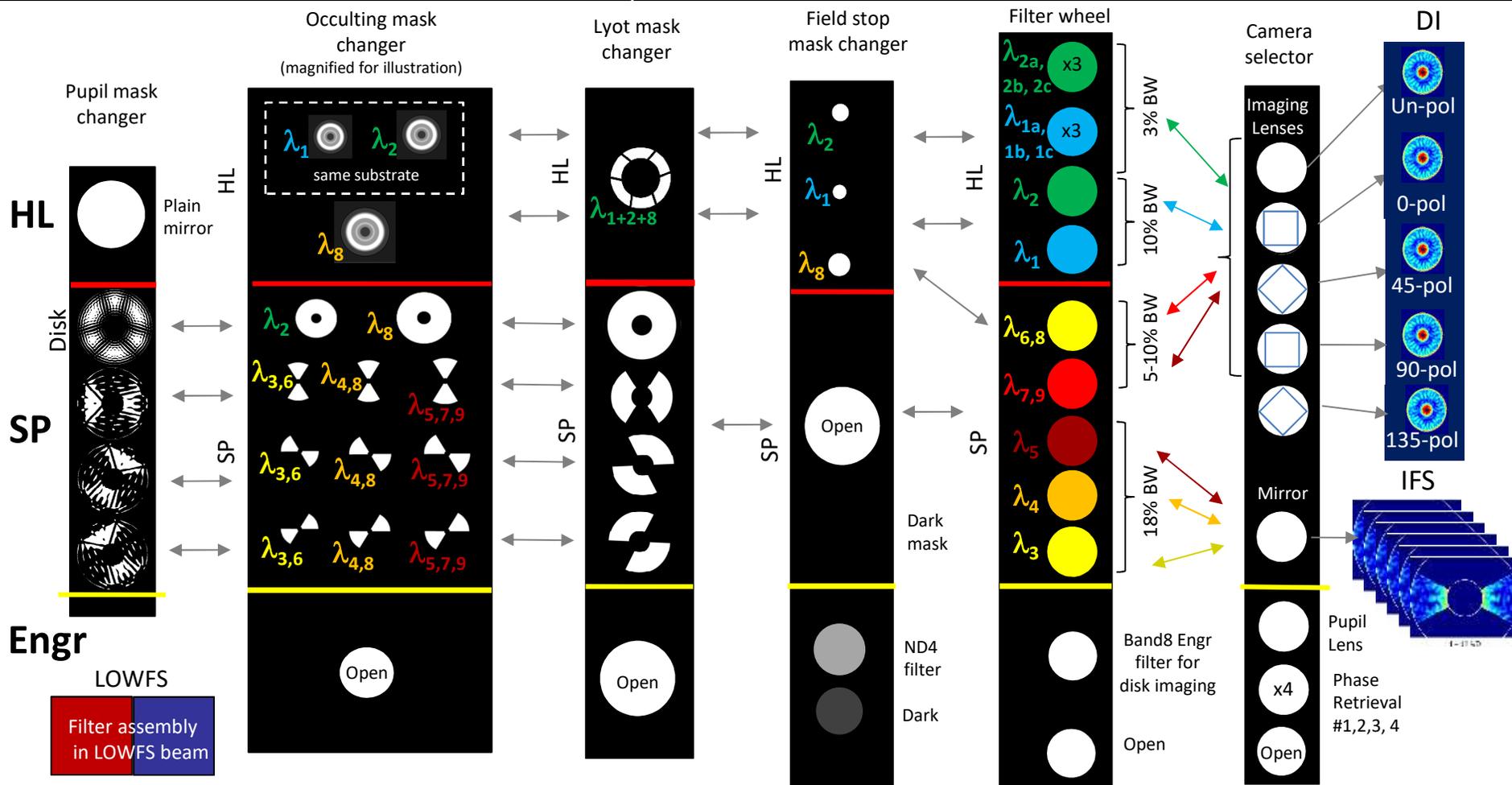




WFIRST Spacecraft Architecture



CGI Filter Wheel Populations



$\lambda_1 = 508\text{nm}$

$\lambda_2 = 575\text{nm}$

$\lambda_3 = 660\text{nm}$

$\lambda_4 = 770\text{nm}$

$\lambda_5 = 890\text{nm}$

$\lambda_{1a} = 491\text{nm}$

$\lambda_{1c} = 524\text{nm}$

$\lambda_{2a} = 555\text{nm}$

$\lambda_{2b} = 594\text{nm}$

$\lambda_6 = 661\text{nm}$

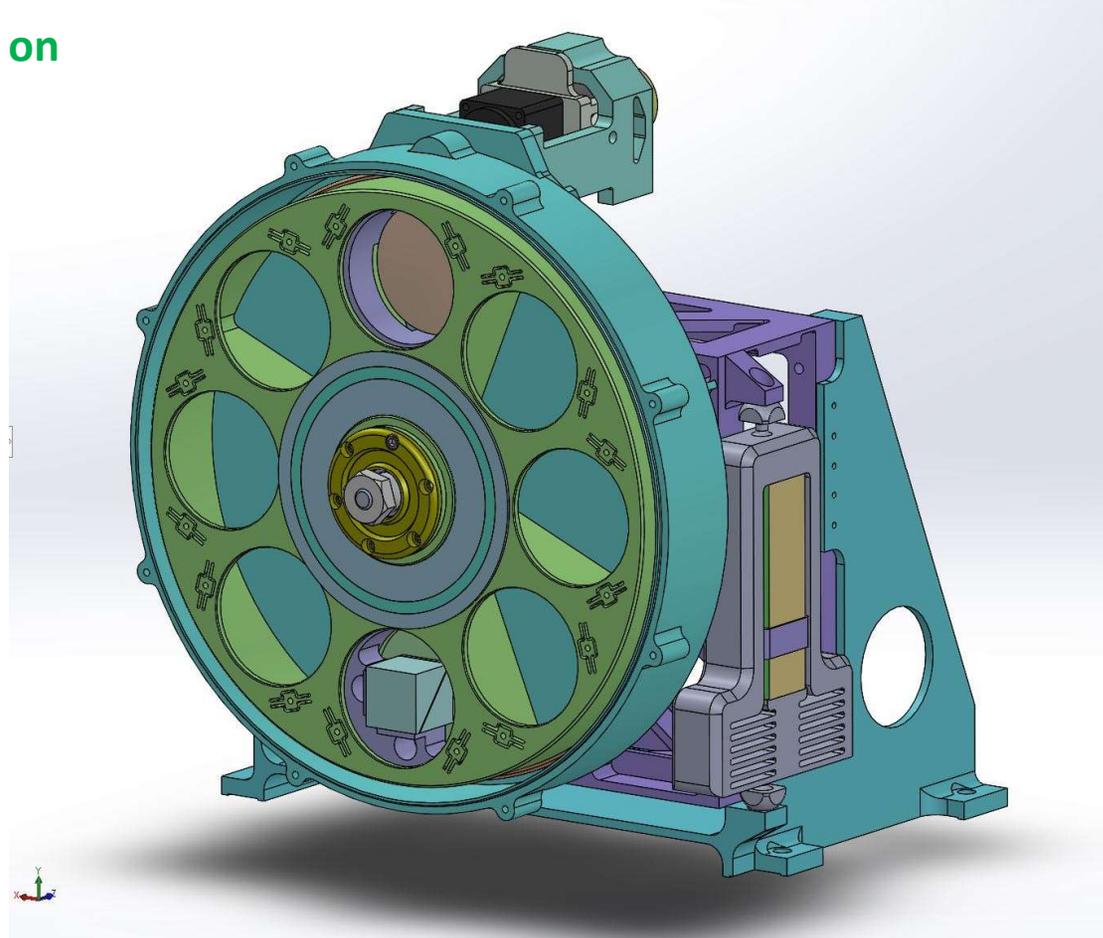
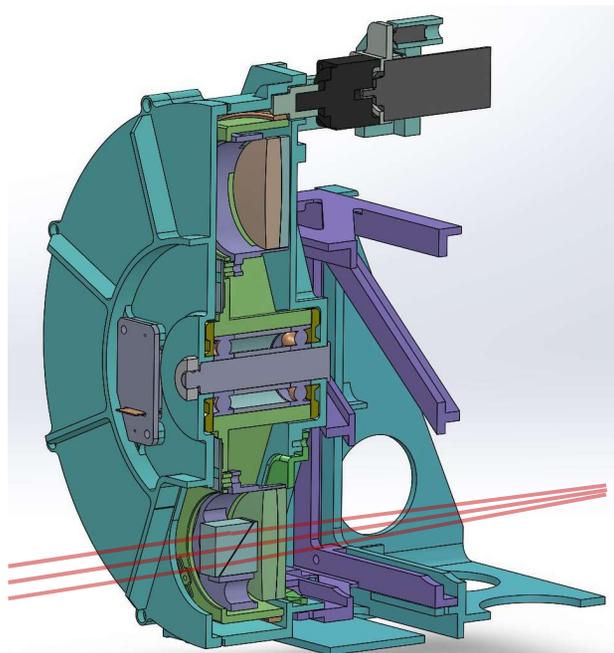
$\lambda_8 = 721\text{nm}$

$\lambda_7 = 883\text{nm}$

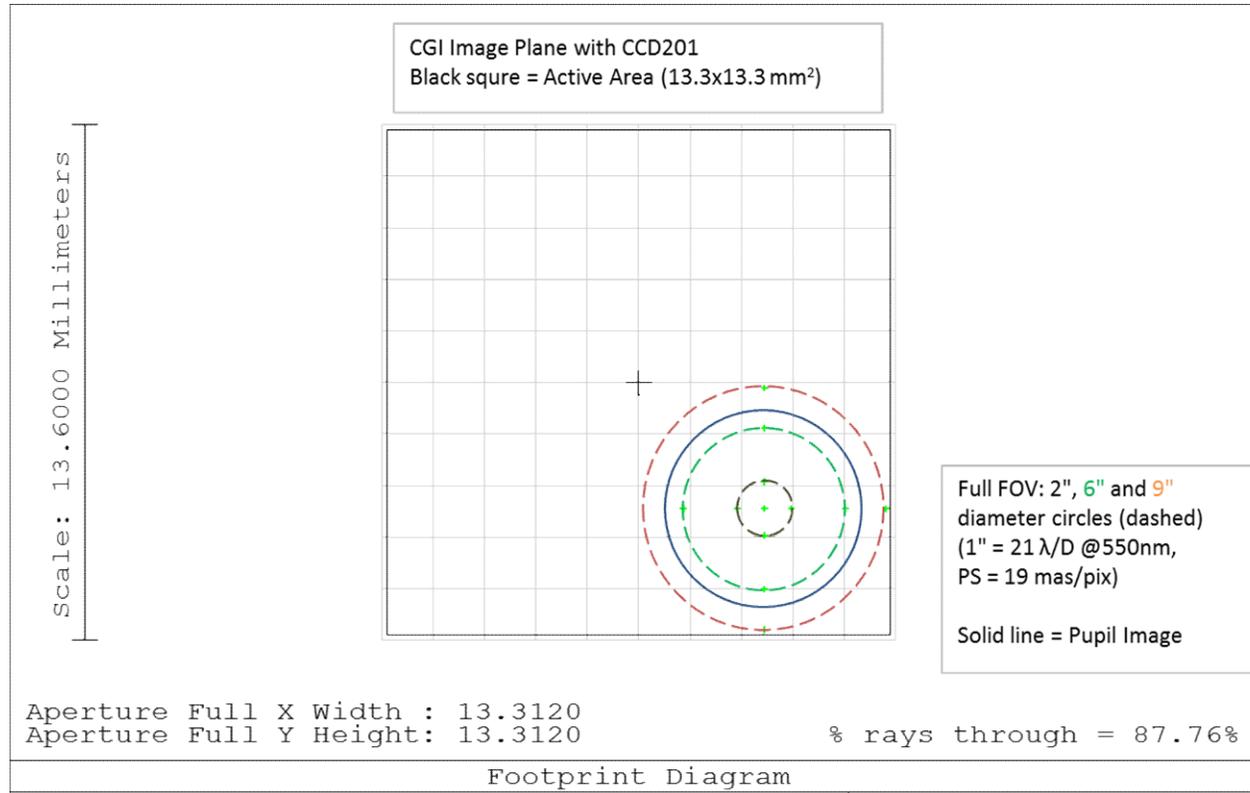
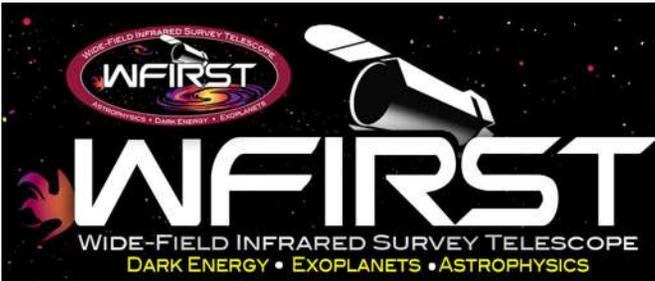
$\lambda_9 = 950\text{nm}$



Polarizer and lens fits in a slot on
Camera Select wheel



Proposed Placement of Image on CCD



- Image in the quadrant of fewest charge transfers
- Least impacted by traps

Wavefront Control Modeling



- Electric Field Conjugation was used in these cases, with regularization and using field weights applied. PROPER was used for propagation. The computed wavefronts were used as “measured” wavefronts (i.e., exact knowledge).
- The **image** in a single polarization channel is the sum of the **intensities** of the -45° and $+45^\circ$ wavefronts in that channel (e.g., $\text{Pol}_x = \text{Pol}_{x,-45^\circ} + \text{Pol}_{x,+45^\circ}$). Without polarization splitting, the image is the sum of intensities from both channels ($\text{Pol}_x + \text{Pol}_y$).
- The **measured wavefront** in a single polarization channel is the average of the -45° and $+45^\circ$ wavefronts in that channel. Without splitting, it is the average of the wavefronts in both angles in the X and Y channels (four wavefronts in all).
- When running wavefront control (EFC) for one polarization channel (X or Y), the “measured” wavefront is computed using the mean wavefront of the two angles to provide a DM solution that is then evaluated by computing the fields for both angles separately and then adding their intensities together.
- The worst case will be a solution optimized for both X and Y polarizations simultaneously (equivalent to no polarization splitting). The best will be without any polarization errors. The single-channel (X or Y) result will be in-between.

