

A starshade petal error budget for exo-earth detection and characterization

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SPIE Meeting 8151
August 23, 2011

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Overview

- Build upon last year's work: development of error budget tools and strawman error budget.
- Focus on engineering requirements
- Make it easier: spin the starshade to smear out the speckles.
- Four cases:
 - TDEM starshade (32 m), 90 and 75 mas
 - THEIA starshade (40 m) 75 and 60 mas

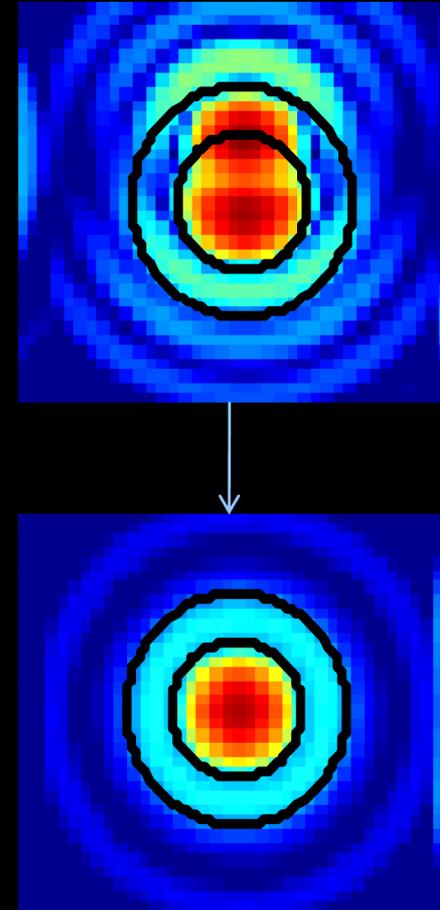


Science Requirements

- From many studies
- $\Delta\text{mag} = 26$
- IWA < 100
- Mean scatter $< 10^{-10}$
- SNR > 4
- Requires r.m.s. of speckle noise floor to be $< 10^{-11}$
- Evaluate in IWA swath, width matched to core of PSF

Spinning the Starshade

- Local errors, e.g. a displaced petal, scatter into speckles in the image plane.
- Speckles look like planets.
 - Speckle requirement is $1e-11$ contrast.
- Spinning the starshade smears the speckles into annuli.
 - Background requirement is $1e-10$.
- This leads to a 3x relaxation of requirements.
- Same requirements apply to planet detection and characterization since limited by zodi and exozodi rather than instrument.
- Spin rate: up to 12 rev/hr, limited by retargeting fuel (assumed 1 kg per 90 deg turn)

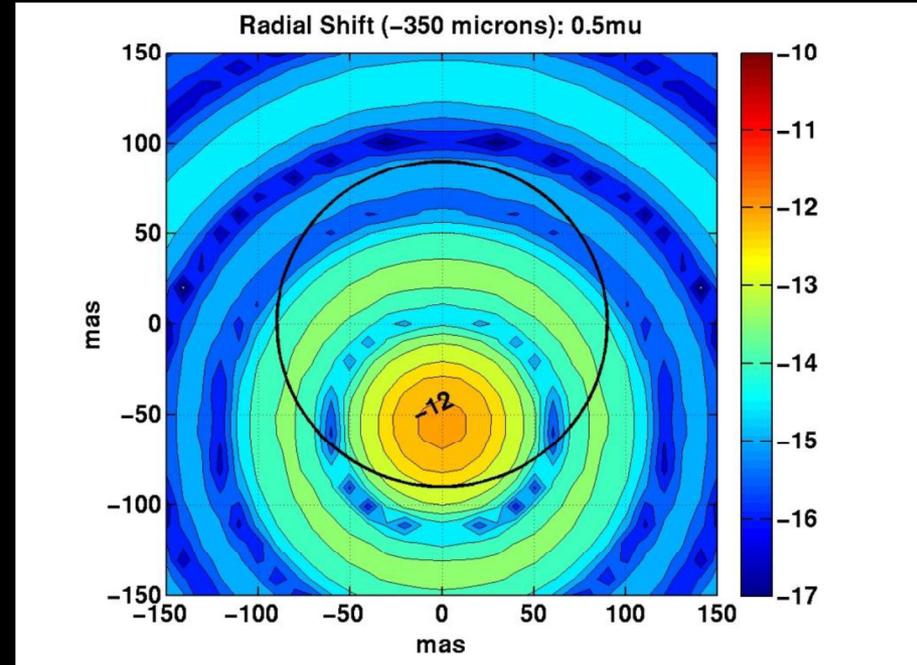
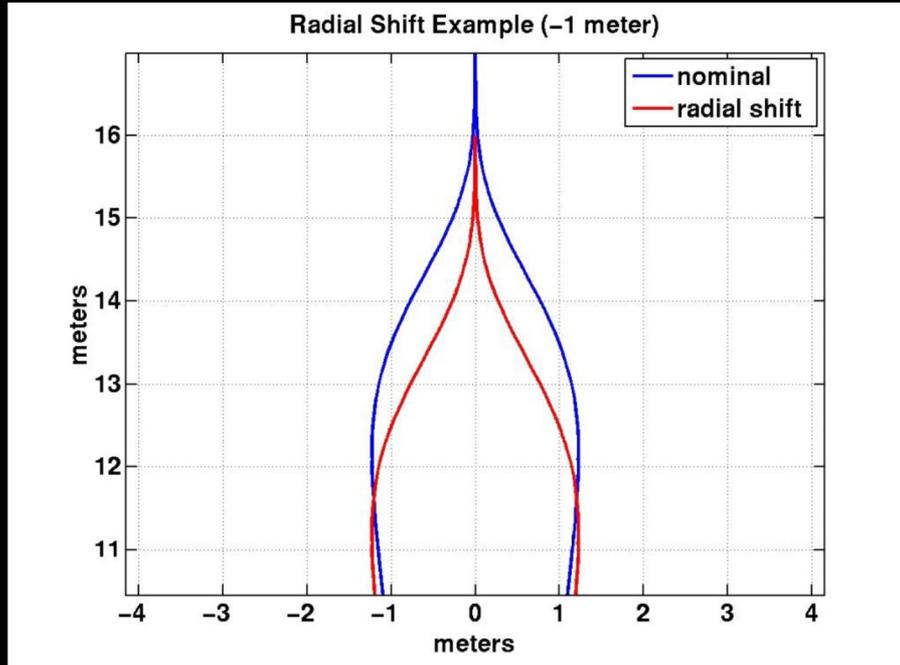




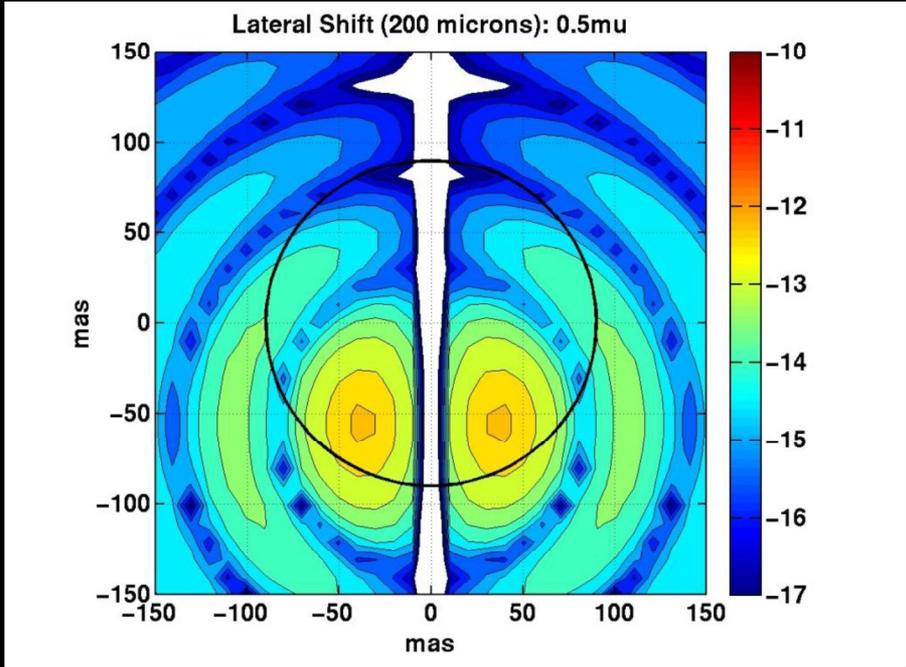
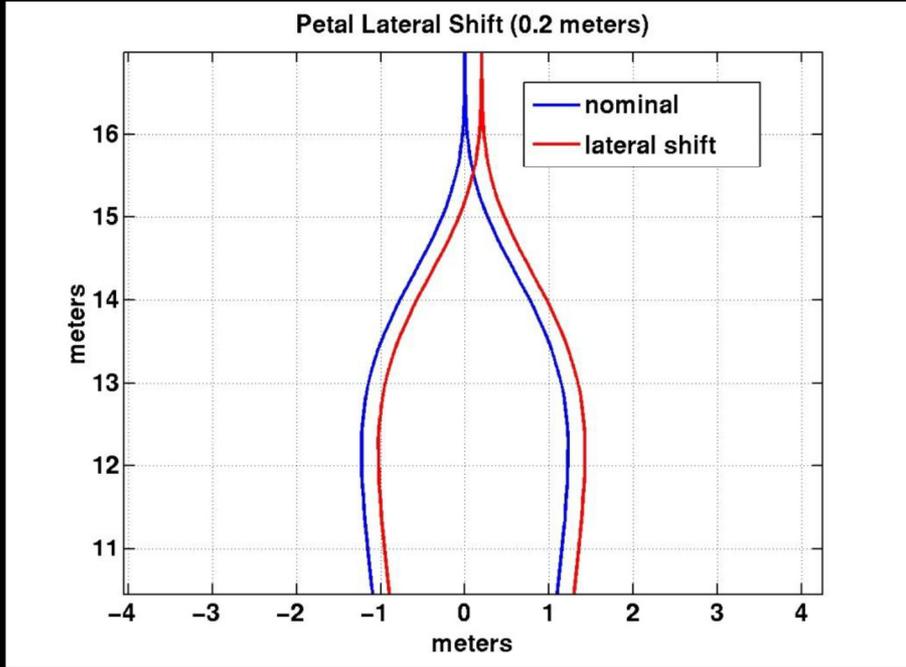
Error Budget Methodology

- Optical Models based on Fresnel propagation. Combination of analytic and Fourier-based slit calculations.
- Evaluate effect of perturbations in the image plane in a swath centered at IWA.
- Treat perturbations as independent.
- Sum up scatter from perturbations

2010 Example: Radial Shift

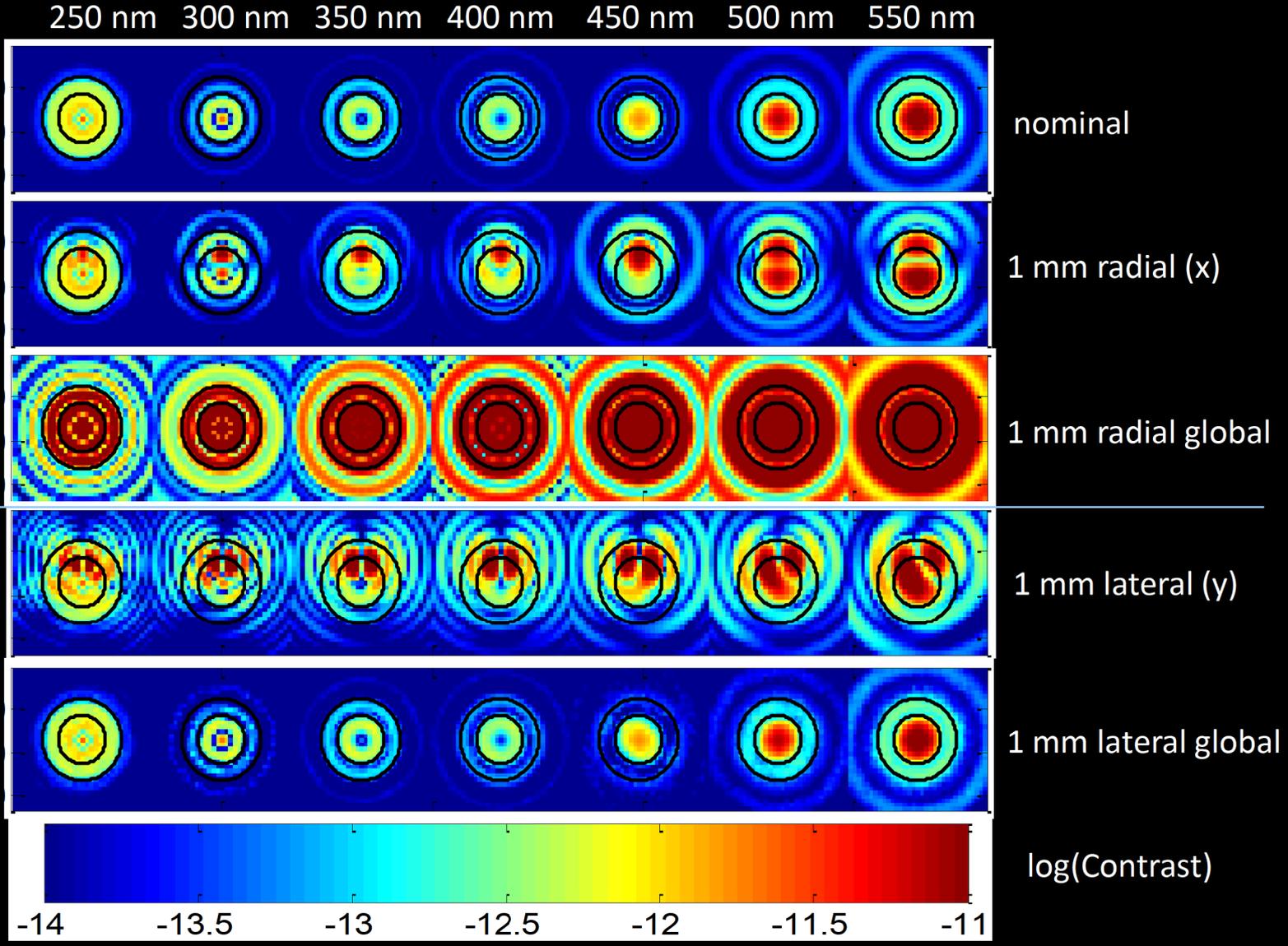


2010 Example: Lateral Shift





2010 Example: Single-Petal and Global Perturbations

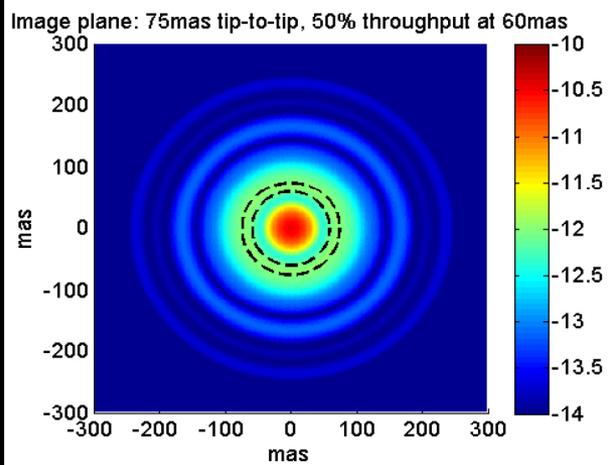
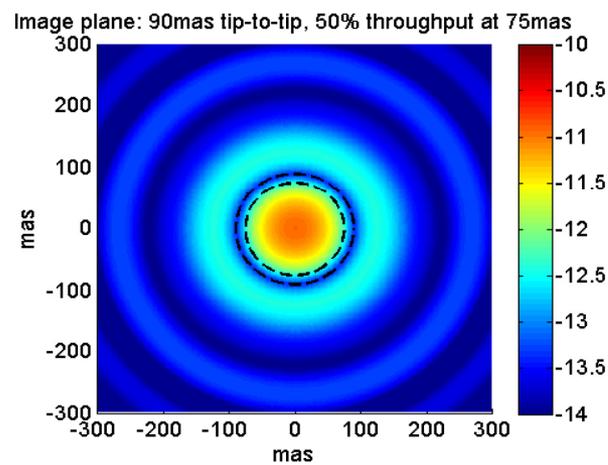
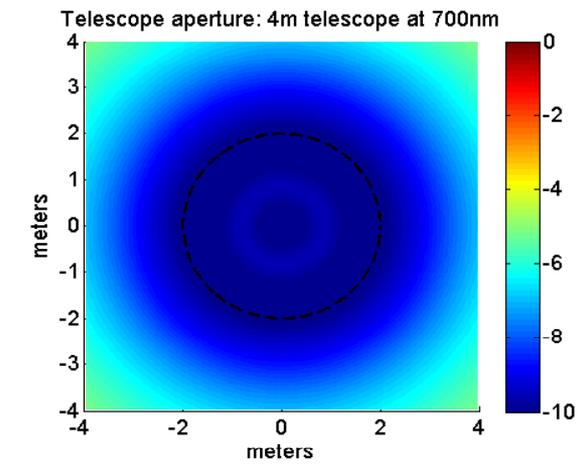
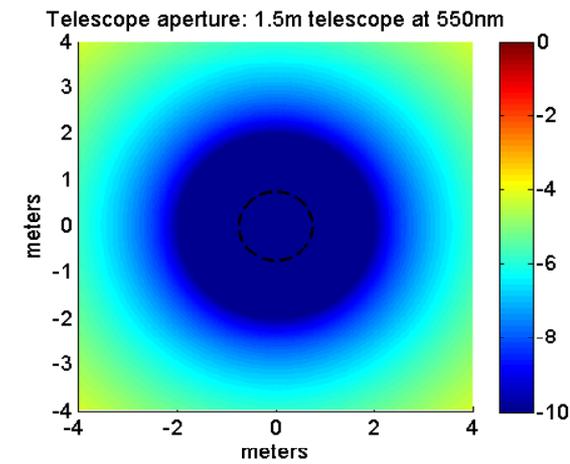
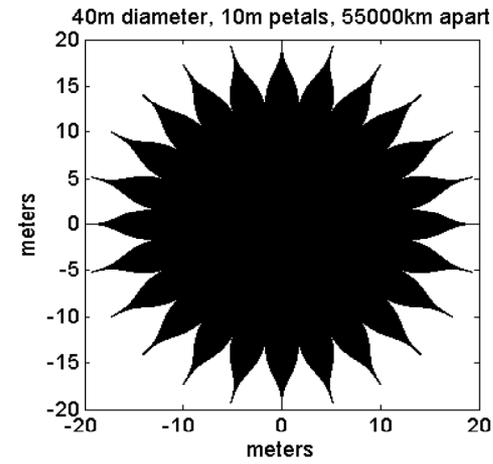
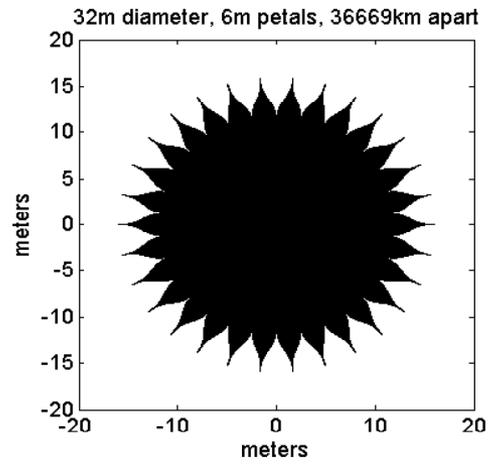




Starshade Mission Designs

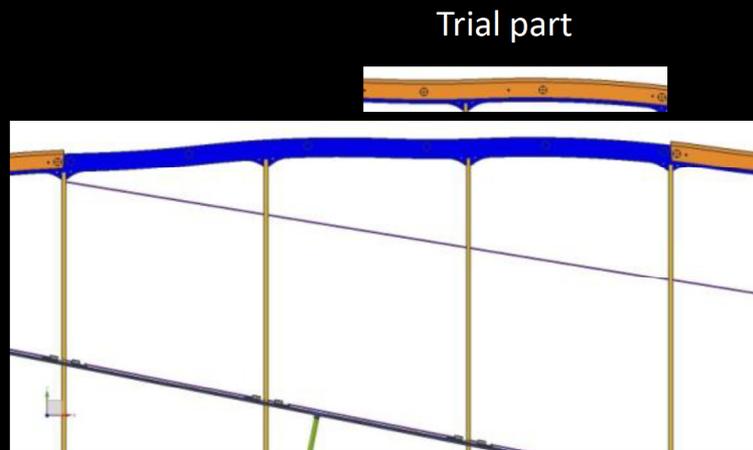
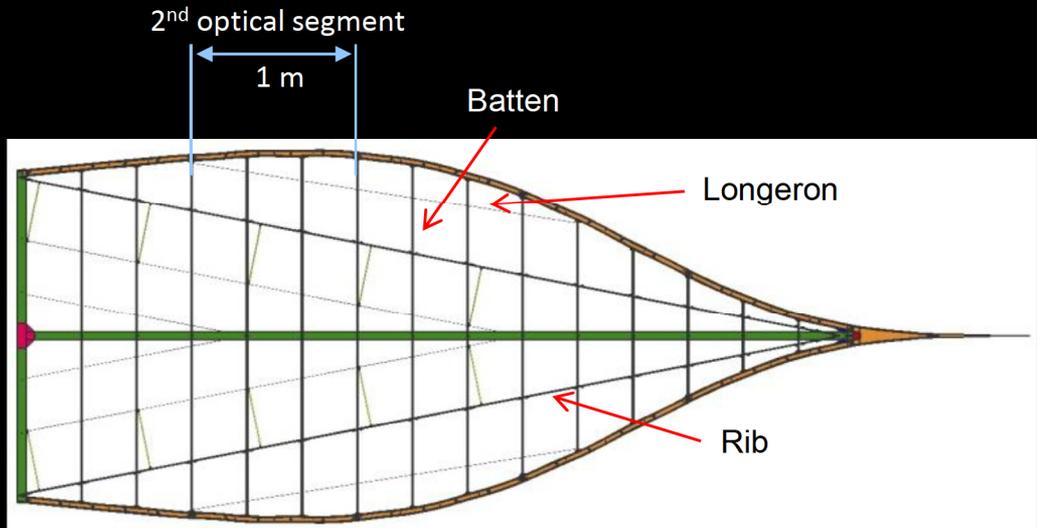
Table 1. Starshade and Telescope Parameters

| | TDEM | THEIA |
|------------------------------|------------|------------|
| Tip-to-Tip diameter | 32 m | 40 m |
| Central Disk Diameter | 20 m | 20 m |
| Petal length | 6 m | 10 m |
| Number of petals | 30 | 24 |
| Petal Base gap width | 1.1 mm | 1.5 mm |
| Petal Tip width | 2.6 mm | 4 mm |
| Max petal width | 2.34 m | 3.275 m |
| Distance to Telescope | 36,700 km | 55,000 km |
| Telescope Diameter | 1.5 m | 4 m |
| 50% throughput WA | 75 mas | 60 mas |
| 100% throughput WA | 90 mas | 75 mas |
| Bandpass at nominal Distance | 250-550 nm | 250-700 nm |





Petal Manufacture





Petal Manufacture





Conservative Assumptions

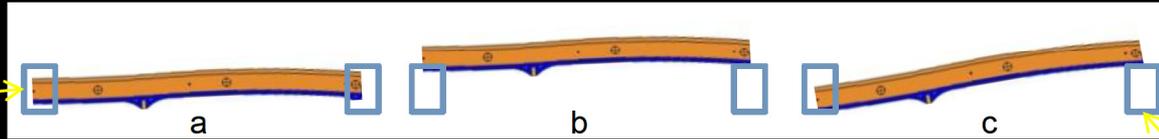
- Assume all errors are global
 - common to all petals.
 - Except those that have no global impact.
- Assume worst case wavelength
 - 550 nm for TDEM, 700 nm for THEIA
- Assume edge segments max out +/- against tolerance.
- Assume worst case for each tolerance envelope (see following slide).

| Perturbation | Global to Random ratio |
|----------------------------------|------------------------|
| Proportional width or petal tilt | 2.4 |
| Tip clip | 2.0 |
| Radial shift | 2.3 |
| Quadratic out-of-plane bend | 1.8 |
| 1 cycle/petal | 8.2 |
| 2 cycle/petal | 5.2 |
| 3 cycle/petal | 8.2 |
| 4 cycle/petal | 5.5 |
| 5 cycle/petal | 3.6 |
| 6 cycle/petal | 1.6 |
| Displ. of segment 10-11 meters | 2.6 |
| Displ. of segment 11-12 meters | 2.3 |
| Displ. of segment 12-13 meters | 2.1 |
| Displ. of segment 13-14 meters | 2.0 |
| Displ. of segment 14-15 meters | 1.8 |



Use Worst Case for Tolerancing

25 μm
 tall box.

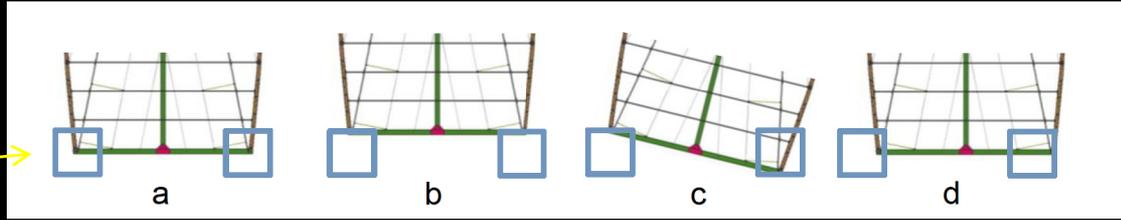


Edge segment placement

Case (b) scatters 2-3 x more light than case (c).

Width can be $> 50 \mu\text{m}$.

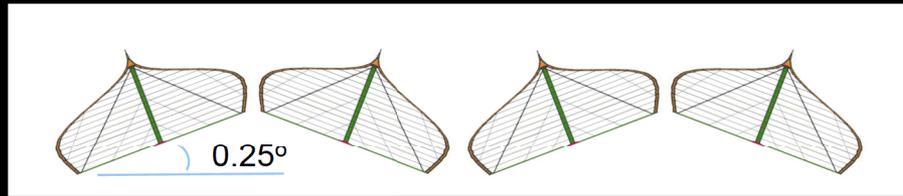
1 mm
 square box



Petal positioning relative to ideal.

Case (b) scatters 4x more light than (c).

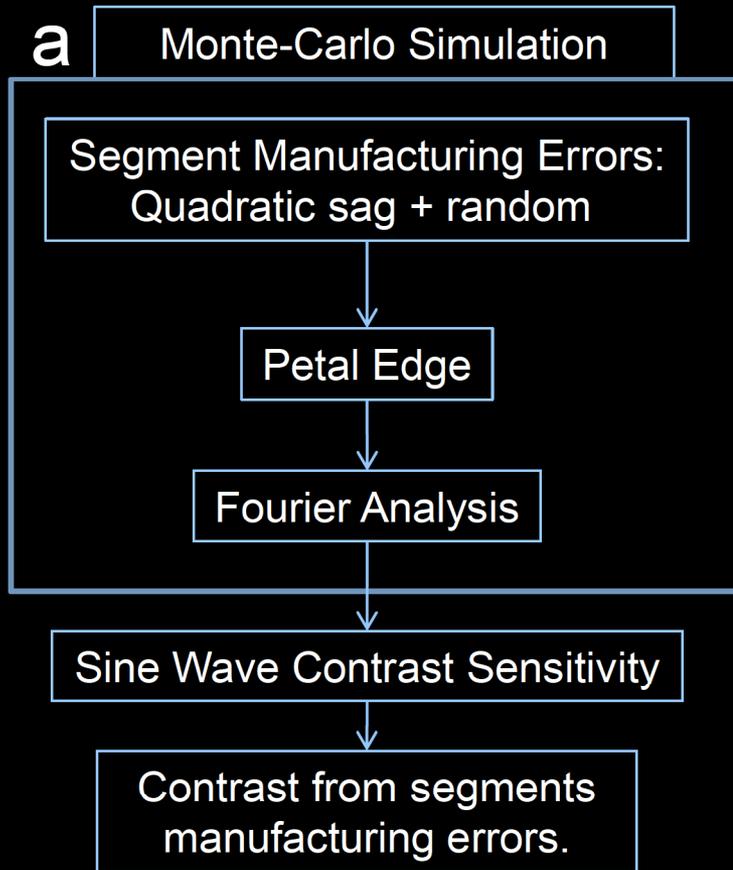
Case (d) has no global effect.



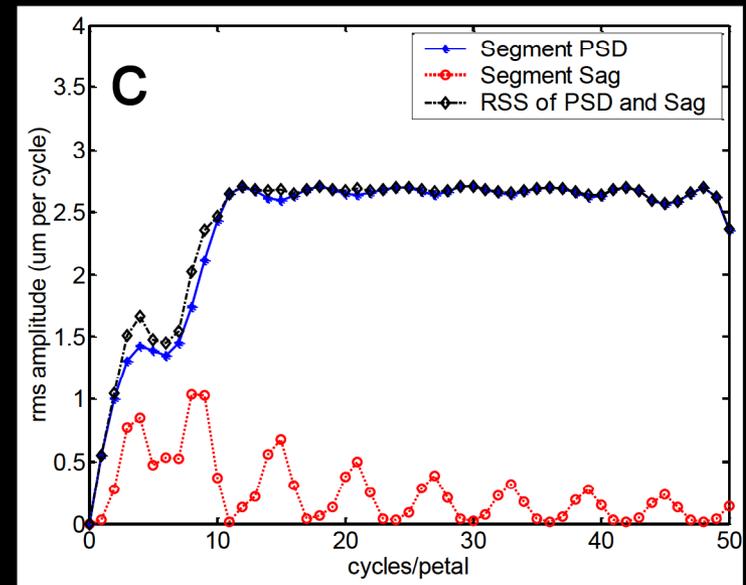
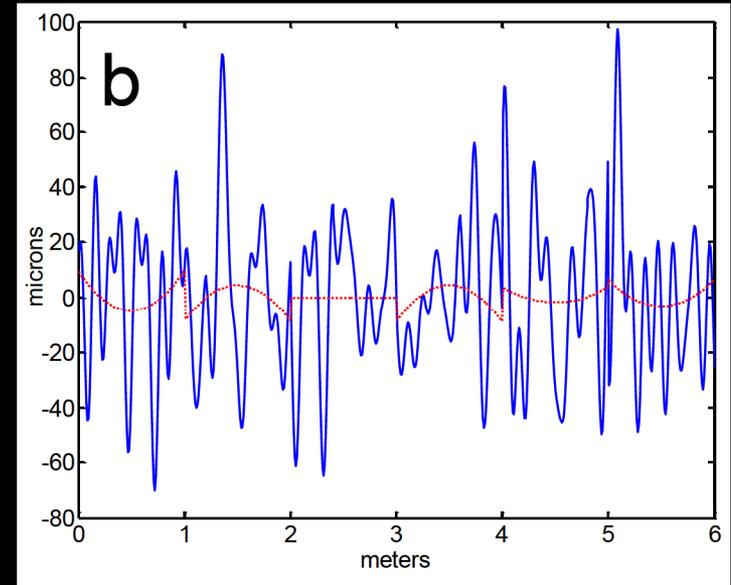
Petals tilted out of plane.



Segment Scatter

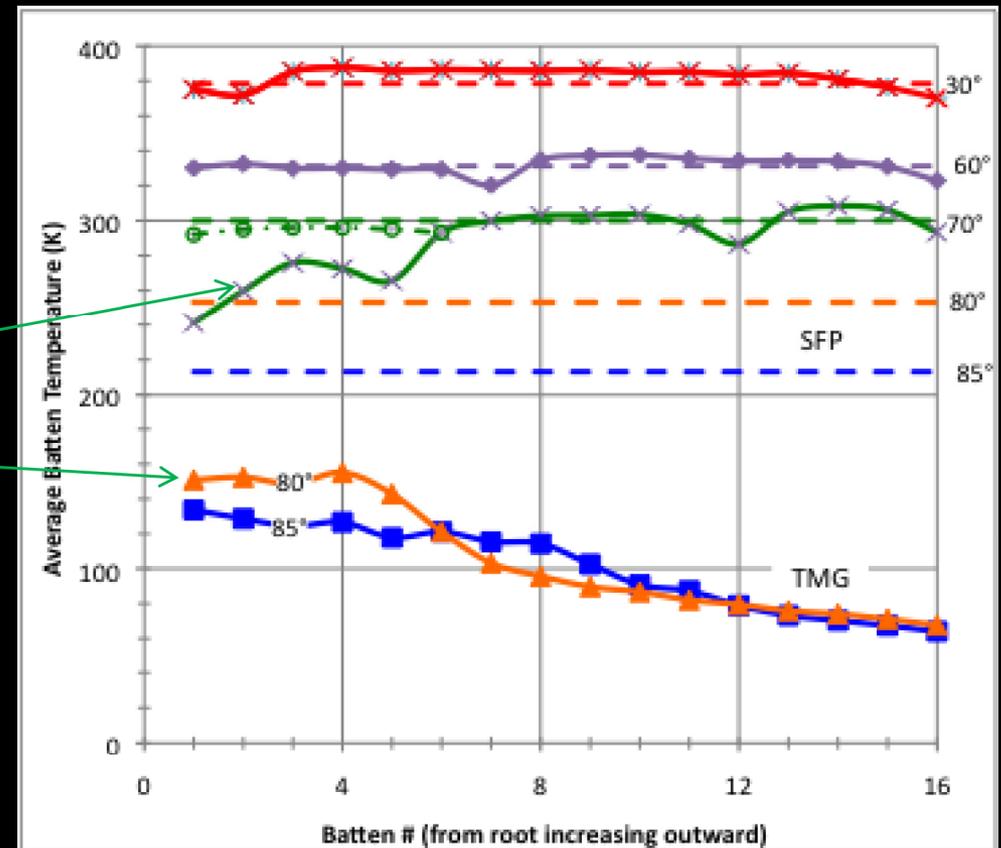
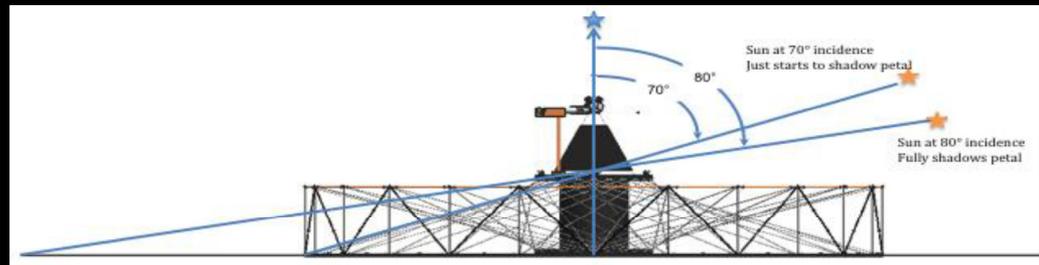
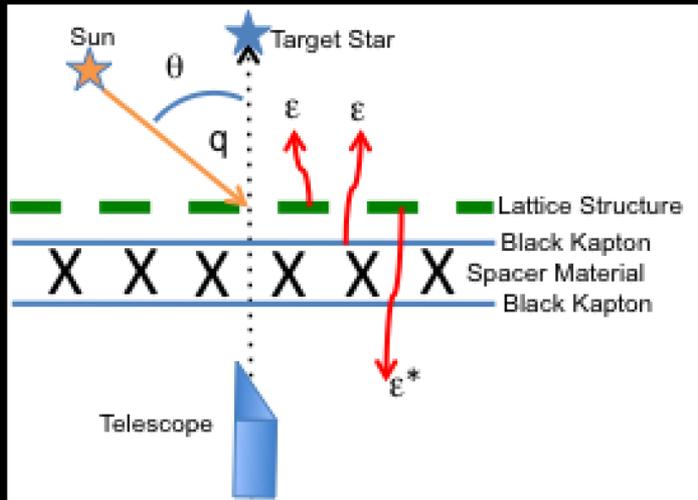


- a) Monte-Carlo simulation that generates petal edges from 6 segments each having a flat PSD from 1-8 cycles/petal and a quadratic sag.
- b) An example petal edge without segment positioning errors.
- c) Fourier Analysis. Petal sag contributes mainly in the 3-9 cycle/petal region, while PSD errors contribute mainly above 10 cycles.



Thermal Modeling

Steady-state (non-spinning) predicts

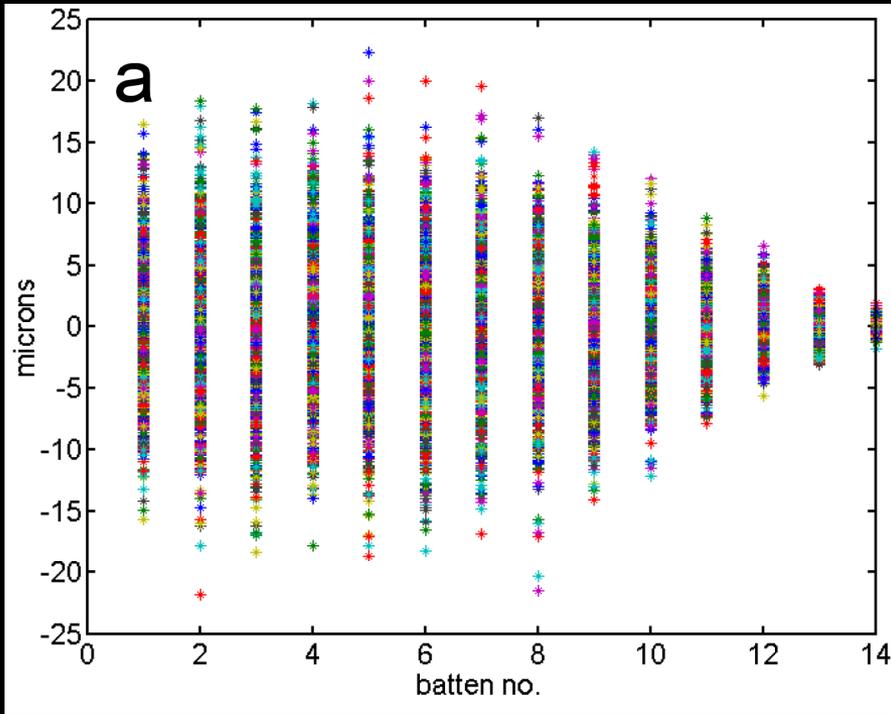


Partial Shadowing from s/c

Fully shadowed petal

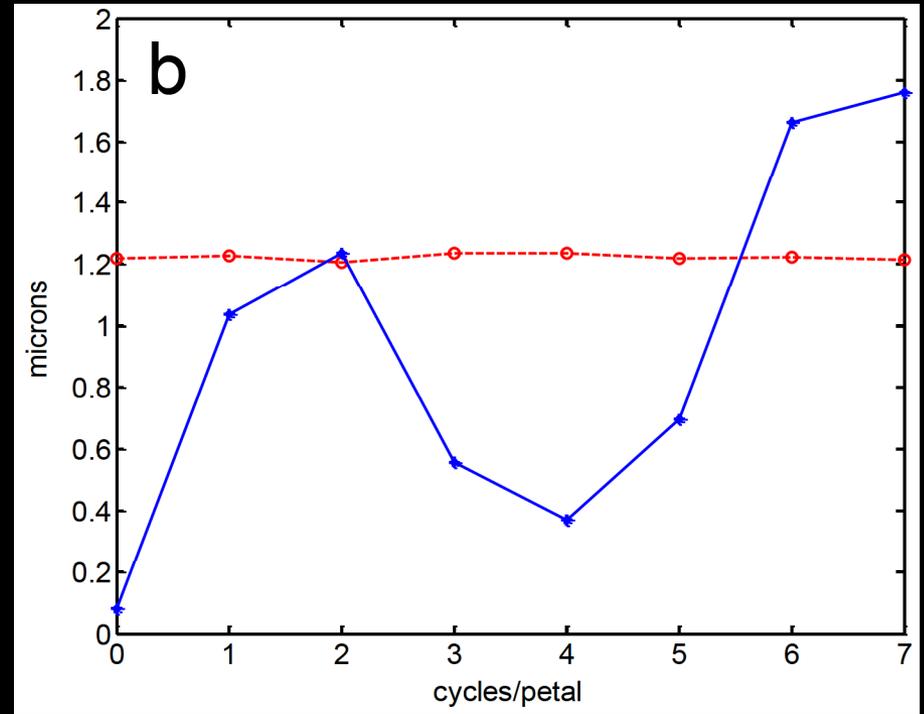
Dashed lines are analytical predictions in the absence of shadowing.

Random Thermal Variations



1000 realizations of the change in length of the 14 battens that control the TDEM petal width.

$\sigma = 2.5$ ppm, roughly ± 18 μm p-v



Blue: FFT of one realization normalized to show the r.m.s. variation in a 1 cycle/petal bandwidth.

Red: average of 1000 realizations, a white spectrum with 1.2 μm r.m.s. per cycle.



Thermal Analysis:

uniform, gradient, and random variation across a petal

| Deformation Type | Worse-case parameters | Max temp deviation with unc'ty (K) | Max deformation (ppm) | Tolerance Allocation (ppm) | Margin against allocation (%) | Notes |
|----------------------------------|---|------------------------------------|-----------------------|----------------------------|-------------------------------|---|
| Uniform - proportional width | $\epsilon^* = 0.1$ $\theta = 30^\circ$ to 85° | 100 | 20 | 35 | 43 | ΔT is relative to reference temp. set midway between extremes |
| Non-uniform - monotonic gradient | $\epsilon^* = 0.7$ $\theta = 80^\circ$ | 30 | 6 | 15 | 60 | Allocation applies at extreme temp. points |
| Non-uniform - semi random | $\epsilon^* = 0.7$ $\theta = 70^\circ$ | 15 | 3 | 7.5 | 60 | Allocation applies as envelope about average batten temp. |

| | Manufact. | Deployed Shape | Deployed Position | Thermal | Dynamic/ Form. Fly | Incoherent | Description | Units |
|--------------------------------|-----------|----------------|-------------------|---------|-----------------------|------------|--|-----------|
| Proportional width | x | x | | x | | | Prescribed width is $w(\rho)$, actual width is $\epsilon w(\rho)$ | ppm |
| Tip clip | x | | | | | | Tip segment length is too short or too long. | mm |
| Segment azimuthal displacement | x | x | | | | | Edge segments are displaced making local petal width too wide or narrow | mm |
| Segment in-plane rotation | x | x | | | | | Edge segments are rotated in plane relative to nominal local petal shape | radians |
| Base-to-tip thermal gradient | | | | x | | | The base is warmer than the tip causing differential petal growth | ppm |
| Random batten length change | | | | x | | | Shadowing and spinning cause the battens to grow and contract | ppm |
| In plane quadratic bend | | x | | x | | | Petal center line is shifted in plane by $a(\rho-\rho_0)^2$, where ρ_0 is the radial | mm at tip |
| Out of plane quadratic bend | | x | | x | | | Petal center line is shifted out of plane by $b(\rho-\rho_0)^2$, where ρ_0 is the | mm at tip |
| Radial Shift | | | x | x | | | Petal is moved radially, in plane. | mm |
| Lateral Shift | | | x | x | | | Petal is moved normal to center line, in plane. | mm |
| In plane rotation | | | x | | | | Petal center line is rotated in plane, starting at petal base. | mm at tip |
| Rotation about petal spine | | | x | | | | Petal rotates about its center line. Effect is equivalent to prop. Width. | deg |
| Truss Deformation | | | x | | | | Elliptical and higher order deviations from ideal circular shape | mm |
| Truss modes | | | | | x | | Deformation of truss due to dynamic perturbations (e.g. thrusters). | mm |
| Petal modes | | | | | x | | Deformation of petals due to dynamic perturbations. | mm |
| Lateral Formation Flying | | | | | x | | Starshade shifts laterally relative to star-telescope line-of-site | m |
| Incoherent contributions | | | | | | x | Solar scatter from edge RoC and roughness, holes, solar scatter in | um, PSD |

| | TDEM Design 6 m petals, 32 m tip-to-tip 1.5 m diam. telesocpe | | THEIA Design 10 m petals, 40 m tip-to-tip 4 m diam. telescope | | |
|--------------------------------|---|----------------|---|----------------|-----------|
| | 90 mas | 75 mas | 75 mas | 60 mas | 3-sigma |
| MANUFACTURE | | | | | |
| Proportional width | 10 | 5 | 10 | 10 | ppm |
| Segment placement | 12.5 | 8 | 25 | 25 | um |
| Segment shape | 75 | 60 | 75 | 75 | um |
| Contrast | 1.6E-11 | 1.5E-11 | 4.2E-12 | 8.9E-12 | |
| DEPLOYED SHAPE | | | | | |
| Proportional width | 5 | 5 | 5 | 5 | ppm |
| Segment displacement | 5 | 3.5 | 5 | 5 | um |
| In-plane Quadratic bend | 1 | 1 | 2 | 2 | mm at tip |
| Out of plane quadratic bend | 10 | 10 | 20 | 20 | mm at tip |
| Contrast | 2.0E-12 | 5.7E-12 | 3.1E-13 | 1.2E-12 | |
| DEPLOYED POSITION | | | | | |
| Radial Shift | 0.50 | 0.24 | 0.50 | 0.50 | mm |
| Lateral Shift | 0.50 | 0.24 | 0.50 | 0.50 | mm |
| Rotation about petal spine | 0.25 | 0.25 | 0.25 | 0.25 | deg |
| Elliptical truss def. | 1.00 | 0.75 | 1.00 | 1.00 | mm |
| Contrast | 2.2E-11 | 2.5E-11 | 1.3E-11 | 2.3E-11 | |
| THERMAL | | | | | |
| Proportional width | 35 | 15 | 35 | 35 | ppm |
| Base to tip gradient | 30 | 30 | 30 | 30 | ppm |
| Random batten length | 7.5 | 7.5 | 7.5 | 7.5 | ppm |
| In-plane Quadratic bend | 1 | 1 | 2 | 2 | mm at tip |
| Out of plane quadratic bend | 10 | 10 | 20 | 20 | mm at tip |
| Radial Shift | 0.2 | 0.13 | 0.2 | 0.2 | mm |
| Lateral Shift | 0.2 | 0.13 | 0.2 | 0.2 | mm |
| Contrast | 1.3E-11 | 1.8E-11 | 4.8E-12 | 8.3E-12 | |
| FORMATION FLYING | 1 | 0.25 | 1 | 1 | m |
| Contrast | 3.3E-12 | 4.5E-12 | 2.0E-12 | 4.7E-12 | |
| DYNAMICS ALLOCATION | 5.0E-12 | 5.0E-12 | 5.0E-12 | 5.0E-12 | |
| EDGE SCATTER ALLOCATION | 2.0E-11 | 2.0E-11 | 2.0E-11 | 2.0E-11 | |
| RESERVE | 1.8E-11 | 6.8E-12 | 5.1E-11 | 2.9E-11 | |
| TOTAL | 1.0E-10 | 1.0E-10 | 1.0E-10 | 1.0E-10 | |



Conclusions

- Requirements for building a high-performance starshade petal are achievable with current technology
 - Build segments to 25 μm rms, attach them within a 25 μm window.
 - Edge RoC should be ~ 50 μm . Technique for achieving this is under study. A matter of material choice and processing.
- Requirements for positioning the petals appear to be achievable within current technology
 - 1 mm deployment window on a 20 m diameter truss.
- We have made many conservative (worst-case) assumptions. Simulations show that performance loss due to petal manufacture is expected to be minimal.
- Thermal performance has significant margin even without spinning.
- By spinning the starshade, performance is limited by photometric rather than systematic scatter. This applies to both characterization and detection.



Future Work

- Measure the new TDEM petal and model scatter
- Perform deployment tests to show that ± 0.5 mm is achievable with our design.
- Complete thermal analysis of spinning starshade and analyze the performance margin (expected to be substantial).
- Perform dynamics analysis.
- Include Model Uncertainty Factors and perform material uniformity studies.