



# Studies of the Effects of Optical System Errors on the HCIT Contrast Performance

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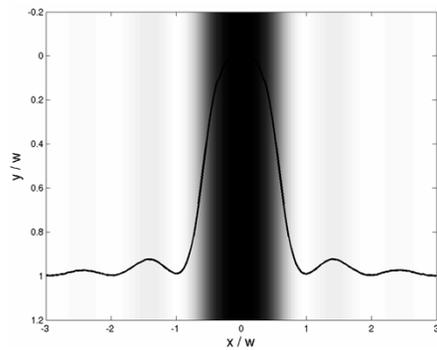
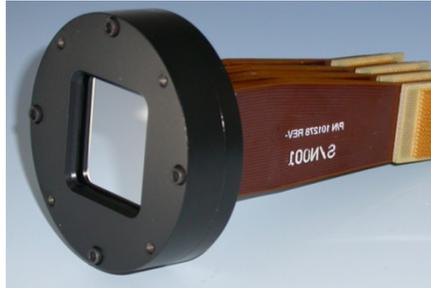
# Beginning Remarks

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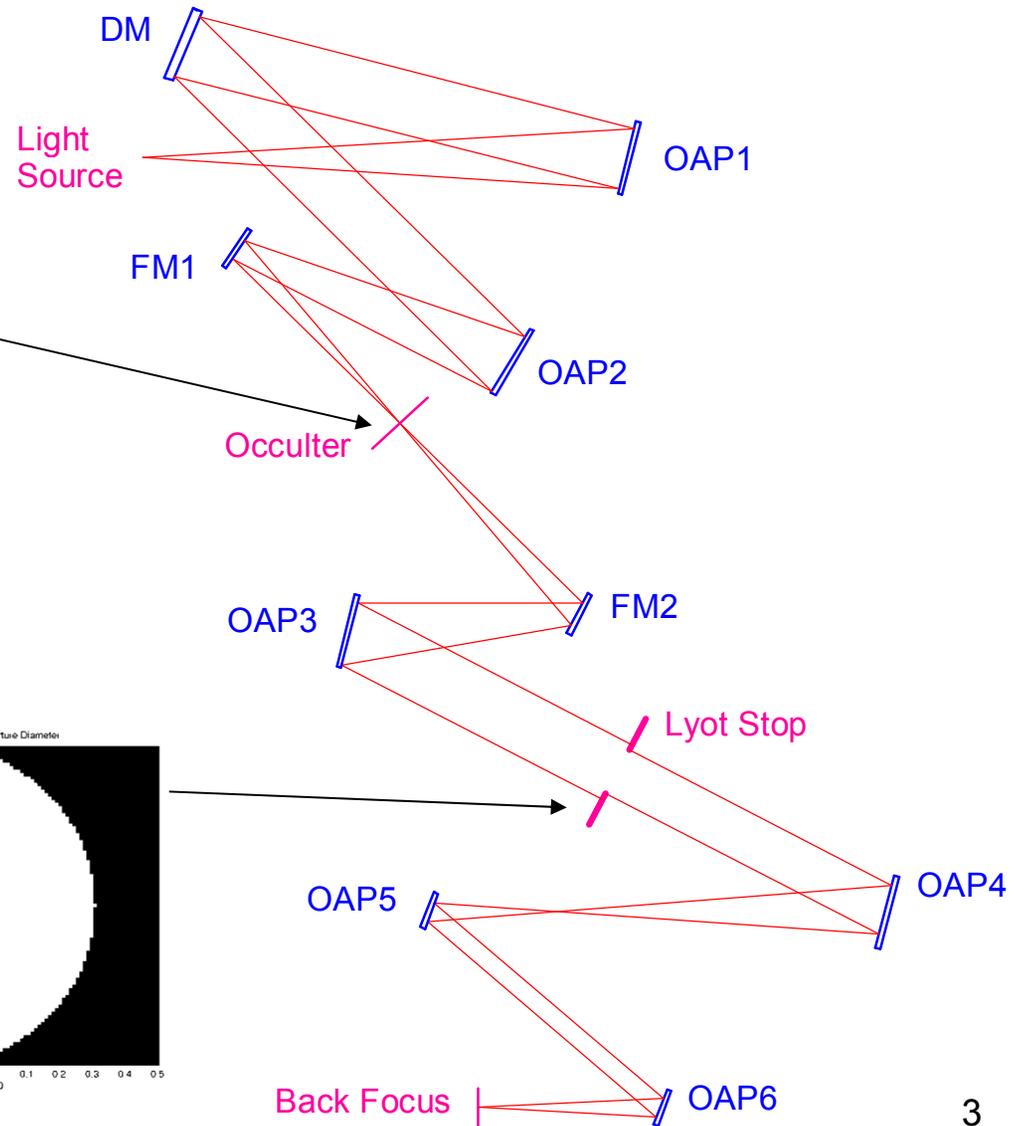
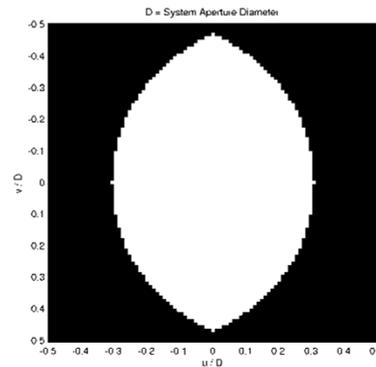
- One of the important milestones of the TPF Coronagraph project is to demonstrate the ability to predict the performance sensitivities of the system at levels consistent with exo-planet detection requirement.
- Want to gain some general understanding about the potentials and the limitations of the current single-DM HCIT system through modeling and simulations
- Specifically, want to understand the effects of some common errors on the estimation and the EFC-based control of e-field over a half dark-hole region
- Investigated errors include:
  - Two or 3 dead actuators (broadband)
  - Lateral and longitudinal movement of the occulting mask (narrowband)
  - Lateral movement of a flat optical surface (narrowband)
- Use a MACOS-based simulation algorithm which
  - combines a ray trace, diffraction model, & a broadband wavefront control algorithm
  - is capable of performing full three-dimensional near-field diffraction analysis

# HCIT Optical System

Deformable-Mirror  
(32x32 actuators)

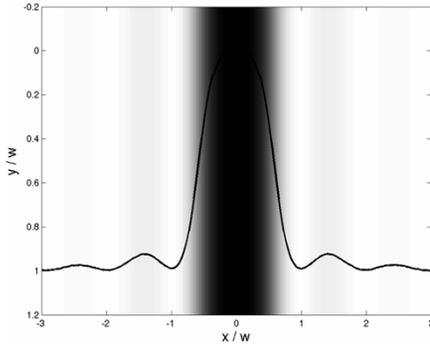


$$T(x) = [1 - \text{sinc}^2(x/w)]^2$$

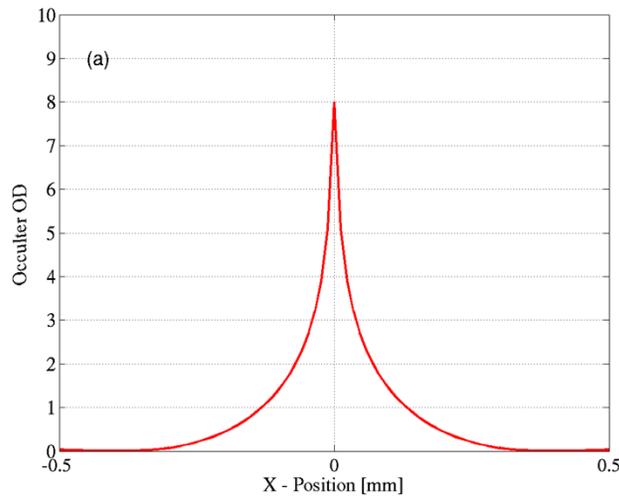


# OD and Phase Profiles of 2 Occulting Masks

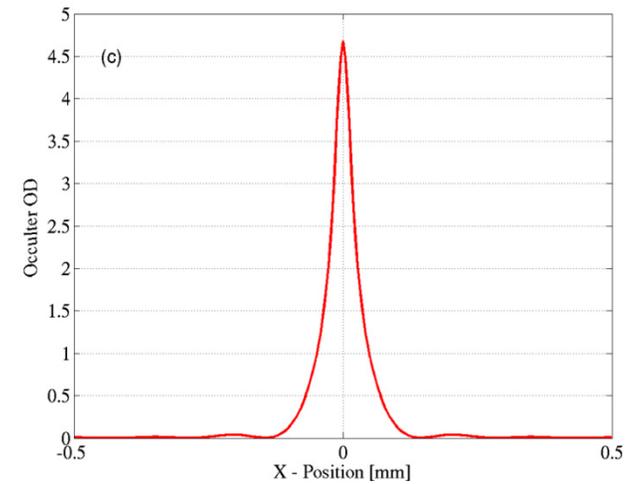
$$T(x) = [1 - \text{sinc}^2(x/w)]^2$$



Platinum (Pt) deposited on a fused-silica and compensated with spatially profiled PM

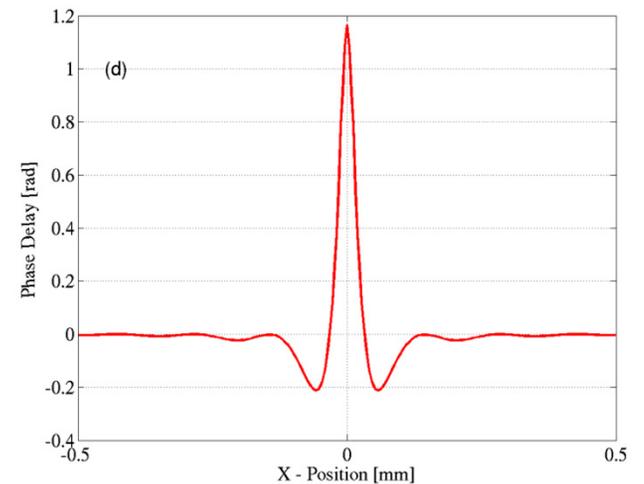
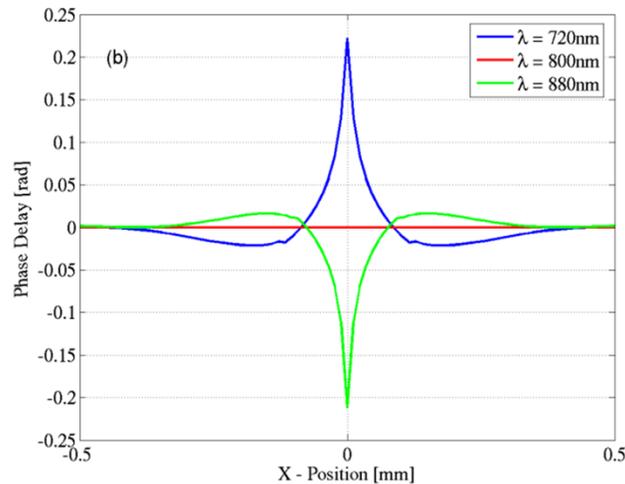


Thin-film Nickel (Ni) occulter deposited on a glass



Pt-occulter is used in "dead-actuator" and FM1 x-translation

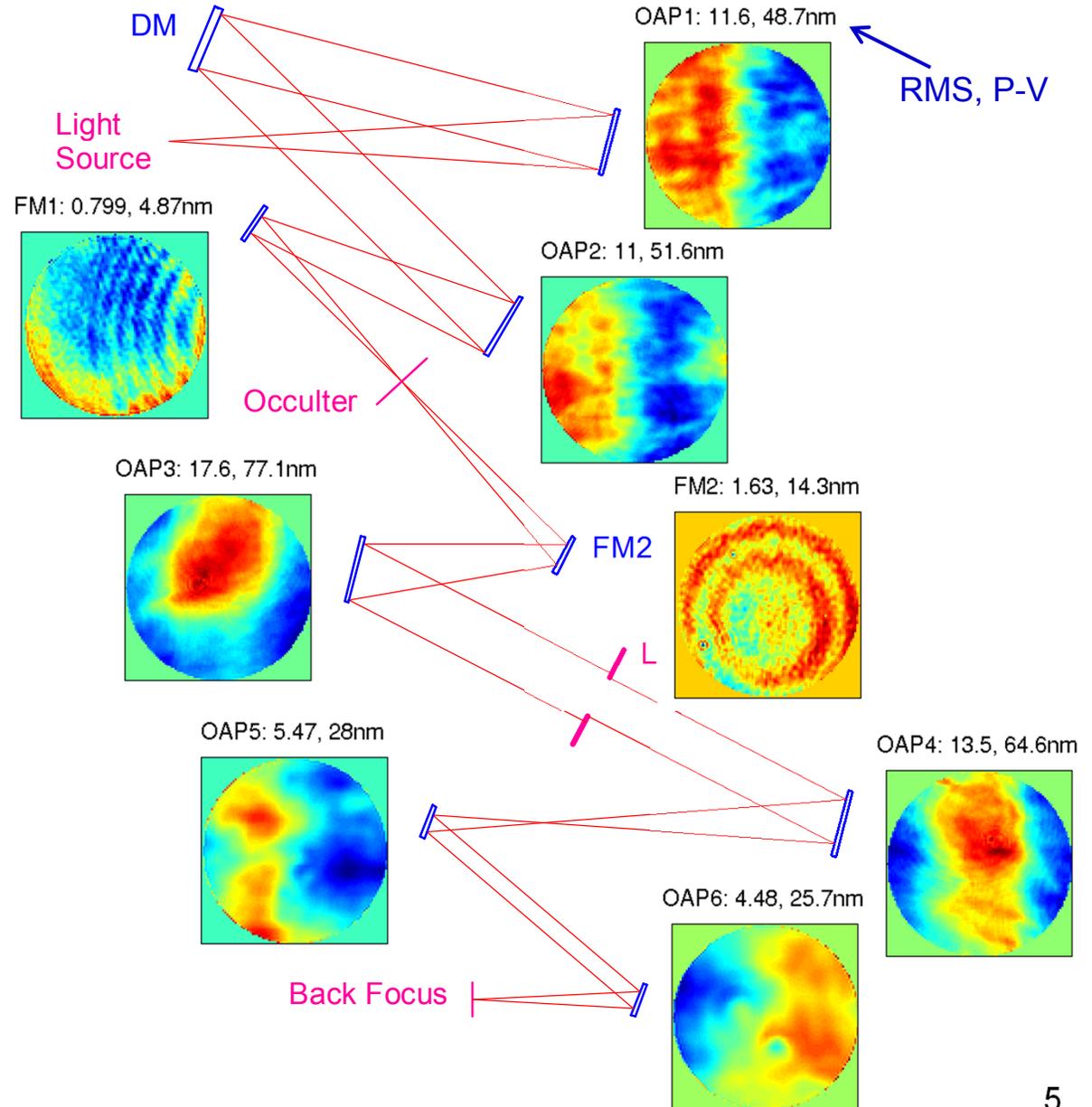
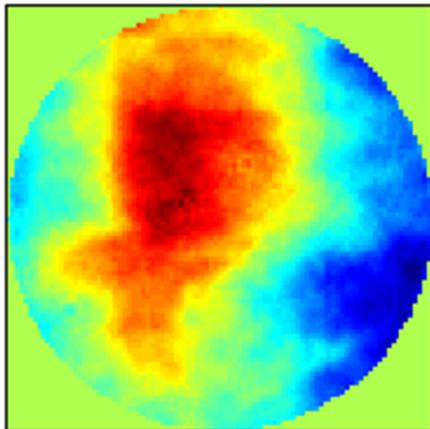
Ni-occulter is used in occulter x- & z-translation



# Surface Errors Used in Simulations

- The phase maps were measured independently with a Zygo interferometer
- Each WF map was obtained by including the phase map of one optic at a time in the optical model
- “All” was obtained by “turning-on” all surface errors
- Will include these 8 surface error maps in simulations

All: 35.9, 163nm



# Definitions: Normalized Intensity & Contrast

**Normalized Intensity:**  $I(x, y) = I_o(x, y) / I_{uo\max}$ ,  $I_o(x, y)$ : Occulted,  $I_{uo\max}$ : Un - Occulted

**Contrast:**  $C(x, y) = \left[ \frac{I_o(x, y)}{I_{uo\max}} \right] \left[ \frac{\text{Max}\{T(x, y)\}}{T(x, y)} \right] = I(x, y) \left[ \frac{T_0}{T(x, y)} \right]$ ,  $T(x, y)$  = Occulter Transmittance

**Normalized positions:**  $X = x / f$ ,  $Y = y / f$ ,  $R = \sqrt{X^2 + Y^2}$

**WFC over  $\Omega_c$ :**  $[X, R] = [4, 11]\lambda / D$

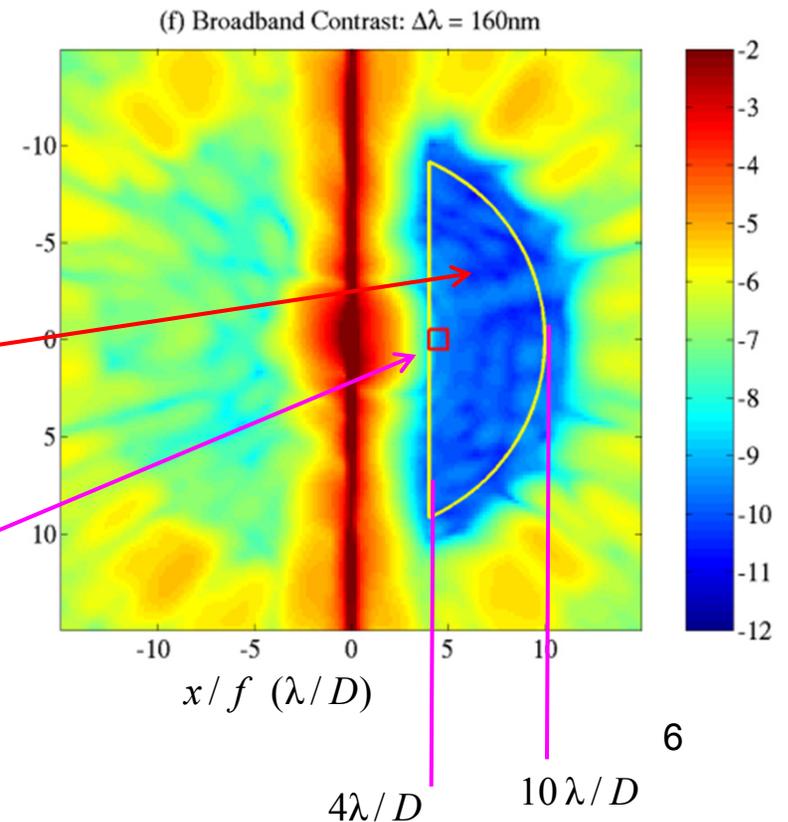
$I_b$  and  $C_b$  are mean values averaged over  $\Omega_b$ :

$$[X, R] = [4, 10]\lambda / D$$

$I_s$  and  $C_s$  are mean values averaged over  $\Omega_s$ :

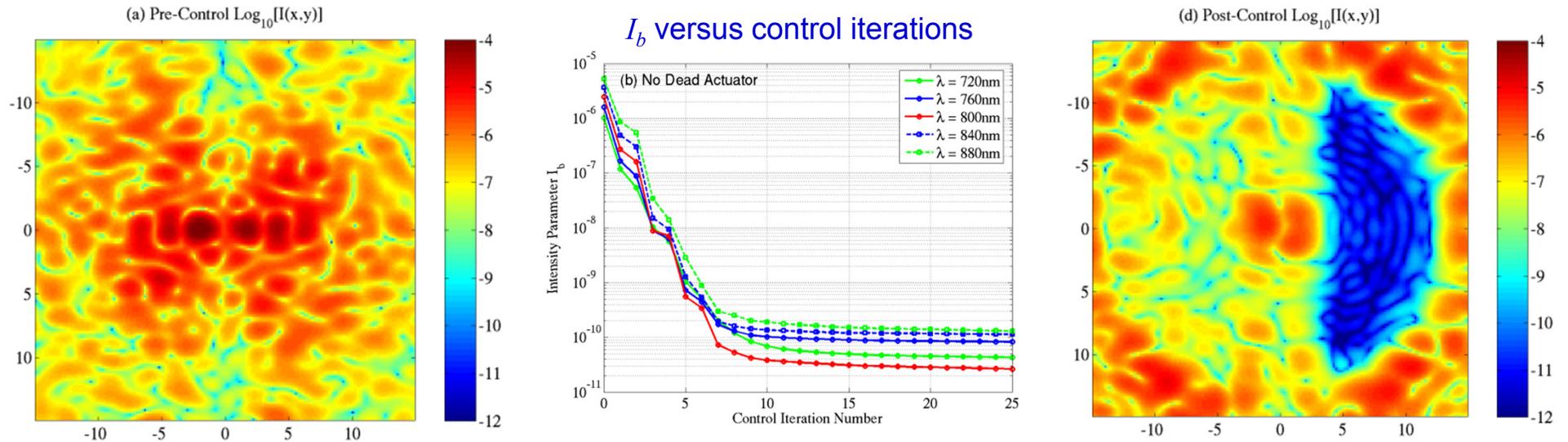
$$\Delta X = \Delta Y = 1\lambda / D$$

$I_m$  and  $C_m$  are maximum values inside  $\Omega_s$



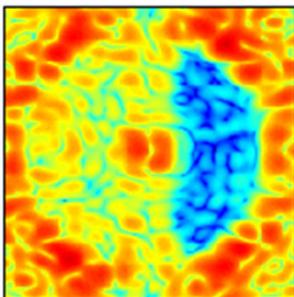
# Nominal Case as a Baseline: Normalized Intensity

Including only optical surface errors and occulter phase

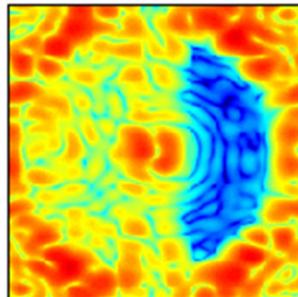


Post-Control  $I(x,y)$  in Log-Scale

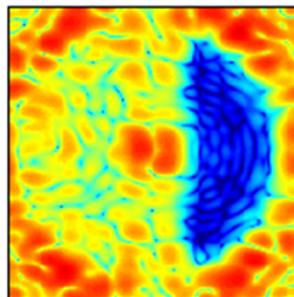
(a)  $\lambda = 720\text{nm}$



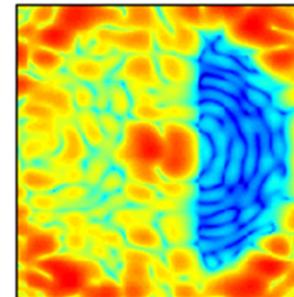
(b)  $\lambda = 760\text{nm}$



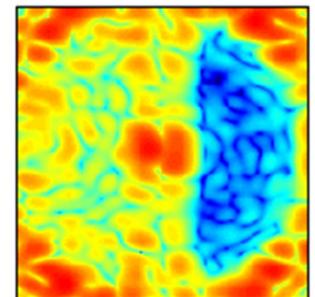
(c)  $\lambda = 800\text{nm}$



(d)  $\lambda = 840\text{nm}$



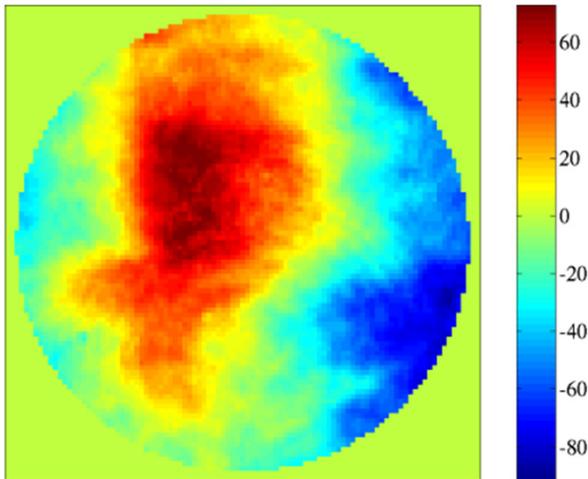
(e)  $\lambda = 880\text{nm}$



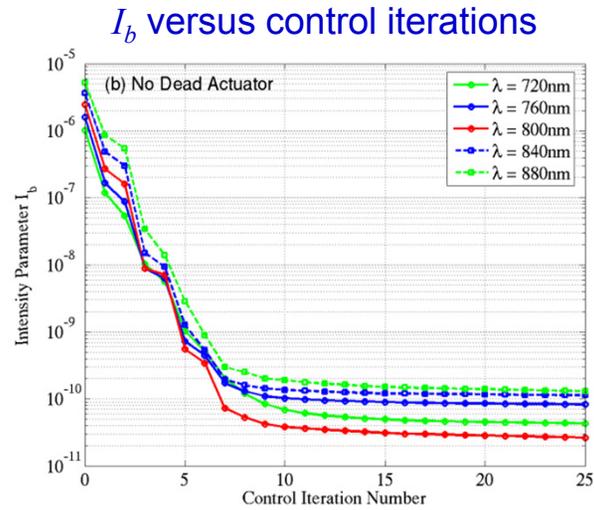
# Nominal Case: OPD, DM Commands & Broadband Contrast

Including only optical surface errors and occulter phase

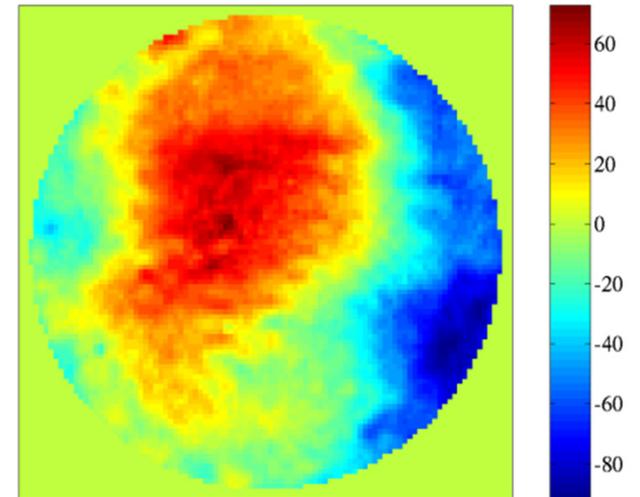
(b) Pre-Control OPD [nm]



RMS = 36.0, PV = 164.0nm

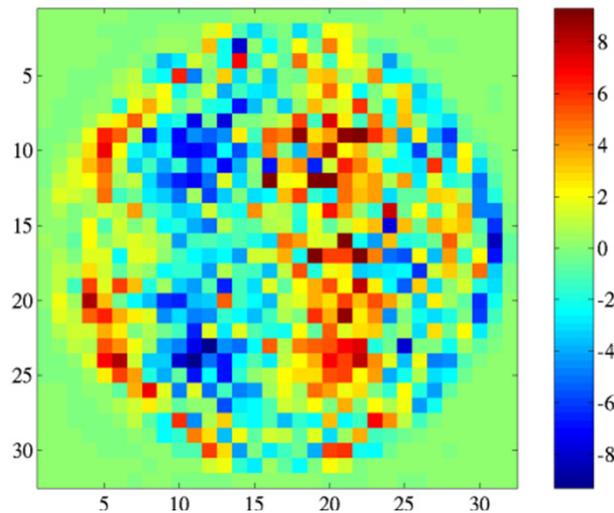


(e) Post-Control OPD [nm]

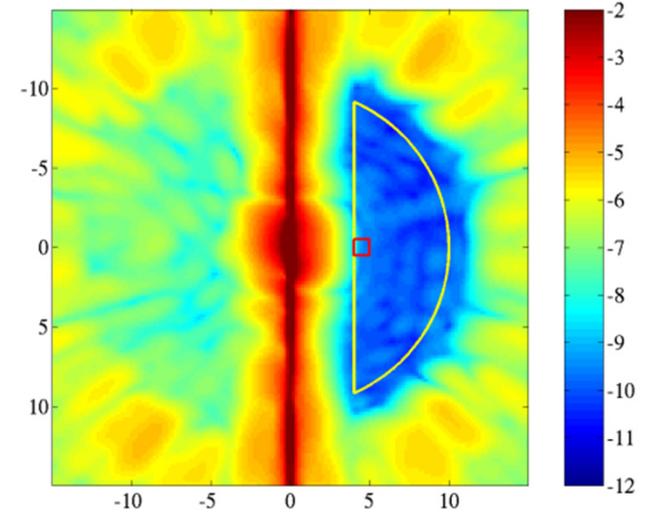


RMS = 35.0, PV = 164.9nm

(c) Actuator Height [nm]



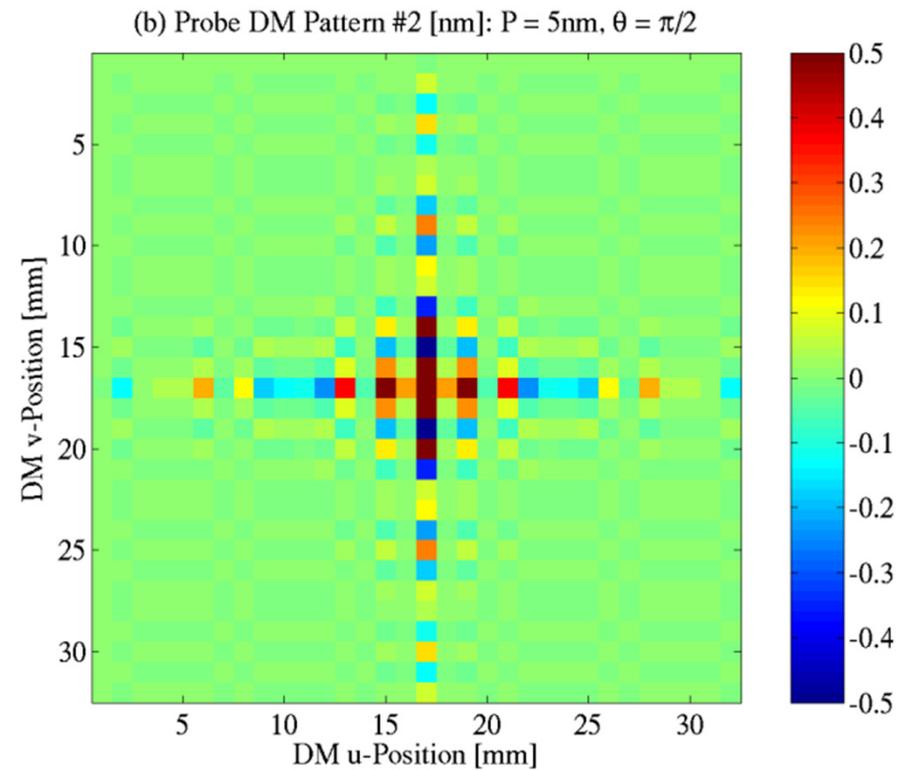
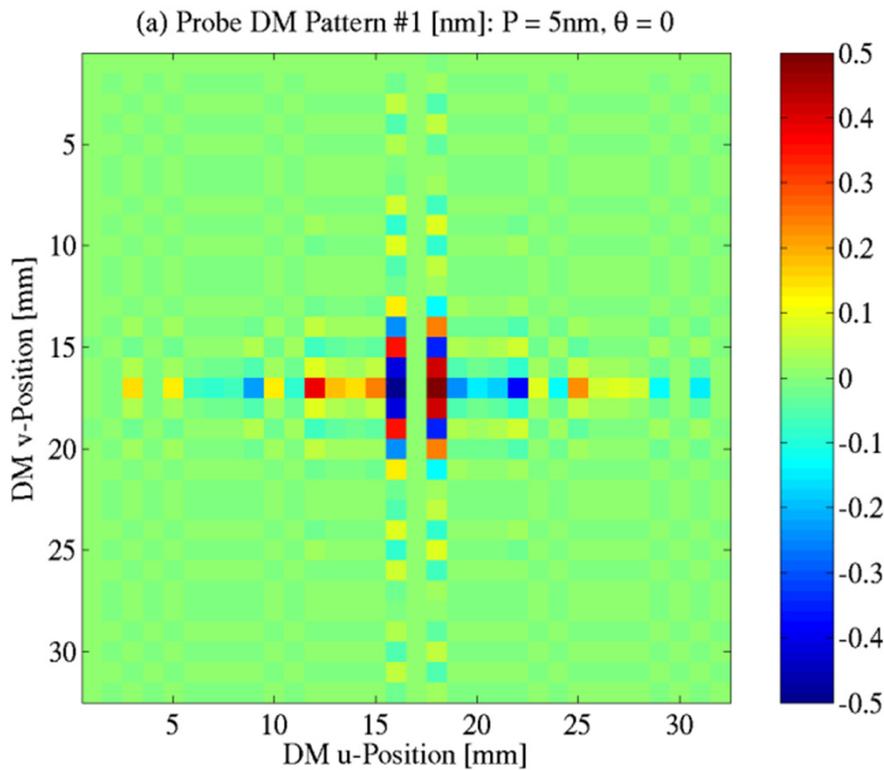
(f) Broadband Contrast:  $\Delta\lambda = 160\text{nm}$



# DM Settings Used in 4-Probes E-Field Estimation

Probe DM Settings:  $\psi(u, v; \theta) = P \operatorname{sinc}(\Delta \xi u) \operatorname{sinc}(\Delta \eta v) \sin(\xi_c u + \theta)$

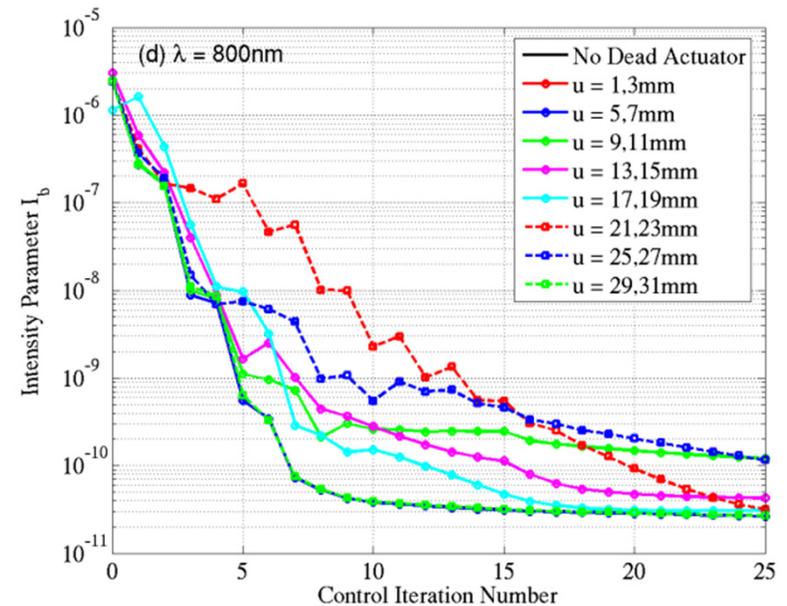
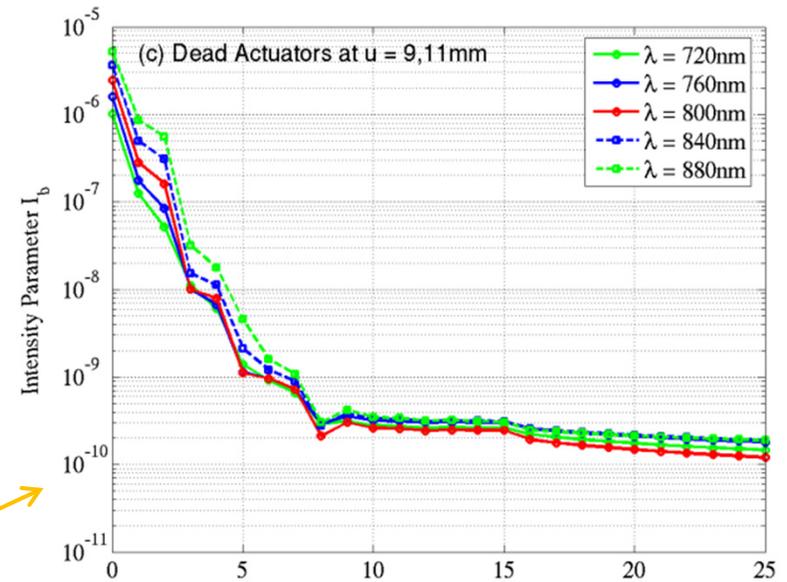
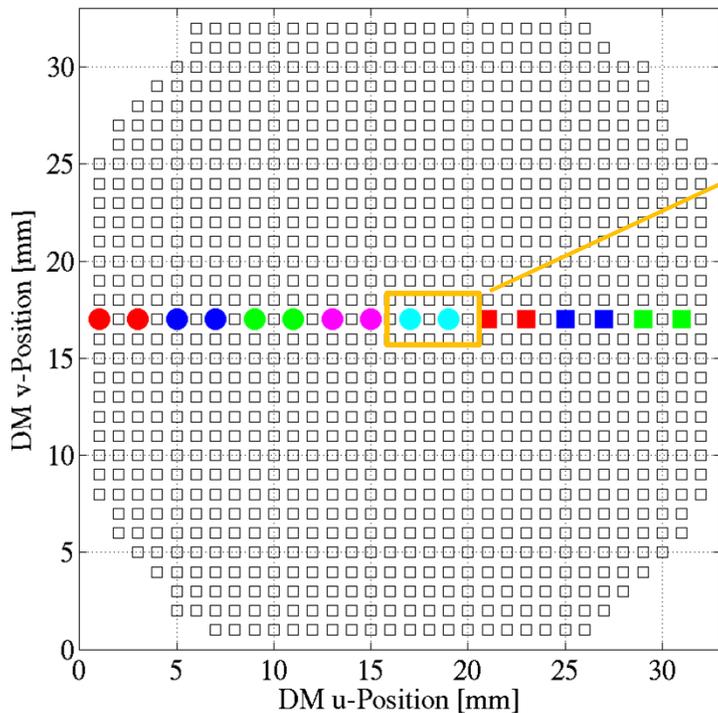
$$\theta = 0, \frac{\pi}{2}, \pi, \frac{3\pi}{2}$$



# Dead Actuators: 2 Actuators Interleaved by One Actuator

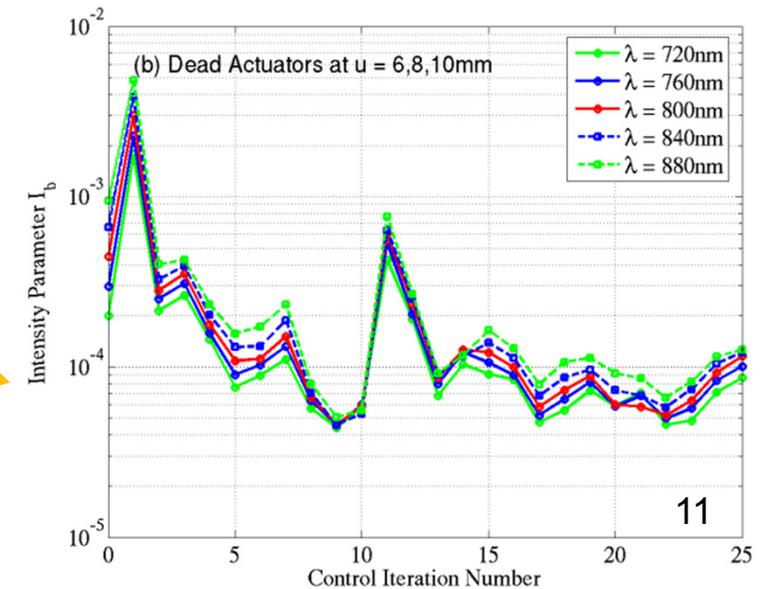
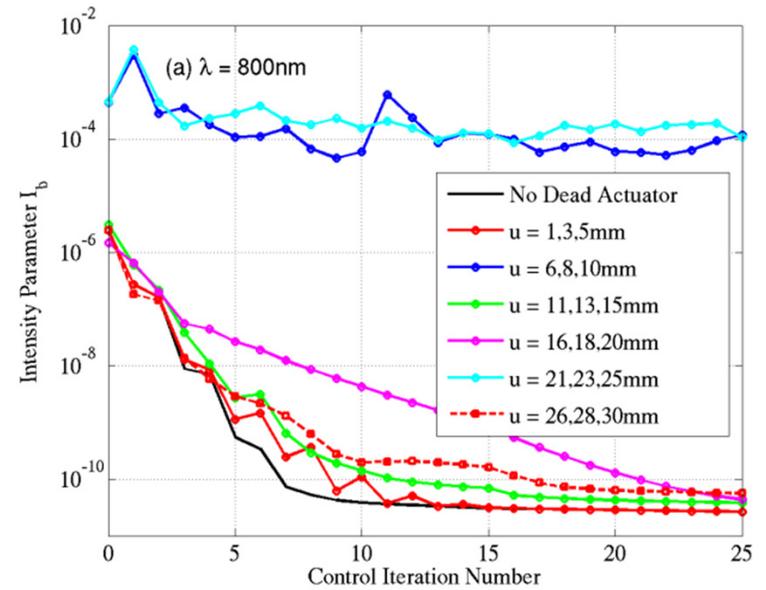
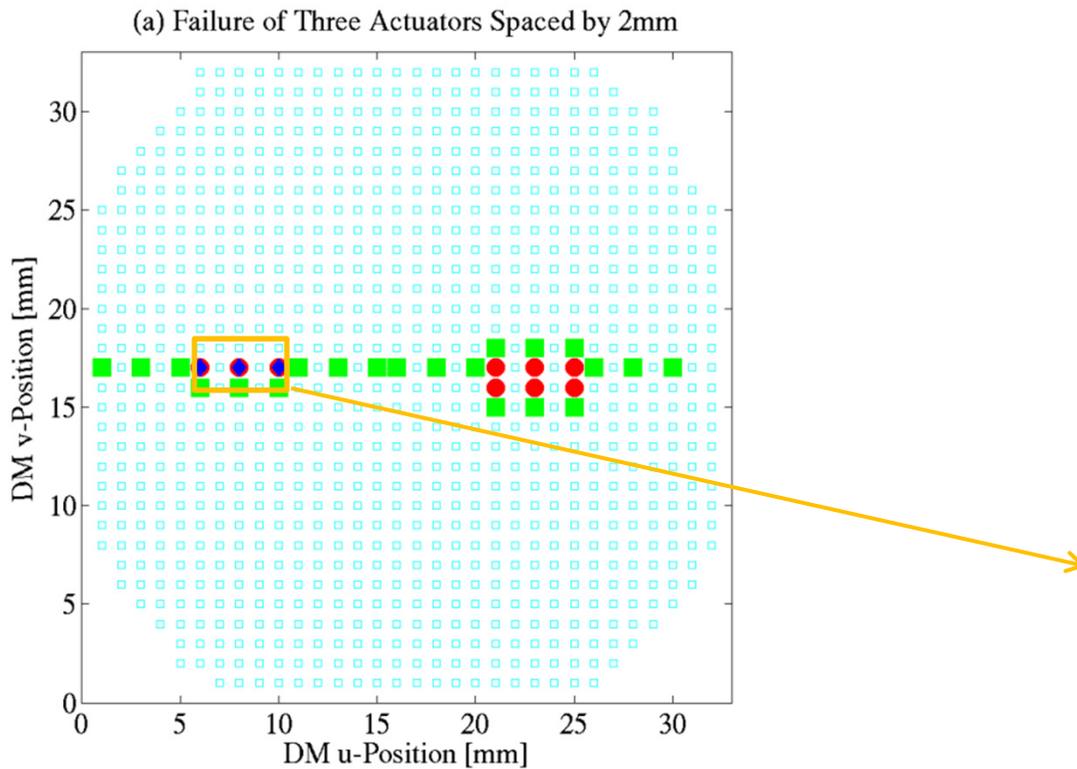
- DM actuator spacing = 1mm
- E-field estimation & control are most sensitive to actuators on row  $v = 17$ mm
- Different colors/shapes represent different dead actuators
- Less WFC efficiency in some cases, but all work

(a) Black: Active Actuators. Colored: Dead Actuator Pairs



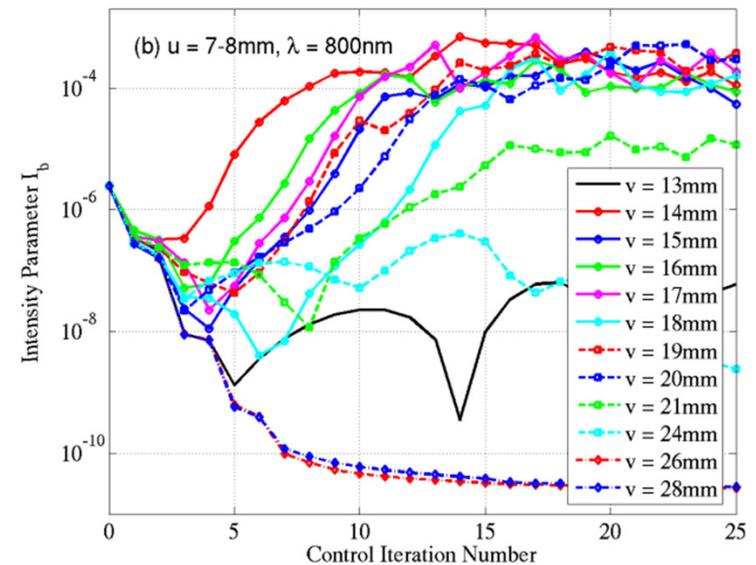
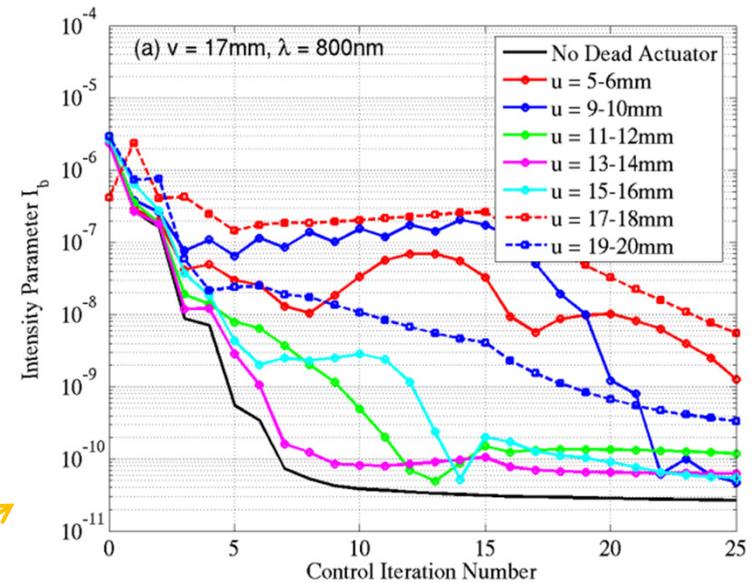
# Dead Actuators: 3 Actuators Interleaved by One Actuator

- DM actuator spacing = 1mm
- E-field estimation & control are most sensitive to actuators on row  $v = 17\text{mm}$
- Green groups: Work
- Red groups: Fail
- Blue on top of the red: Fail with e-field estimation, but work without it

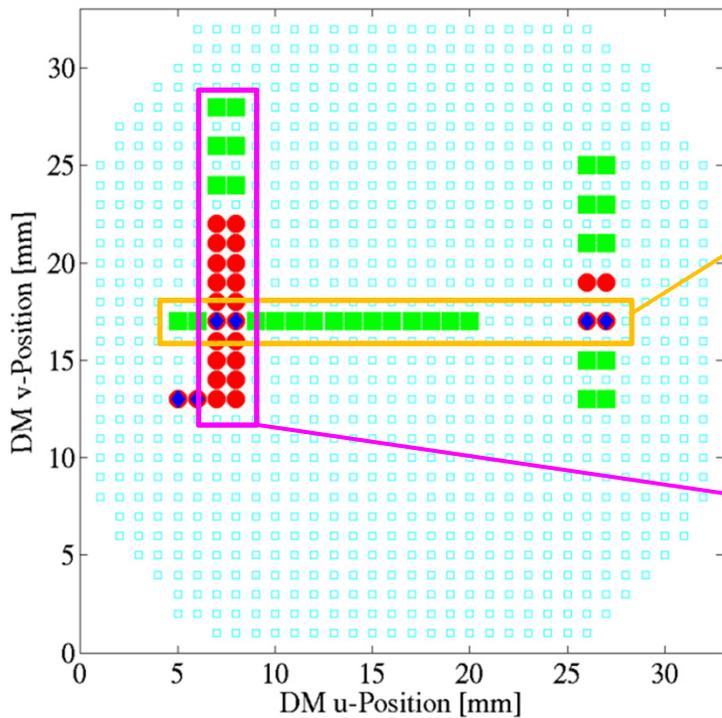


# Case of 2 Adjacent Actuators Dead

- DM actuator spacing = 1mm
- E-field estimation & control are most sensitive to actuators on row  $v = 17$ mm
- Green groups: Work
- Red groups: Fail
- Blue on top of the red: Fail with e-field estimation, but work without it



(b) Failure of Two Adjacent Actuators



# X-Translation ( $T_x$ ) of FM1—Case of Sine-Wave Phase

True:  $\Delta I(x, y) = |E(x - T_x, y) - E(x, y)|^2 / I_{u0max}$

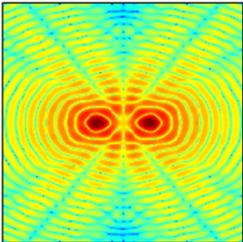
Predicted:  $\Delta I(x, y) = (\pi / \lambda)^2 [PV(\Delta OPD) / 2]^2 |M(x - N_x \lambda f / D, y) E(x', y')|^2 / I_{u0max}$

Origin of  $[x', y'] = [0, 0]$ ;    Origin of  $[x, y] = [N_x \lambda f / D, 0]$

$N_x$  = Spatial – Frequency

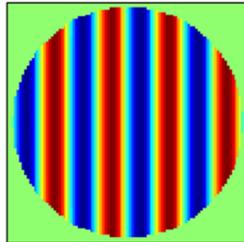
- “True” and “Predicted” agree well

PSF: Pre-Control, 932



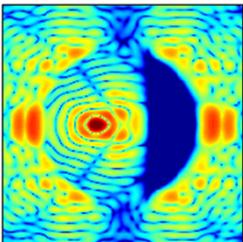
Cb = 8.53e-07

OPD: Pre-Control



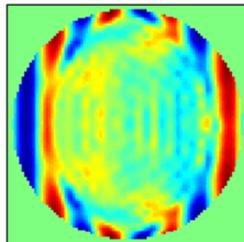
1.9, 5.3nm

PSF: Post-Control

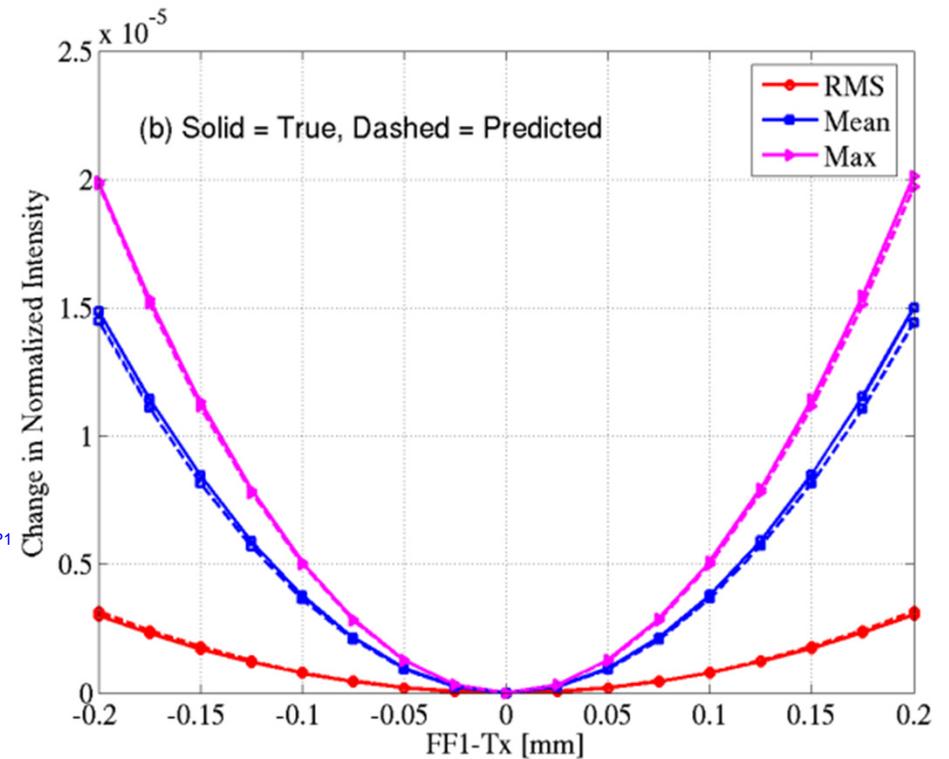
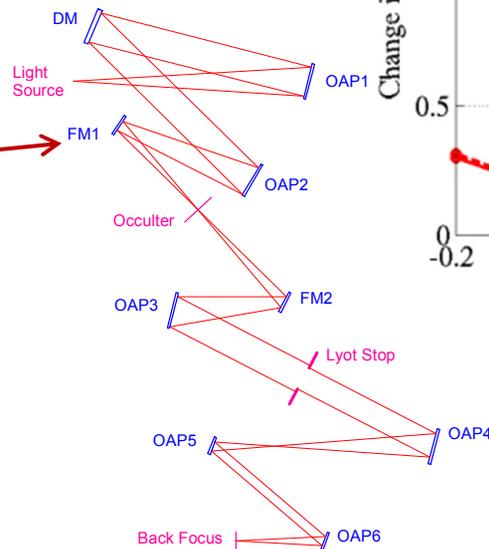


Cb = 2.06e-14

OPD: Post-Control

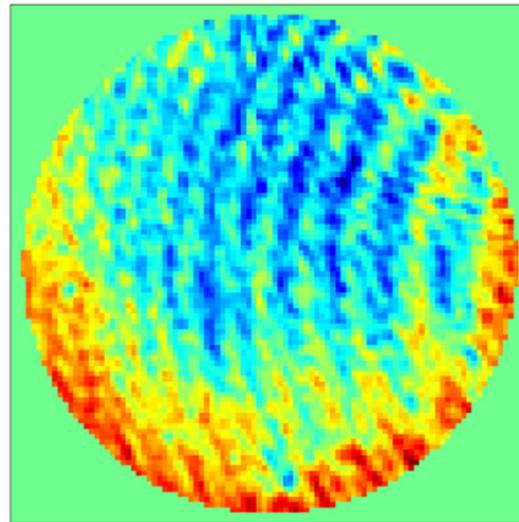


1.0, 5.5nm



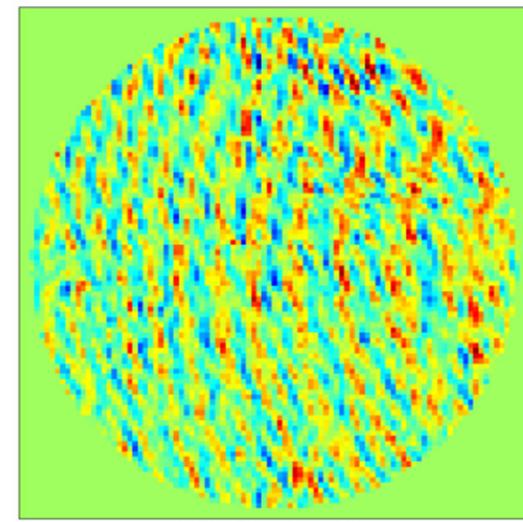
# X-Translation ( $T_x$ ) of FM1—Case of All 8 True Phase Errors

(a) OPD Caused By FM1 Surface Error



RMS = 0.9, PV = 5.3nm

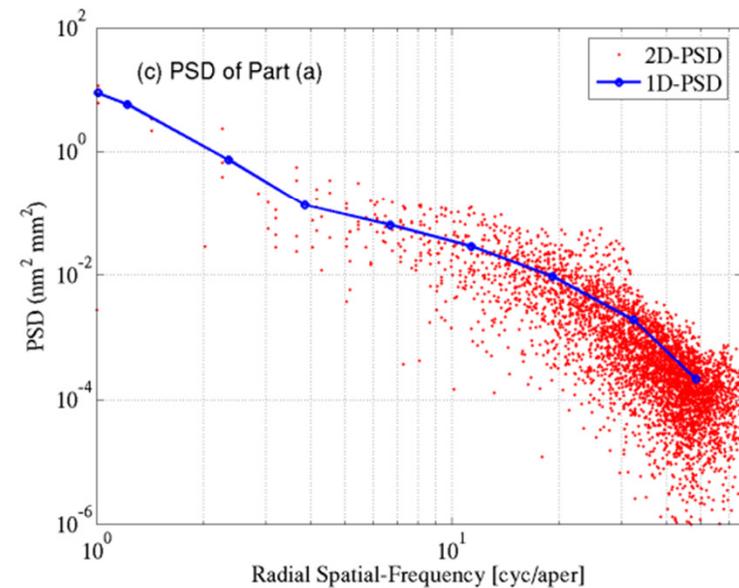
(b)  $\Delta$ OPD When FM1- $T_x = -0.2$ mm



RMS = 0.5, PV = 4.6nm

Change in OPD at exit-pupil:

$$\Delta OPD = OPD(T_x) - OPD(0)$$

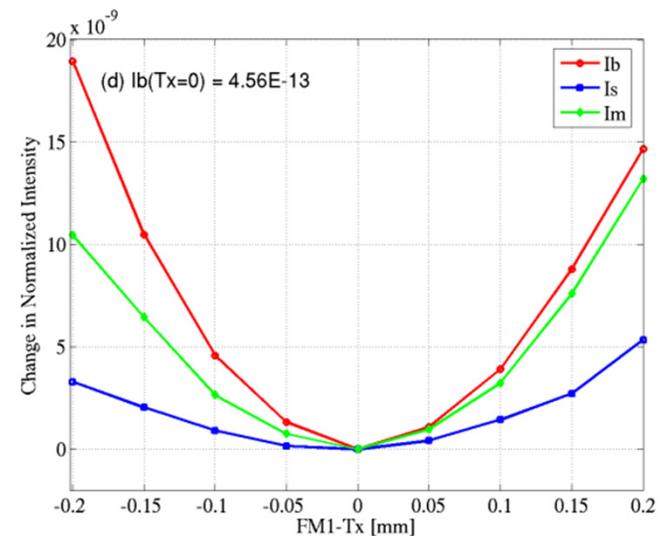
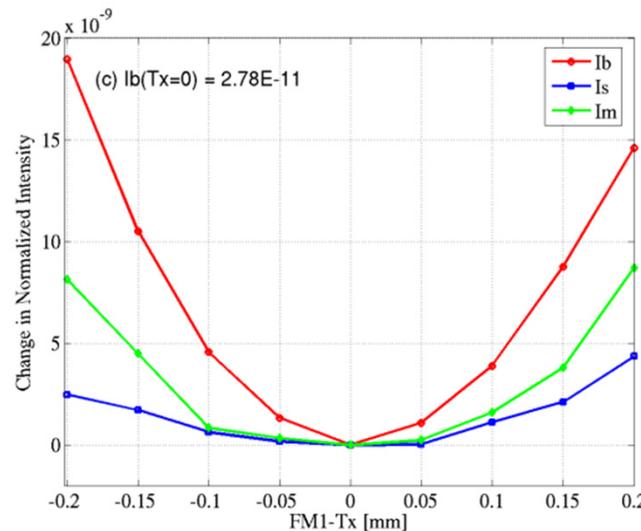
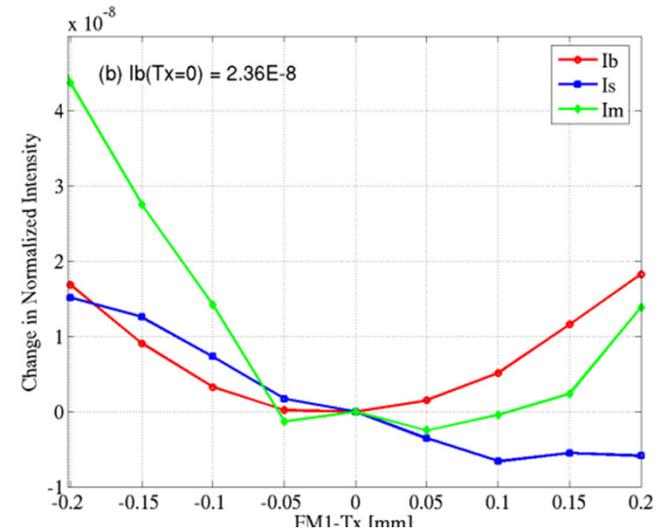
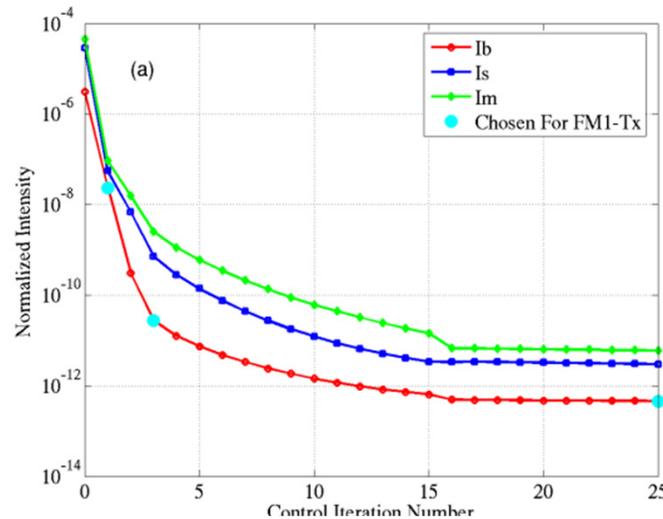


# FM1- $T_x$ —Case of All 8 True Phase Errors (cont)

- Change in  $I(x,y)$ :  $\Delta I(x,y; T_x) = I(x,y; T_x) - \Delta I(x,y;0)$
- $\Delta I(x,y; T_x)$  is evaluated at 3 different contrast levels

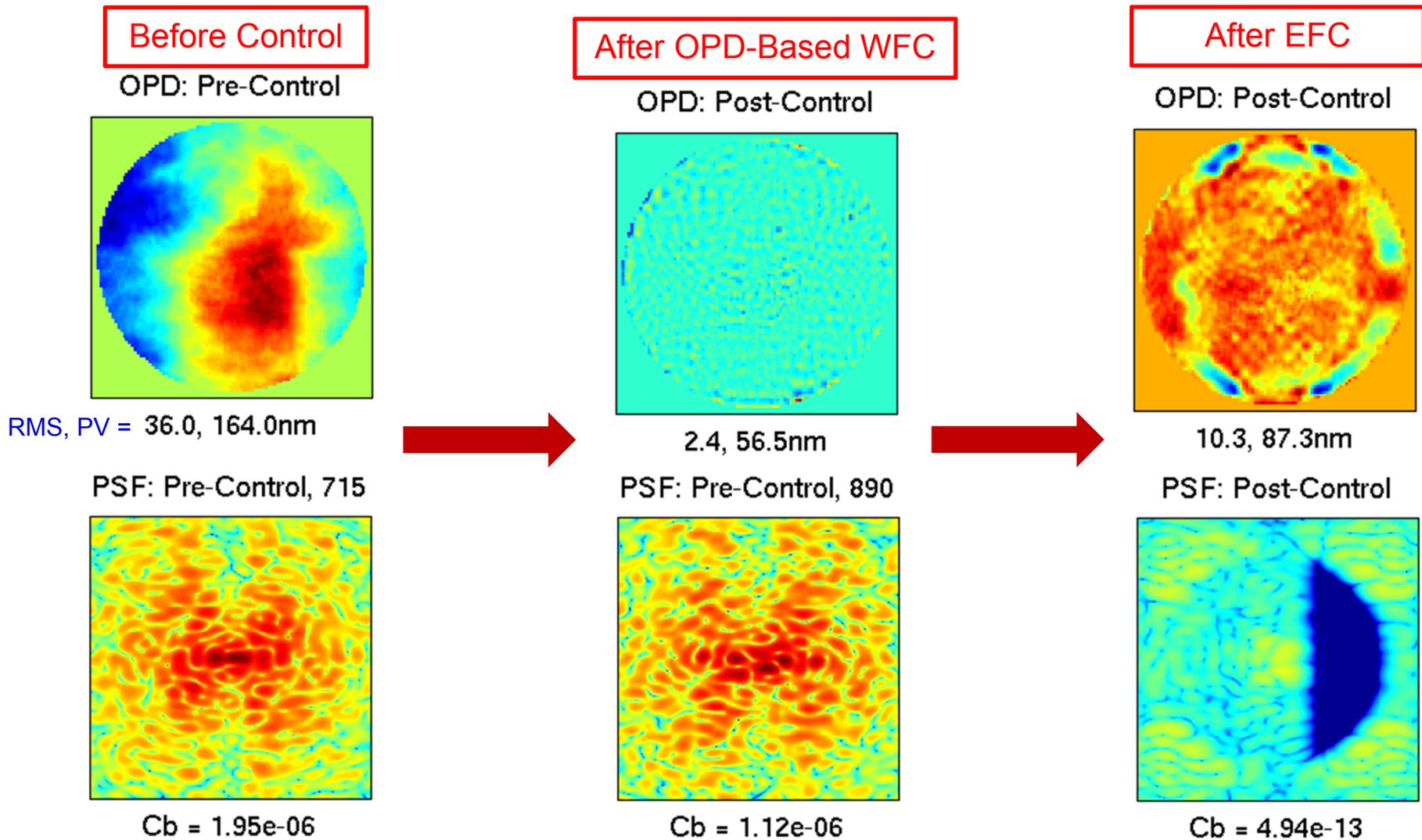
- $\Delta I(x,y; T_x)$  is not symmetric with respect to FM1- $T_x$

- $I(x,y)$  sensitivity to FM1- $T_x$  depends on the darkness of the dark-hole achieved



# Occulter $T_x$ and $T_z$ Translations: 2-Step WFC

- Before x- and y-translations of the occulter, 2-step WFC was conducted to generate a dark-hole
- All surface errors are included in the simulation

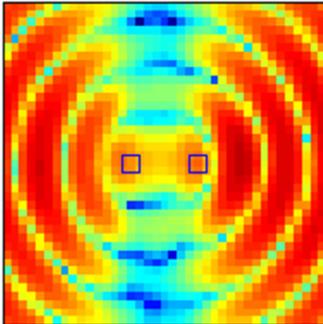


# Occulter $T_x$ & $T_z$ : Finding the Symmetric Point in $T_x$

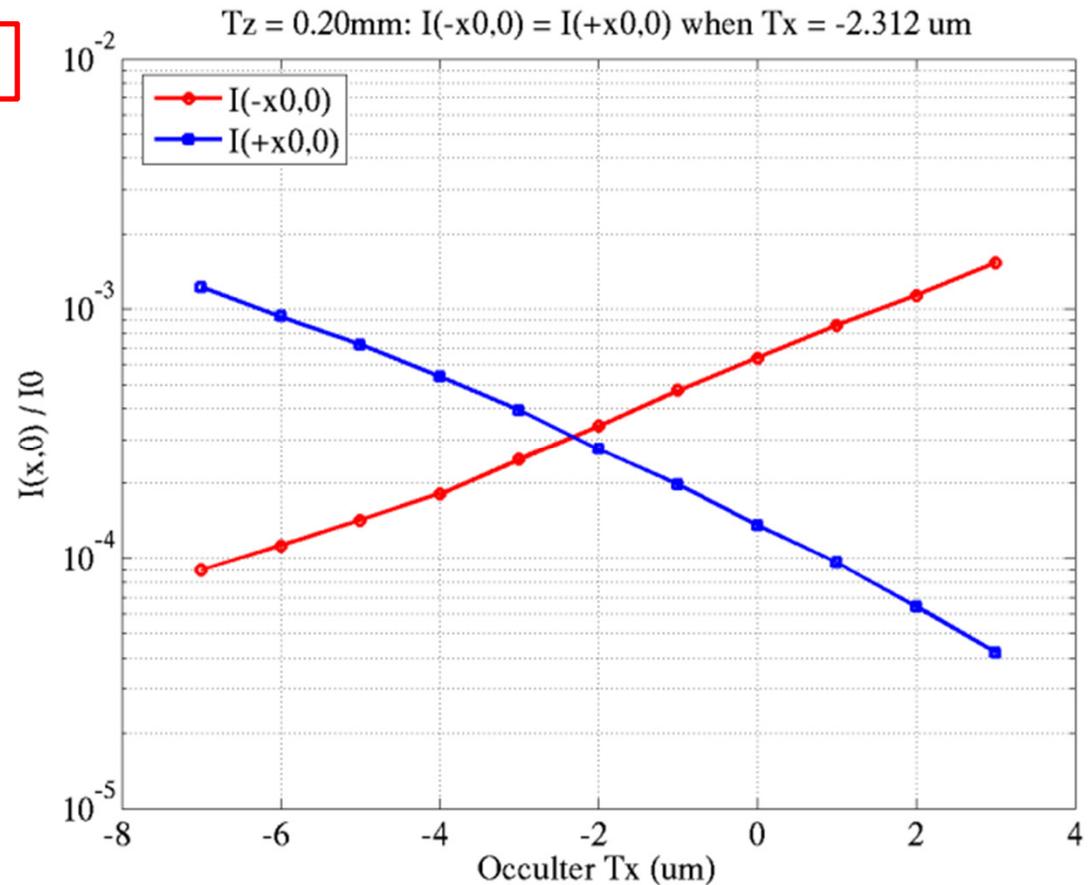
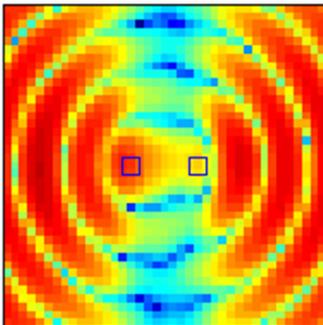
- Remove the Lyot Stop
- Move the Occulter by  $T_z$
- Move (scan) the Occulter along the x-axis to find the symmetric point  $T_{x0}$  where PSF side-lobes have the same peak value

PSF when Occulter is out

$\Delta x = -3\mu\text{m}$



$\Delta x = 1\mu\text{m}$

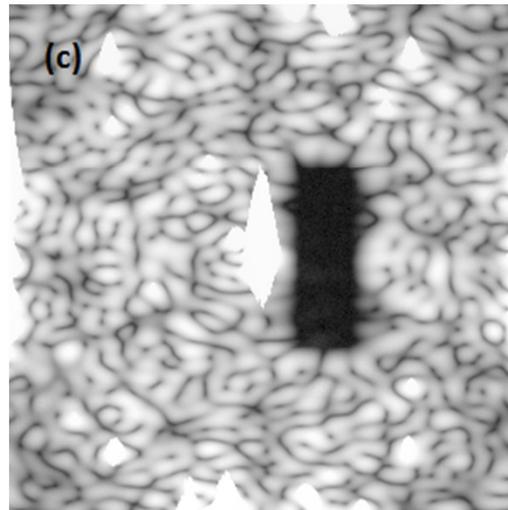


# Occulter $T_x$ & $T_z$ : Contrast Sensitivity

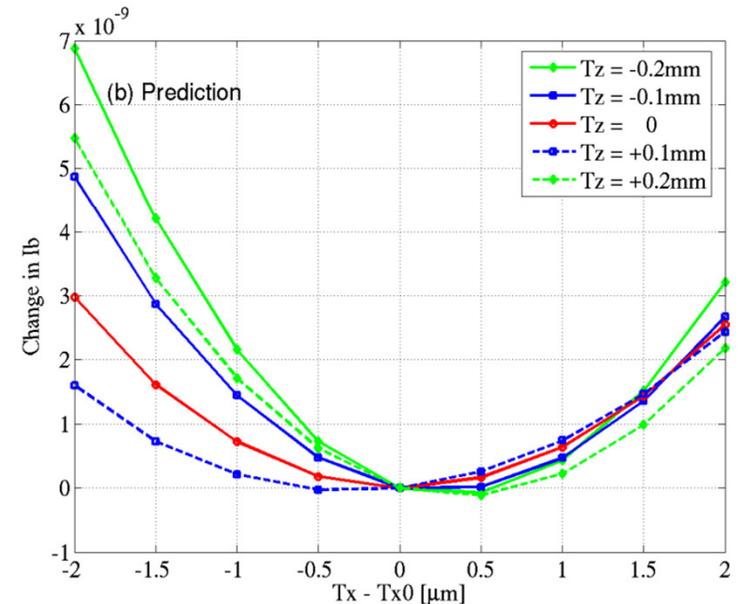
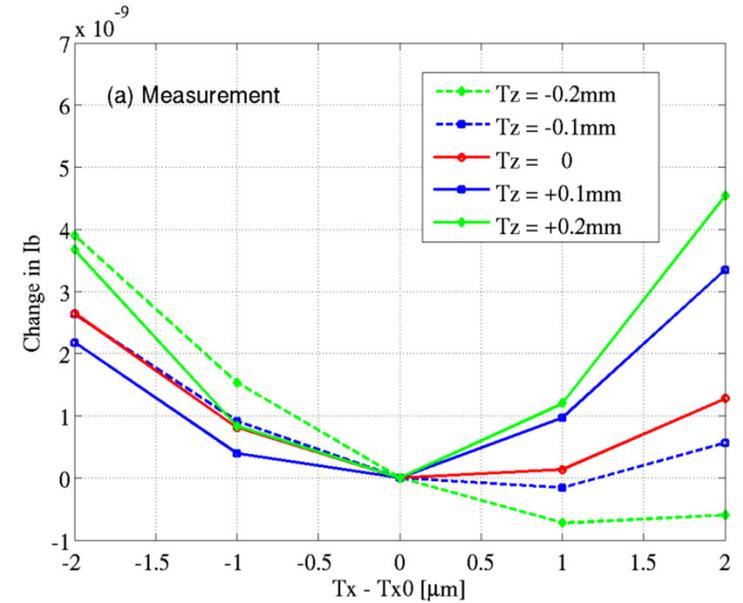
- Change in  $I(x,y)$  as a function of  $T_x$  with  $T_z$  as a parameter
- Difference between measurement & simulation:
  1.  $\lambda$ : 808nm vs 800nm
  2. Surface error maps: Magnitude and registration
  3. Occulter: Actual vs design
  4. WFC region: Rectangle vs D-shape
  5. Darkness of the dark-hole achieved

- $\Delta I(x,y)$  is not symmetric with respect to  $T_x$
- Values of  $\Delta I(x,y; T_x)$  depend on the darkness of the dark-hole achieved
- Measured & simulated  $\Delta I(x,y; T_x)$  are comparable

Measured  $I(x,y)$



$$I_b = 2.91E-9$$



# Summary

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- One to 3 dead actuators can be tolerated
  - When 1-3 crucial actuators are dead, we can still make the e-field estimation & control work by rotating or moving the DM, or by moving the probe DM pattern
- When a flat-optic moves towards and away from the dark-hole, the change in contrast exhibits an asymmetric behavior
  - Sensitivity of contrast on such motion depends on the darkness of the dark-hole achieved
  - $\Delta I_b < 2E-9$  when FM1-  $T_x = \pm 50\mu\text{m}$
- When occulter moves towards and away from the dark-hole, the change in contrast exhibits an asymmetric behavior for a given  $T_z$ -value—Same as in the case of FM1-  $T_x$ 
  - Sensitivity of contrast on such motion depends on the darkness of the dark-hole achieved
  - $\Delta I_b < 2E-9$  when Occulter-  $T_x = \pm 1\mu\text{m}$  for all  $T_z$ -values considered (-0.2 to +0.2mm)
  - Measured and simulated dependencies of contrast sensitivity on the occulter motion are comparable