



Investigation of Ruthenium Dissolution in Advanced Membrane Electrode Assemblies for Direct Methanol Based Fuel Cell Stacks

By

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Electrochemical Technologies Group



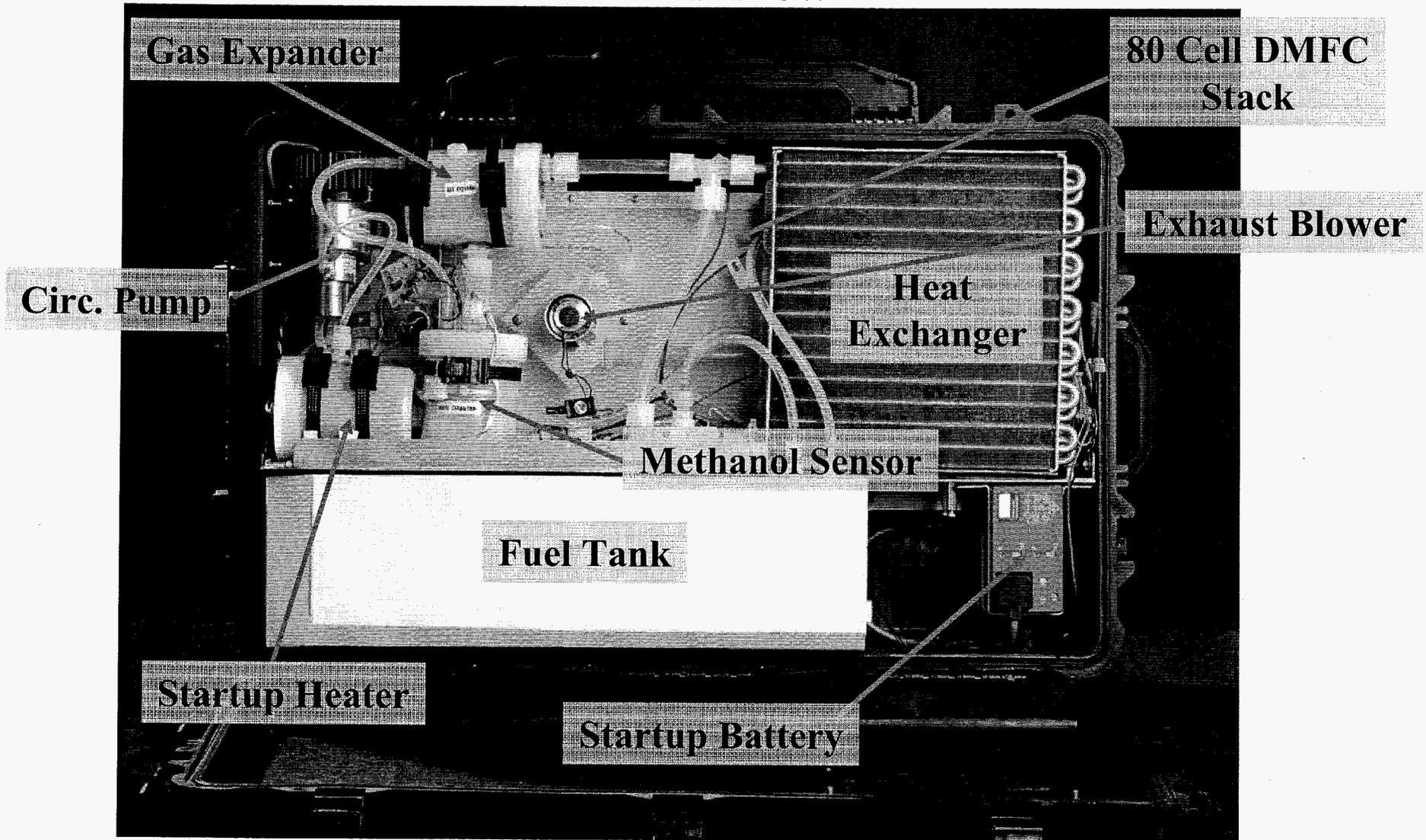
Presentation Outline

- Motivation
 - System Specifications
 - Stack Details
 - Stack Performance Degradation
 - Stack Observations
- Pathways for Cell Degradation
- Cell Duration Testing
- Duration Testing, MEA Analysis
- Stack Degradation Analysis
- Conclusions

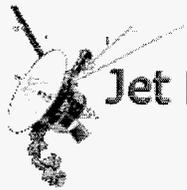


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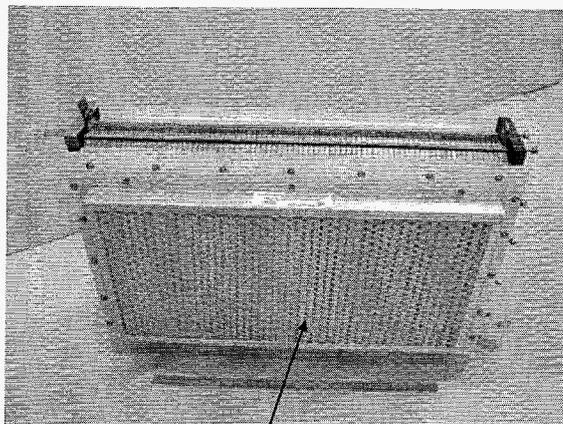
300W Direct Methanol Fuel Cell Power Source, Detailed View



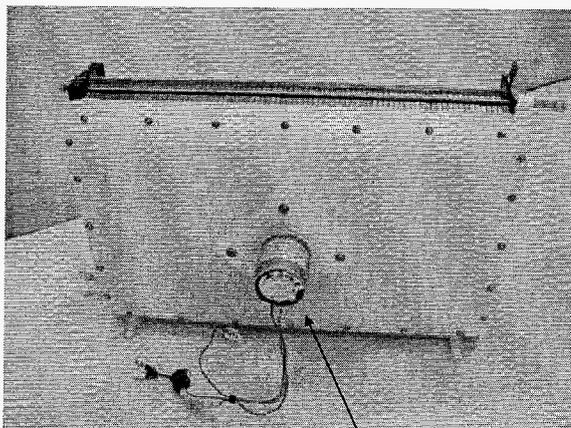
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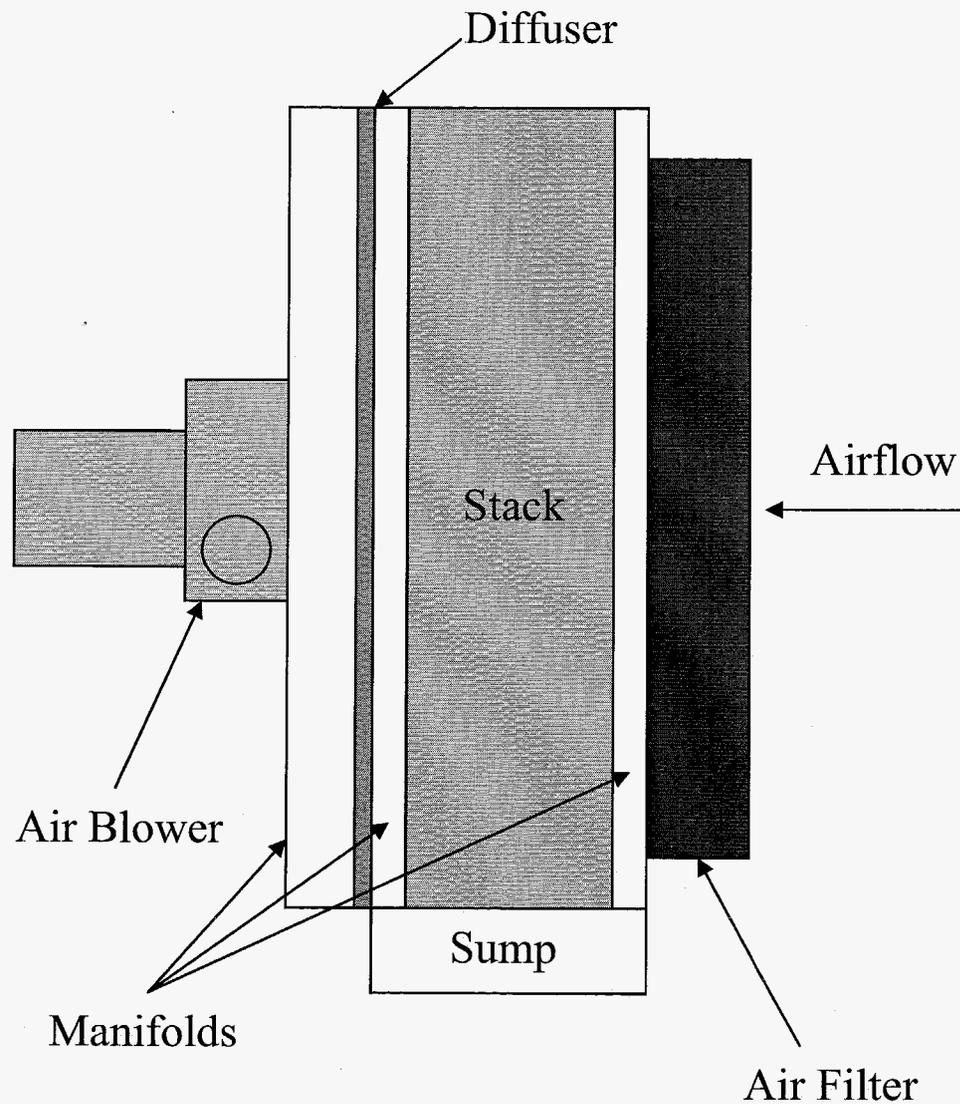
80-Cell DMFC Low Airflow Stack



Donaldson Air filter

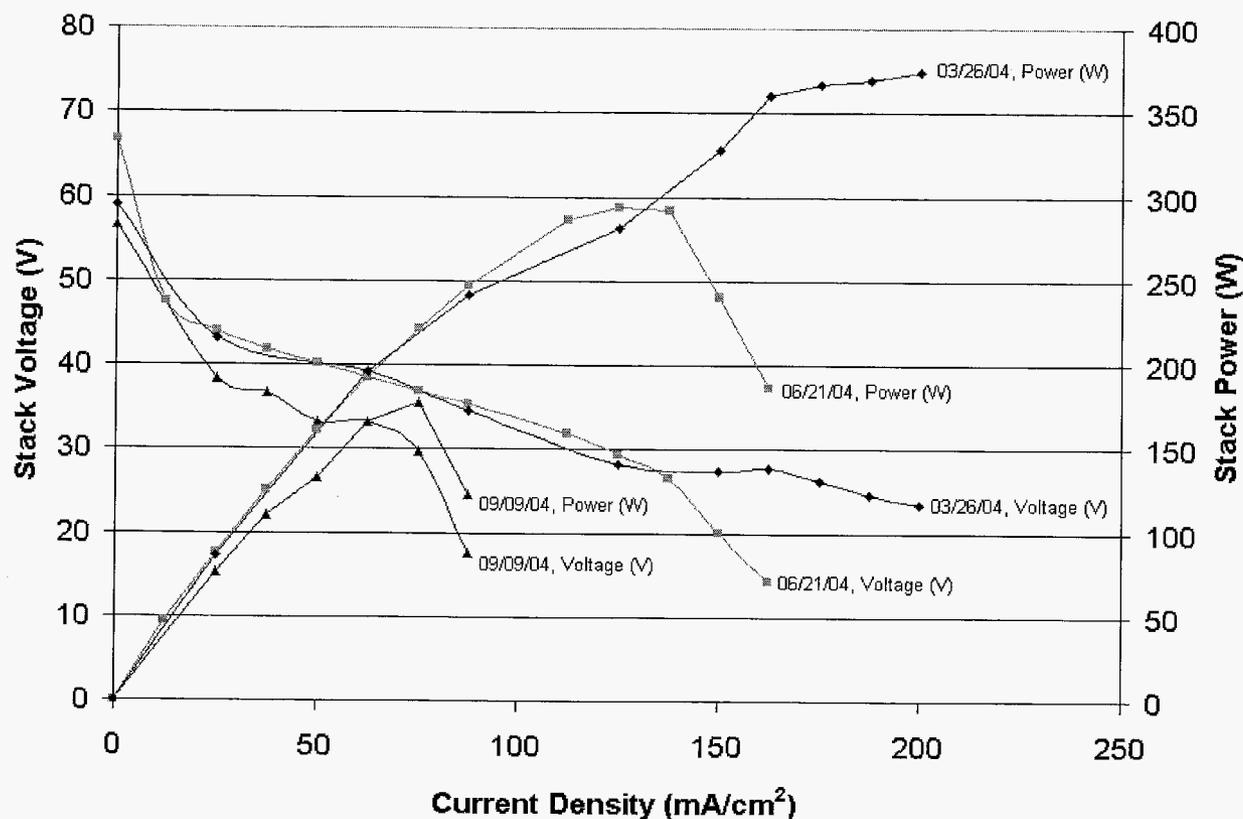


Advanced Air blower

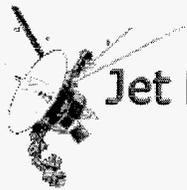




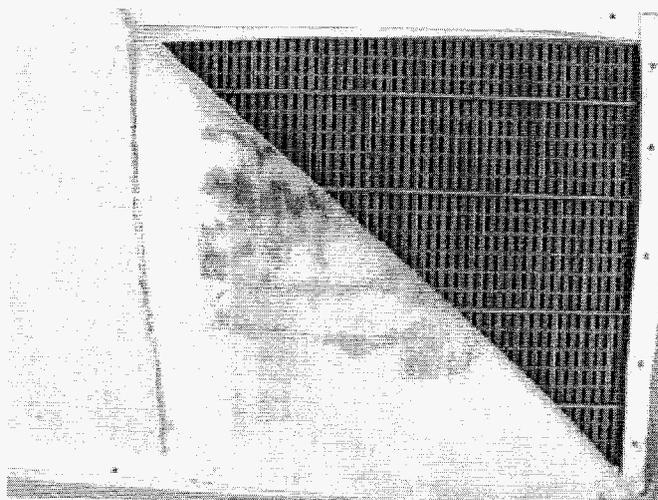
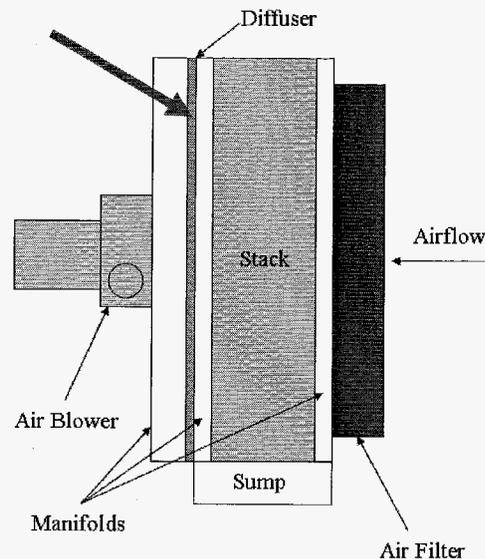
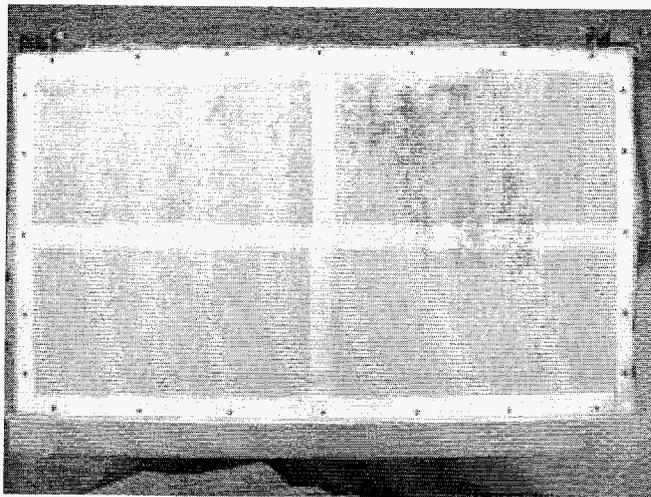
Stack Performance



- Initial stack power performance, 374 Watts
- Stack performance continuously declined over a period of less than six months
- Final stack power performance, 177 Watts



Stack Observations, Diffuser Cloth

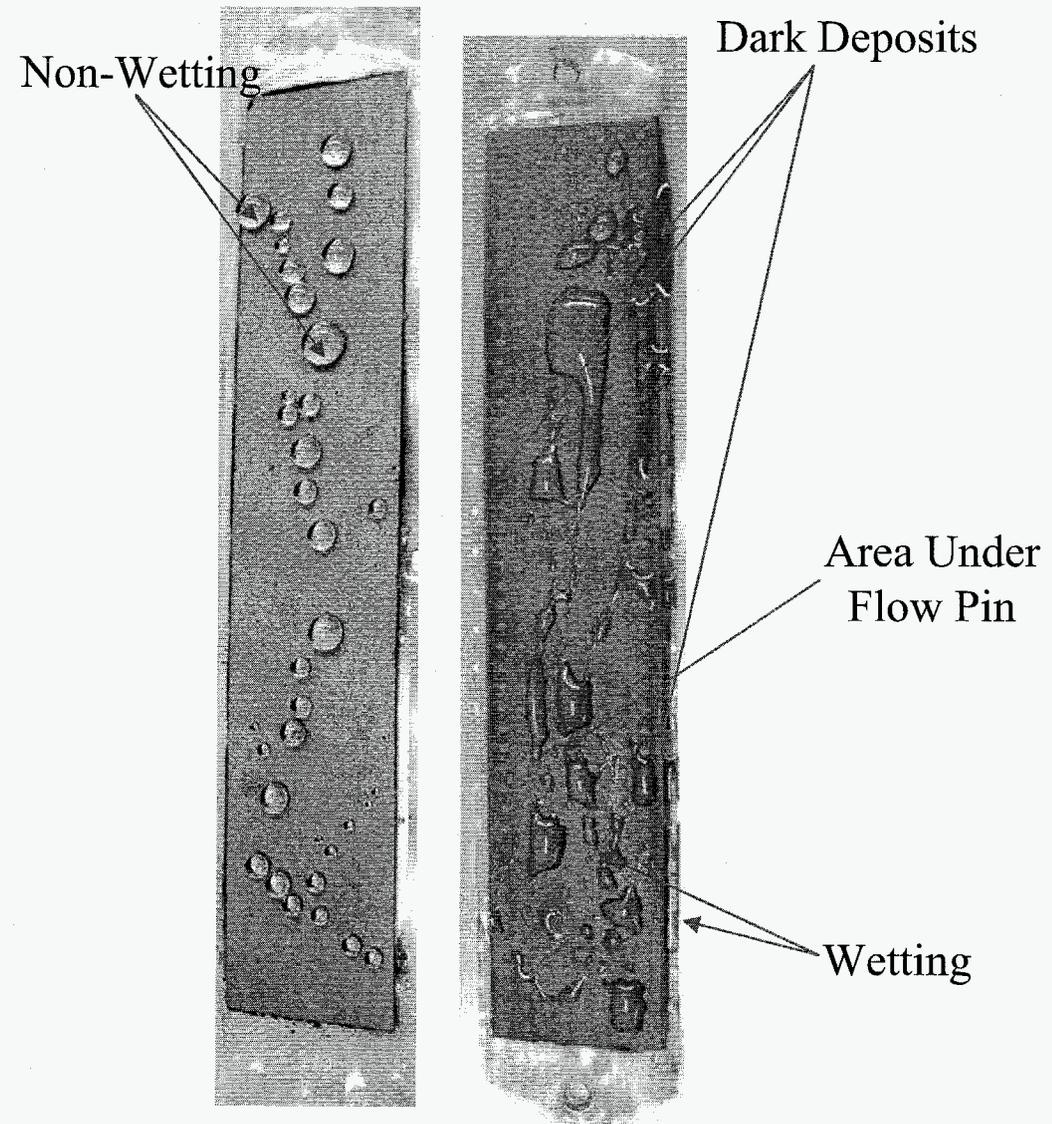


- Diffuser cloth is located at the exit of the stack
- Brownish black precipitate was identified on the cloth in contact with the stack
- Precipitate was identified as ruthenium
- ruthenium found at the cathode is washed out by water and absorbed on to the diffuser



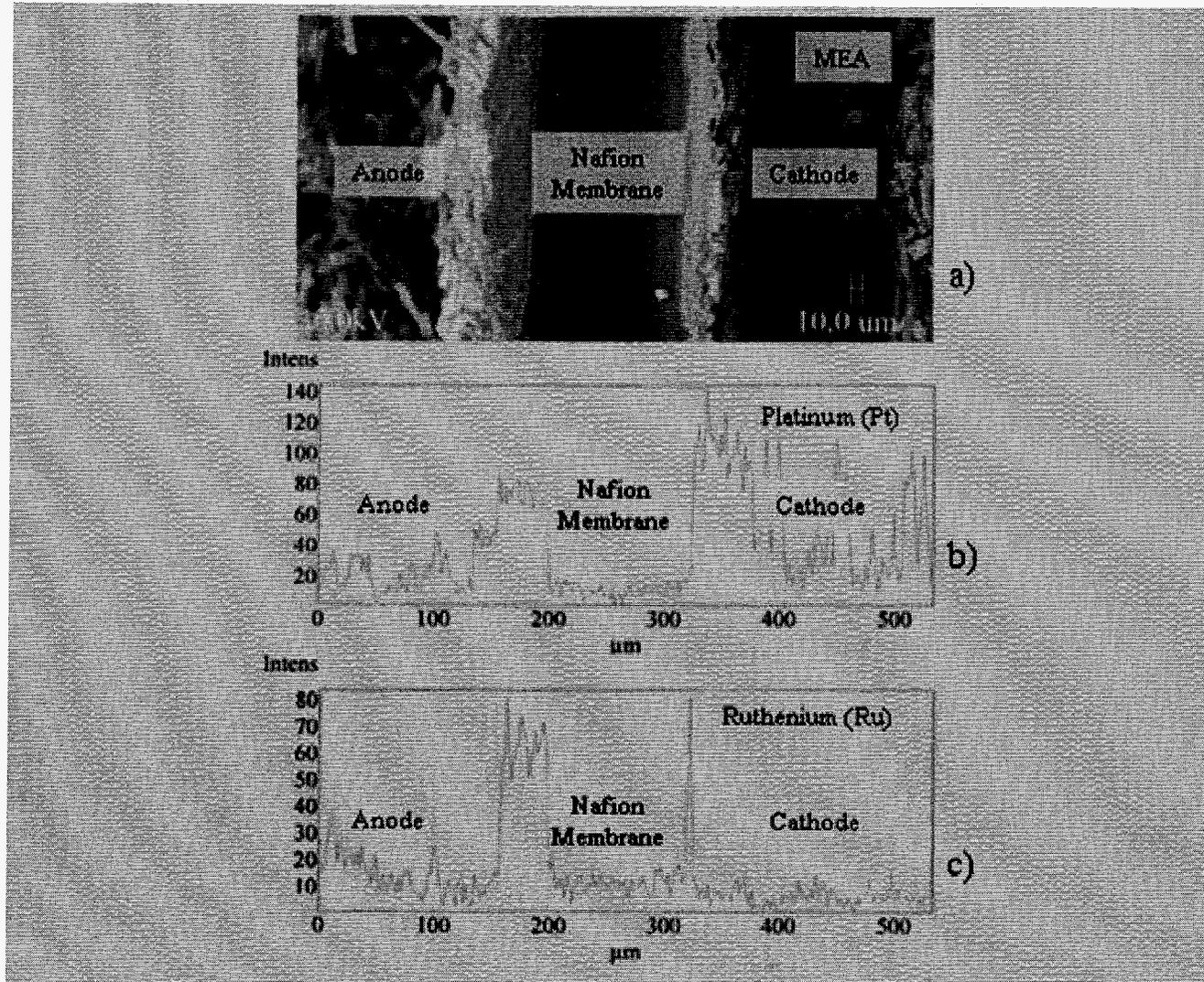
Stack Observations, MEA Observations

- Cathodes of MEAs from the stack exhibited increased wettability compared to a “fresh” MEA.
- Patches of dark gray “deposits” found on various parts of the cathode
- The areas with dark deposits were more wettable than the lighter areas.
- Several representative MEAs showed the same type of cathode changes
- Areas under the flow field pins remained “non-wettable”
- Flow field impressions were light and did not appear to damage the cathode papers





Stack Observations, EDAX Analysis of MEAs



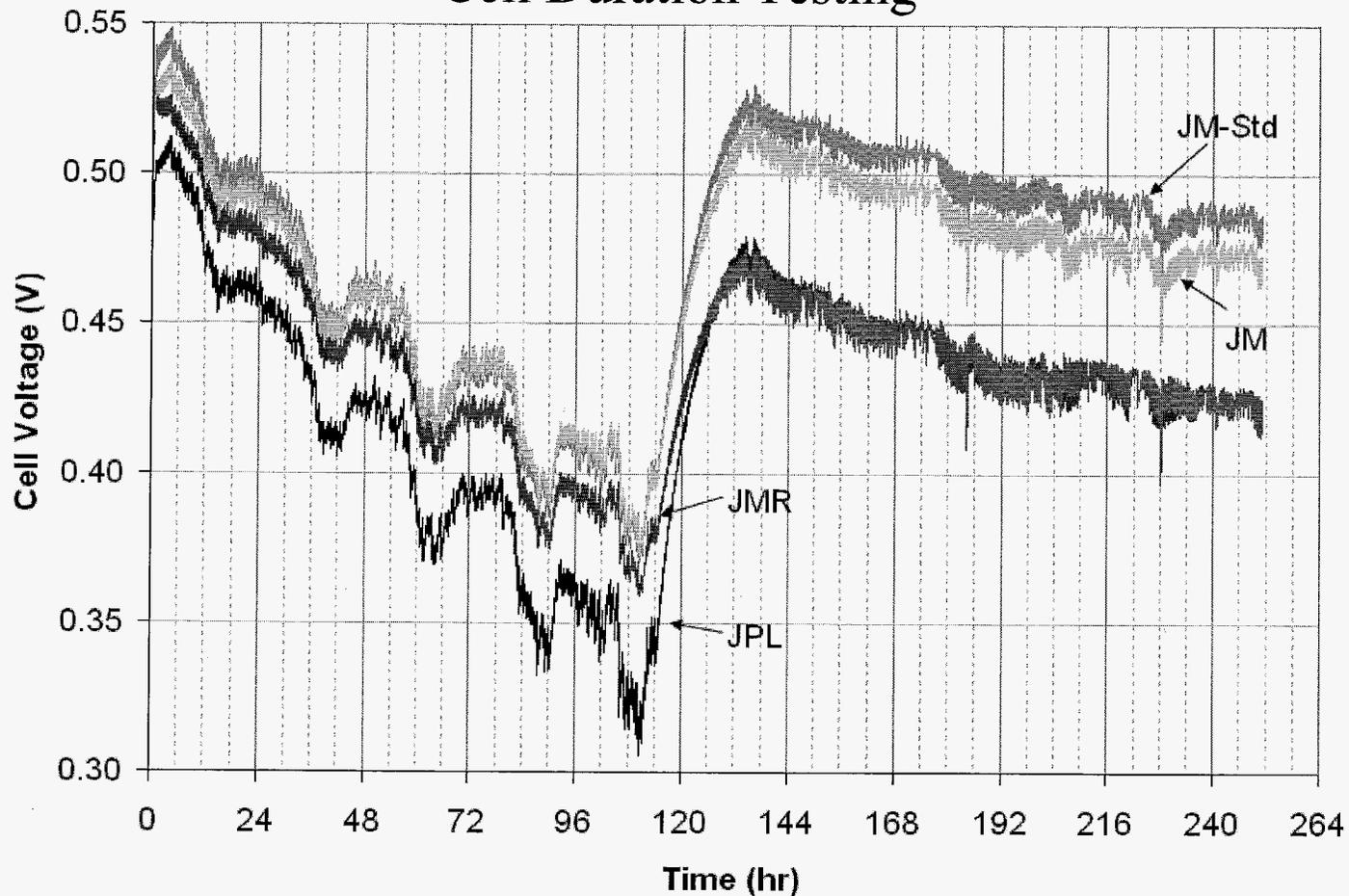


Pathways for Cell Degradation

- Hypothesis For Cell Degradation
 - Stack performance loss is caused by the ruthenium dissolution from the anode catalyst, the deposition of ruthenium at the cathode, and the loss of hydrophobicity at the cathode
 - Degradation pathways
 - Mechanisms for Ruthenium dissolution:
 - Over discharge caused by shunt currents
 - *Instability of platinum-ruthenium commercial catalyst*
 - Mechanisms for Loss of hydrophobicity at the cathode:
 - *Inadequate Teflon content*
 - Deposition of RuO₂ at the cathode
- Experimental
 - Two degradation pathways were investigated, the **stability of platinum-ruthenium commercial catalyst** and the **cathode backing Teflon content**
 - MEAs Fabricated
 - JPL, Anode: JPL-prepared Pt-Ru, Pt Cathode, 15% Teflon backing
 - JM, Anode: Johnson Matthey Pt-Ru, Pt Cathode, 15% Teflon backing
 - JMR, Anode: Reduced Johnson Matthey Pt-Ru, Pt Cathode, 15% Teflon backing
 - JM-STD, Anode: Johnson Matthey Pt-Ru, Pt Cathode 5% Teflon backing (Standard or control MEA)



Cell Duration Testing



- 250 hours of continuous testing complete
- The decrease in cell performance in the initial hundred hours of testing is a result of sensor calibration
- The slopes of the voltage curves after 134 hours are also controlled by methanol concentration control
- In general, the JM-Standard MEA performed the best



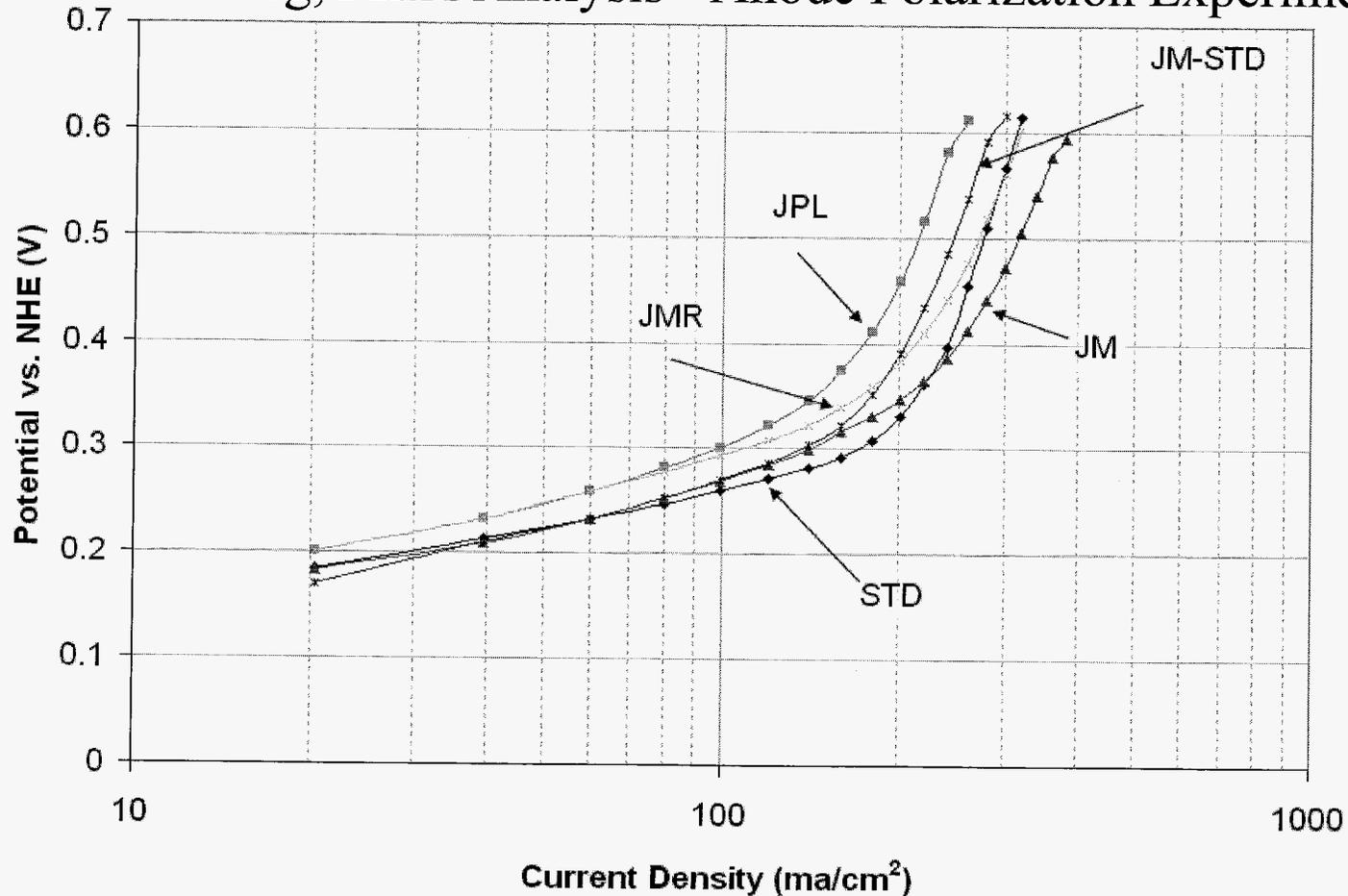
Duration Testing, MEA Analysis - Post 250-hr Testing Performance Summary

MEA	Formulation	Performance Decline (mV)		Performance Decline (mW/cm ²)		Rate of Decay (V/hr)	
		50 mA/cm ²	100 mA/cm ²	50 mA/cm ²	100 mA/cm ²	50 mA/cm ²	100 mA/cm ²
JPL	Anode: JPL Cathode: 15% Teflon	48	150	2.4	15	0.00019	0.0006
JM	Anode: Johnson Matthey Cathode: 15% Teflon	6	67	0.3	6.7	0.00002	0.00027
JMR	Anode: Reduced Johnson Matthey Cathode: 15% Teflon	30	107	1.5	10.7	0.00012	0.00043
JM-STD	Anode: Johnson Matthey Cathode: 5% Teflon (Standard)	6	96	0.3	9.6	0.00002	0.00038

- MEA “JPL” logged 20 more hours of testing than any other MEA
- MEAs fabricated with the commercial Johnson Matthey catalyst showed the least performance decline
- The MEA fabricated with Johnson Matthey anode catalyst and 15% Teflon content cathode paper, showed slightly lower performance decline at high current densities than the MEA fabricated with Johnson Matthey anode catalyst and 5% Teflon content cathode paper
- The MEA fabricated with the reduced Johnson Matthey anode catalyst performed similar to the MEA fabricated with the JPL catalyst
- The test standard performed the best during the durability experiments
- The rate of voltage decay for all MEAs tested is similar to values observed in the past



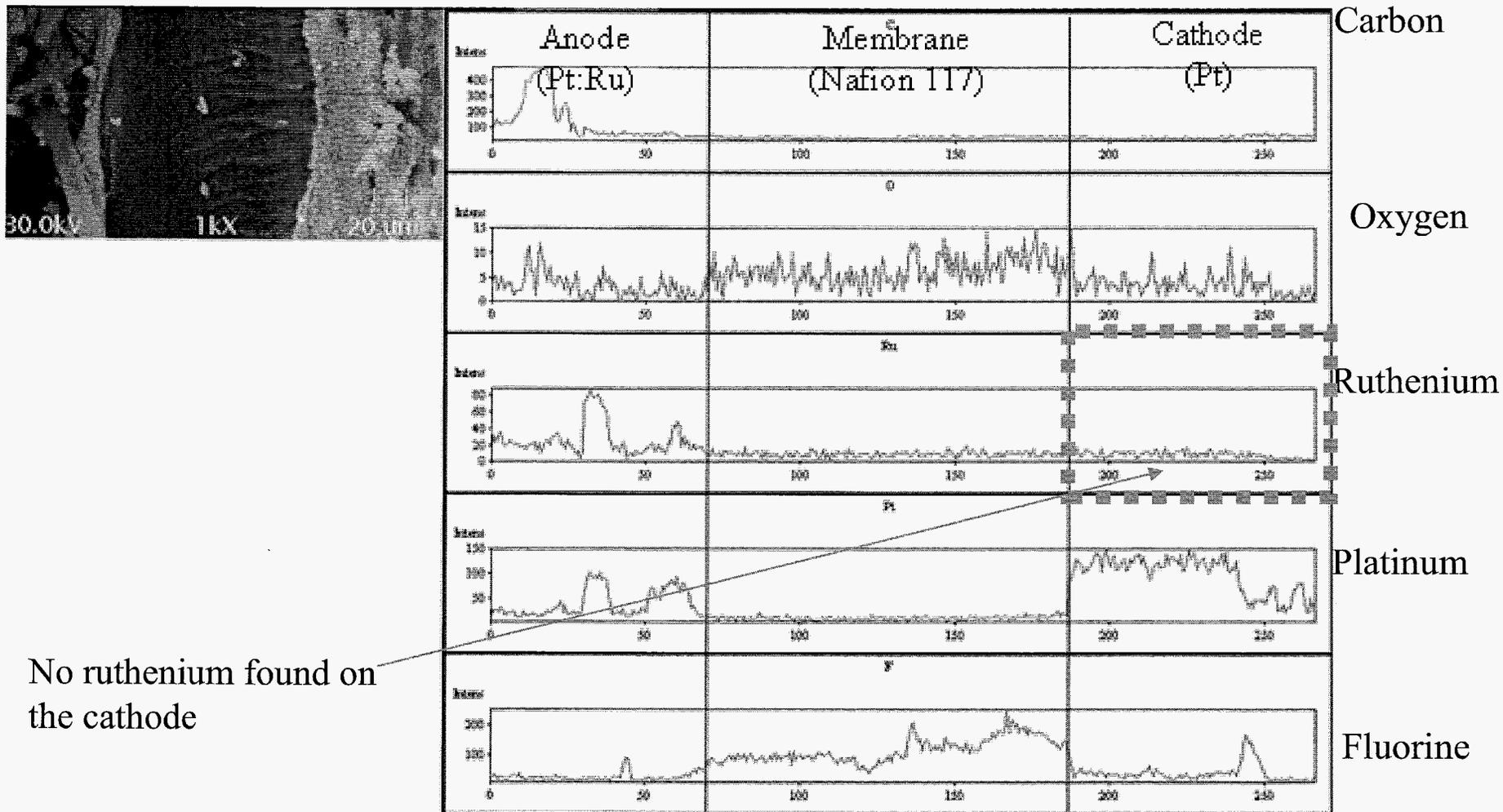
Duration Testing, MEA Analysis - Anode Polarization Experiments



- Anode polarization analysis of the cell post duration experiments reveal no changes anode performance



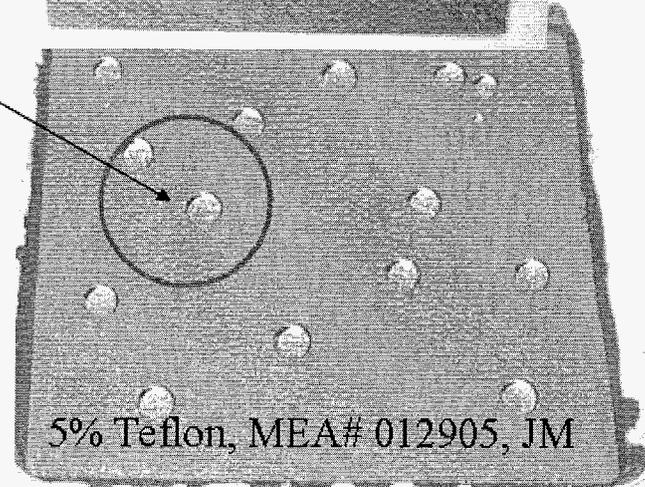
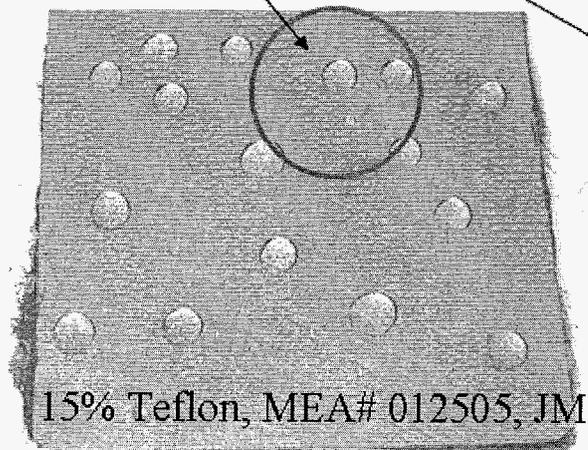
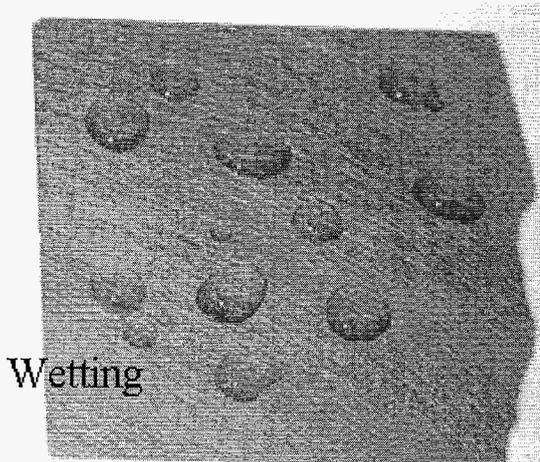
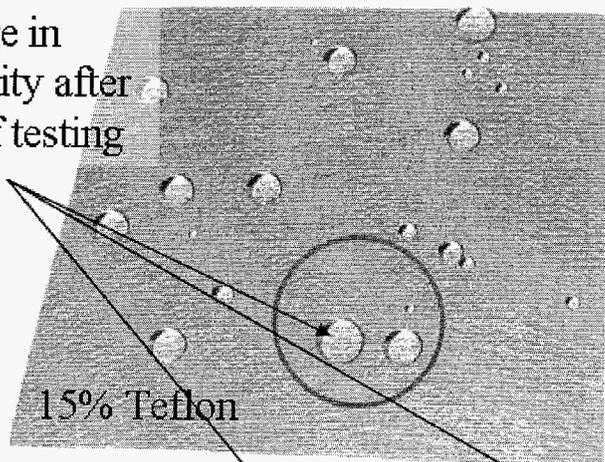
Duration Testing, MEA Analysis - EDAX Analysis





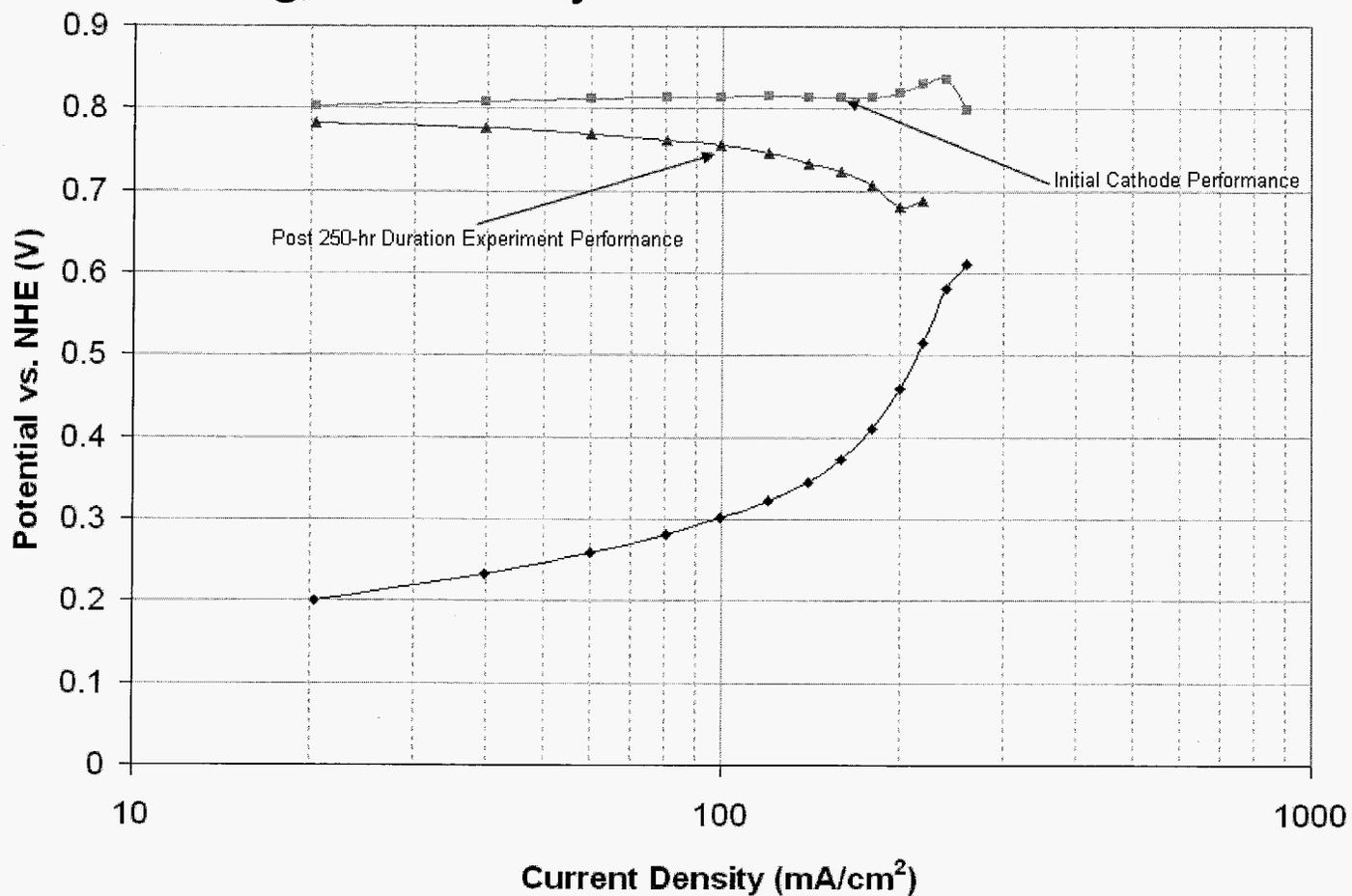
Duration Testing, MEA Analysis - Cathode Hydrophobicity Comparisons

Slight change in hydrophobicity after 250 hours of testing





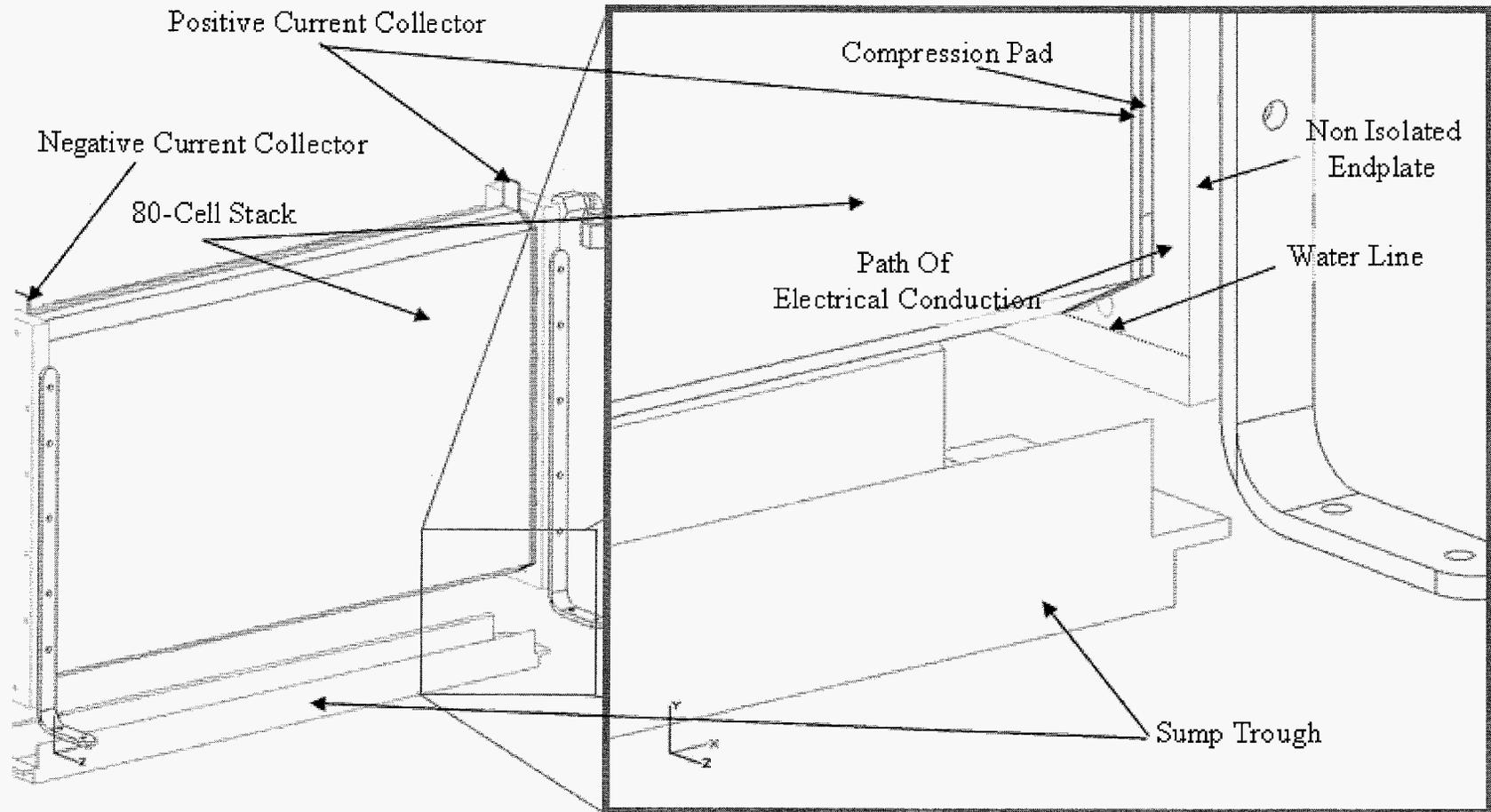
Duration Testing, MEA Analysis - Anode and Cathode Performance

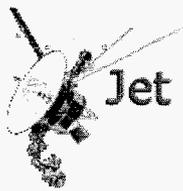


- MEA performance degradation is attributed to losses in cathode performance

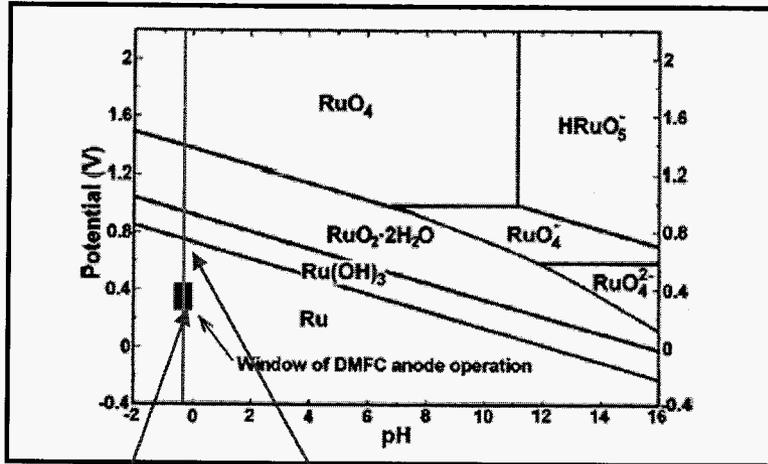


80-cell stack current collection hardware

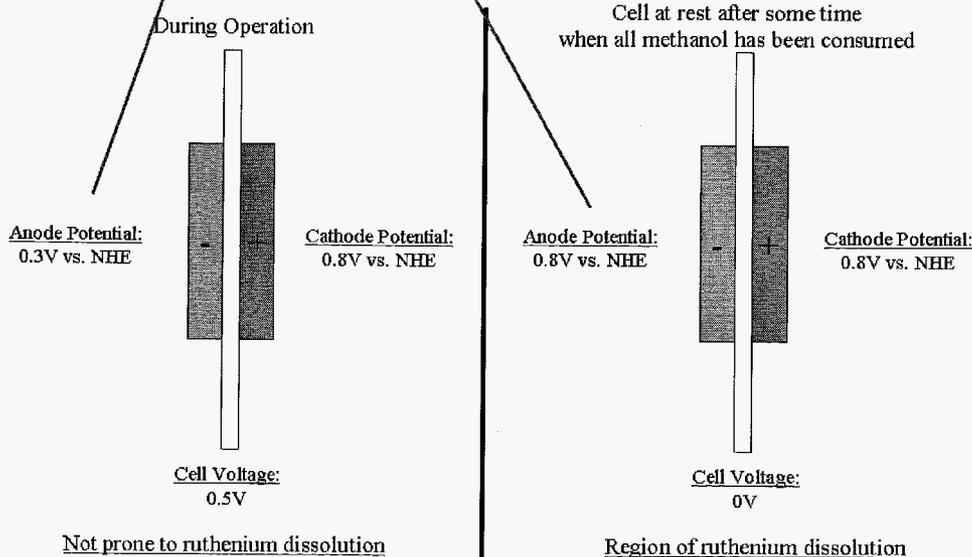
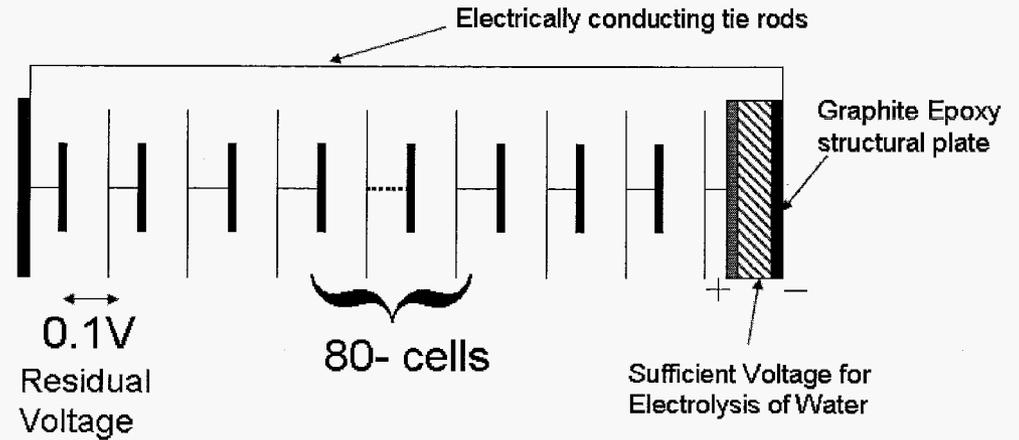




Stack Degradation Analysis – Over-discharge



*P. Pielak, C. Eickes, E. Brosha, F. Garzon and P. Zelenay, Ruthenium Crossover in Direct Methanol Fuel Cell, J. of The Electrochemical Society, 151 (12) A2053-A2059, 2004



1. Reactions without methanol at the anode:
 Anode: $2\text{Ru} \rightarrow 2\text{Ru}^{3+} + 6\text{e}^-$
 Cathode: $3/2\text{O}_2 + 6\text{H}^+ + 6\text{e}^- \rightarrow 3\text{H}_2\text{O}$
2. Ru^{3+} migrates through the Nafion membrane
3. Cathode: $2\text{Ru}^{3+} + 3\text{H}_2\text{O} + 1/2 \text{O}_2 \rightarrow 2\text{RuO}_2$ (black) + 6H^+

Not prone to ruthenium dissolution

Region of ruthenium dissolution



Conclusions

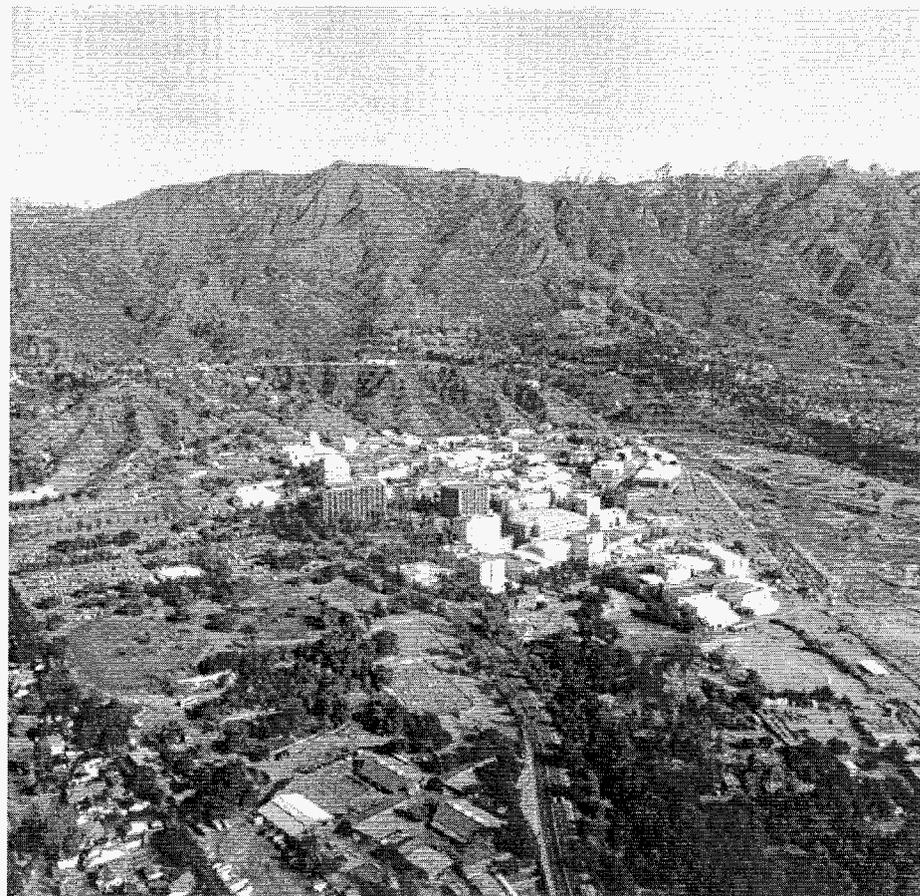
- Dissolution of ruthenium was observed in the 300-Watt system stack
- Duration testing was performed in cells to determine the pathway of cell degradation, no ruthenium dissolution was observed for cells after 250 hours of operation
- EDAX analysis on each of the MEAs has shown that the Johnson Matthey commercial catalyst is stable in DMFC operation for 250 hours
- Ruthenium migration does not seem to occur during cell operation
- Dissolution of ruthenium occurs when methanol is absent from the anode compartment, the cathode compartment has access to air, and the stack is electrically connected to a load (Shunt Currents).
- Stack design allowed for conditions in which the anode could experience elevated potentials for long durations and allow for ruthenium dissolution
- The open-to-air cathode and water collecting trough of this stack design allowed for:
 - The MEAs access to oxygen
 - The system to sustain shunt currents
 - Water accumulated at the manifolds that blocked uniform airflow to portions of the stack and may have contributed to shunt currents
- To prevent ruthenium dissolution, a stack should be designed that can address fuel cell reaction product water removal, allow for uniform airflow to each cell, and limit shunt currents
- Ruthenium dissolution can be prevented by
 - Developing an internally manifolded DMFC stack
 - Insulate the structural endplates from the stack
 - Limit to total number of cells to 25 to limit the shunt currents



Acknowledgements

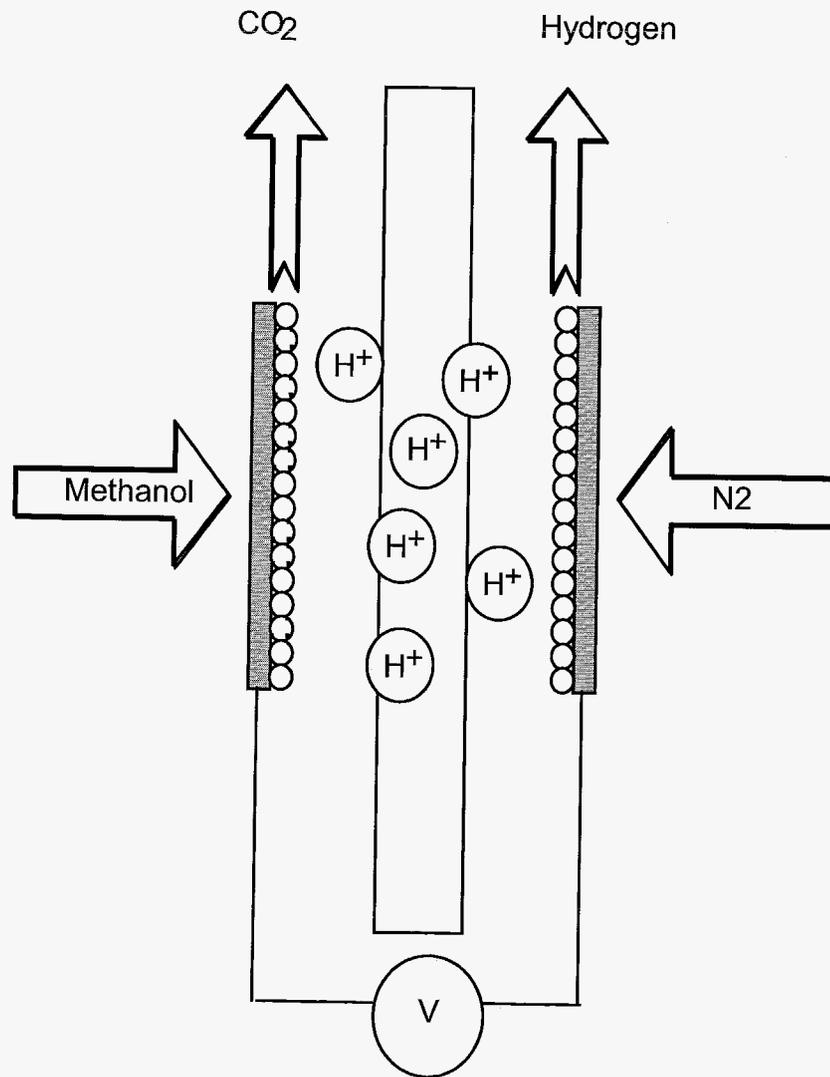


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Anode Polarization Subtraction



- Test Set-up
 - Nitrogen is introduced into the cathode compartment of the fuel cell. The cathode of the fuel cell now becomes a dynamic hydrogen electrode.
 - When the cell is polarized, the resultant curve will be E_a vs. current density at the chosen operating temperature of the cell.
- Polarization Analysis
 - E_{cell} , at any air flow rate, can be added to E_a at the same molarity and temperature to get E_c corresponding to the flow rate.
$$E_c = E_{cell} + E_a$$
 - When E_a and E_c are plotted together as a function of current density, the kinetics of the reaction can be seen.