



# Progress Status of Skutterudite-Based Segmented Thermoelectric Technology Development

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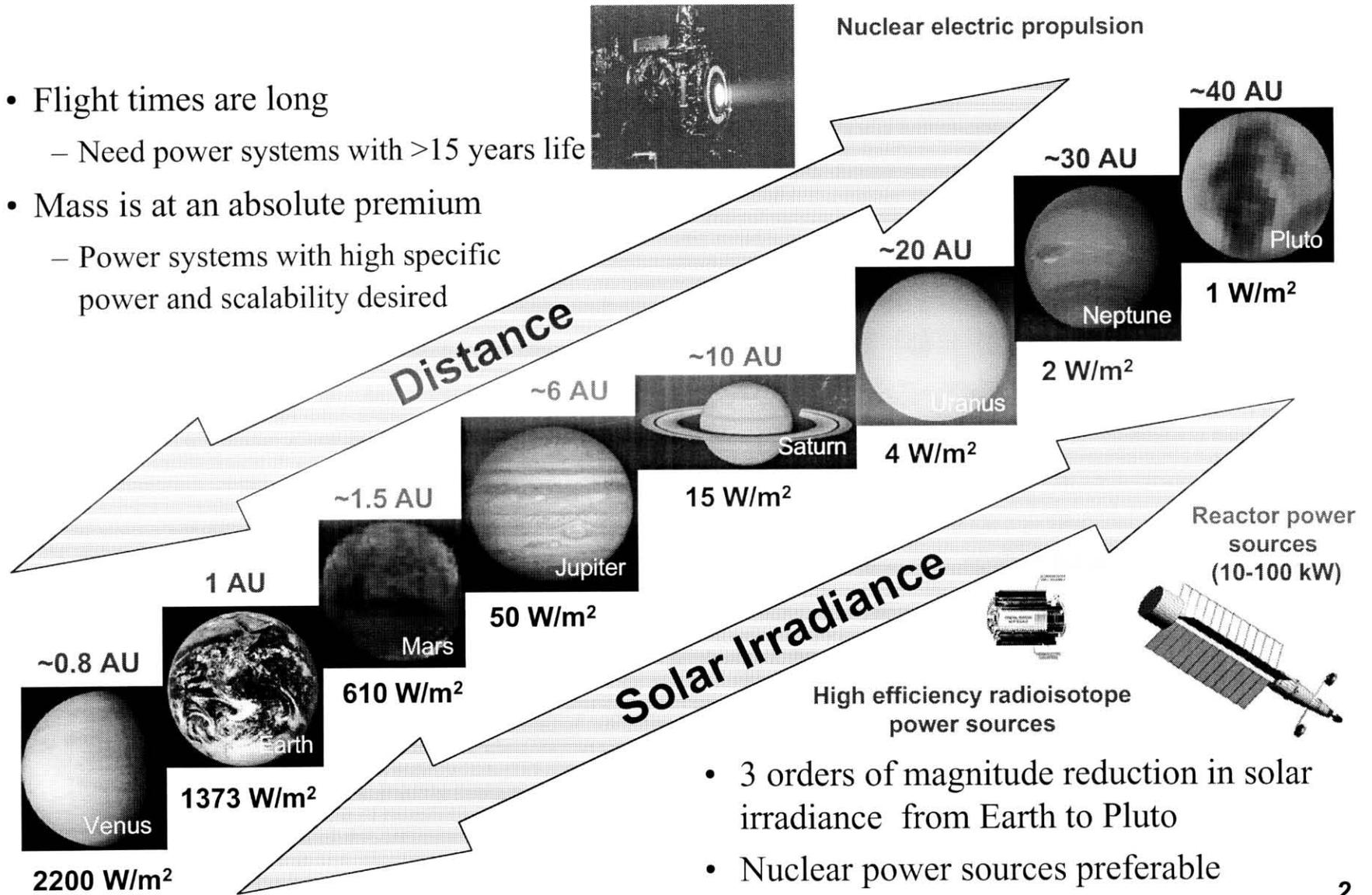
### Acknowledgements:

**Prof. M. El-Genk (University of New Mexico)**  
**NASA (Project Prometheus), ONR & DARPA**



# Power Technology

- Flight times are long
  - Need power systems with >15 years life
- Mass is at an absolute premium
  - Power systems with high specific power and scalability desired



- 3 orders of magnitude reduction in solar irradiance from Earth to Pluto
- Nuclear power sources preferable



## Advanced Radioisotope Power Systems (APRS) for NASA missions

- Overall objective

Develop low mass, high efficiency, low-cost Advanced Radioisotope Power System with double the Specific Power and Efficiency over state-of-the-art radioisotope thermoelectric generators (RTGs)

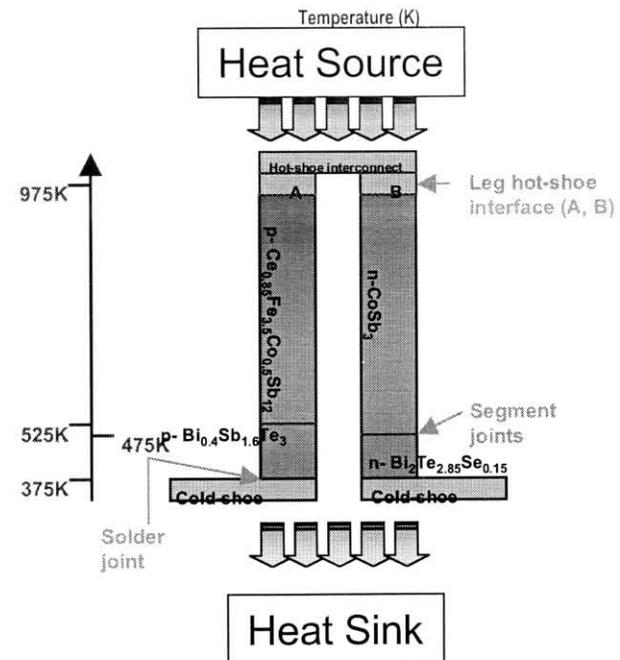
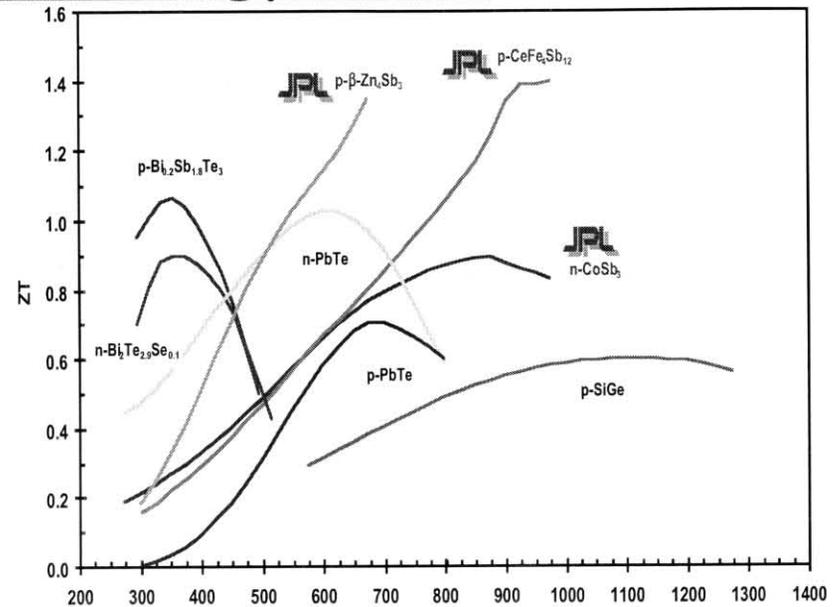


# Segmented Thermoelectric Technology (STE)



- **New high ZT materials**
  - Development initiated in 1991 and supported by ONR and DARPA (Skutterudites and  $Zn_4Sb_3$ )
  - Substantial increase in efficiency over state-of-the-art
- **Segmented uncouples**
  - Large  $\Delta T$ , high ZT  $\rightarrow$  high efficiency
  - Using a combination of state-of-the-art TE materials ( $Bi_2Te_3$ -based materials) and new, high ZT materials developed at JPL
    - Skutterudites :  $CeFe_4Sb_{12}$  and  $CoSb_3$
    - $Zn_4Sb_3$
  - Current new materials operation limited to  $\sim 975K$
  - Higher average ZT values
  - $\rightarrow$  Higher material conversion efficiency
    - $\rightarrow$  Up to 15 % for a 300-975K temperature gradient

Efficiency  $\eta = \frac{T_H - T_C}{T_H} \frac{\sqrt{1 + ZT} - 1}{\sqrt{1 + ZT} + \frac{T_C}{T_H}}$





# JPL Segmented Thermoelectrics (STE) Task overview



## Overall objectives

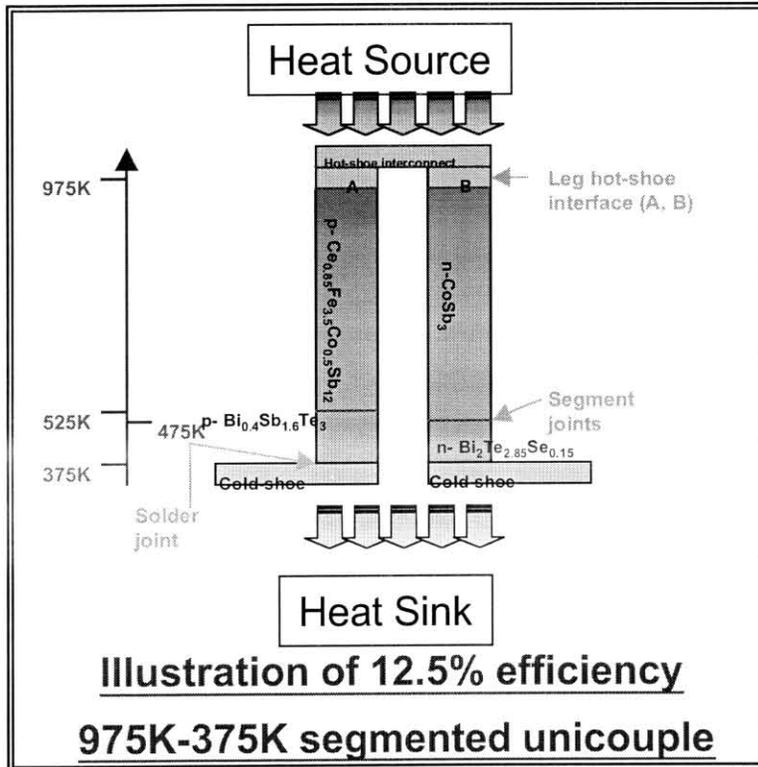
- Develop Segmented Thermoelectric technology to from TRL 3 to TRL4 by end of FY06
- Transfer technology to industry/DOE for integration into a radioisotope power system that can provide  $\sim 7\text{-}8 \text{ W}_e/\text{kg}$  specific power and  $\sim 10\%$  system efficiency

## FY04-06 Major Goals

- Optimize uncouple fabrication technique
- Develop a uncouple thermo-mechanical model
- Perform life testing of STE materials, coupons, components and uncouples
- Further develop sublimation control techniques/materials
- Develop lifetime model

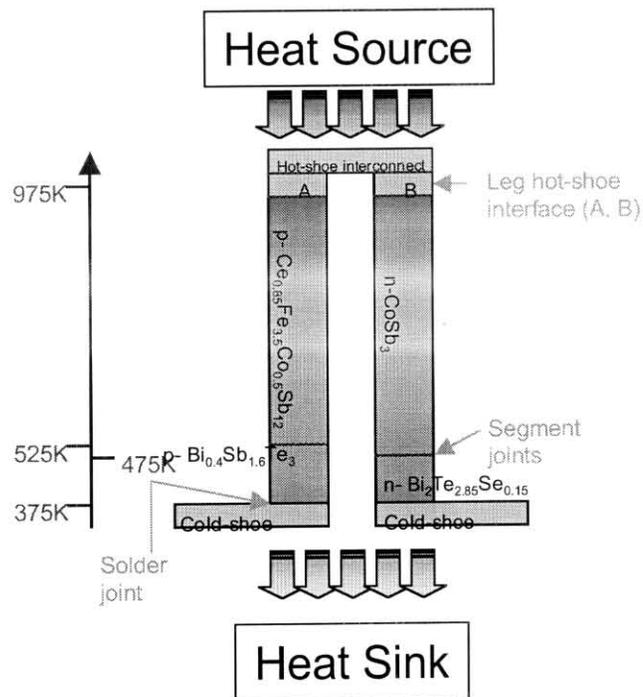
## Schedule

Top-level Tasks	FY04	FY05	FY06
Uncouple development	—◆		
Baseline TE materials/coupons life testing and modeling			◆
Uncouple/components life testing			◆
Uncouple/TE materials optimization			◆
Manage and report			◆





# Key Technology Challenges

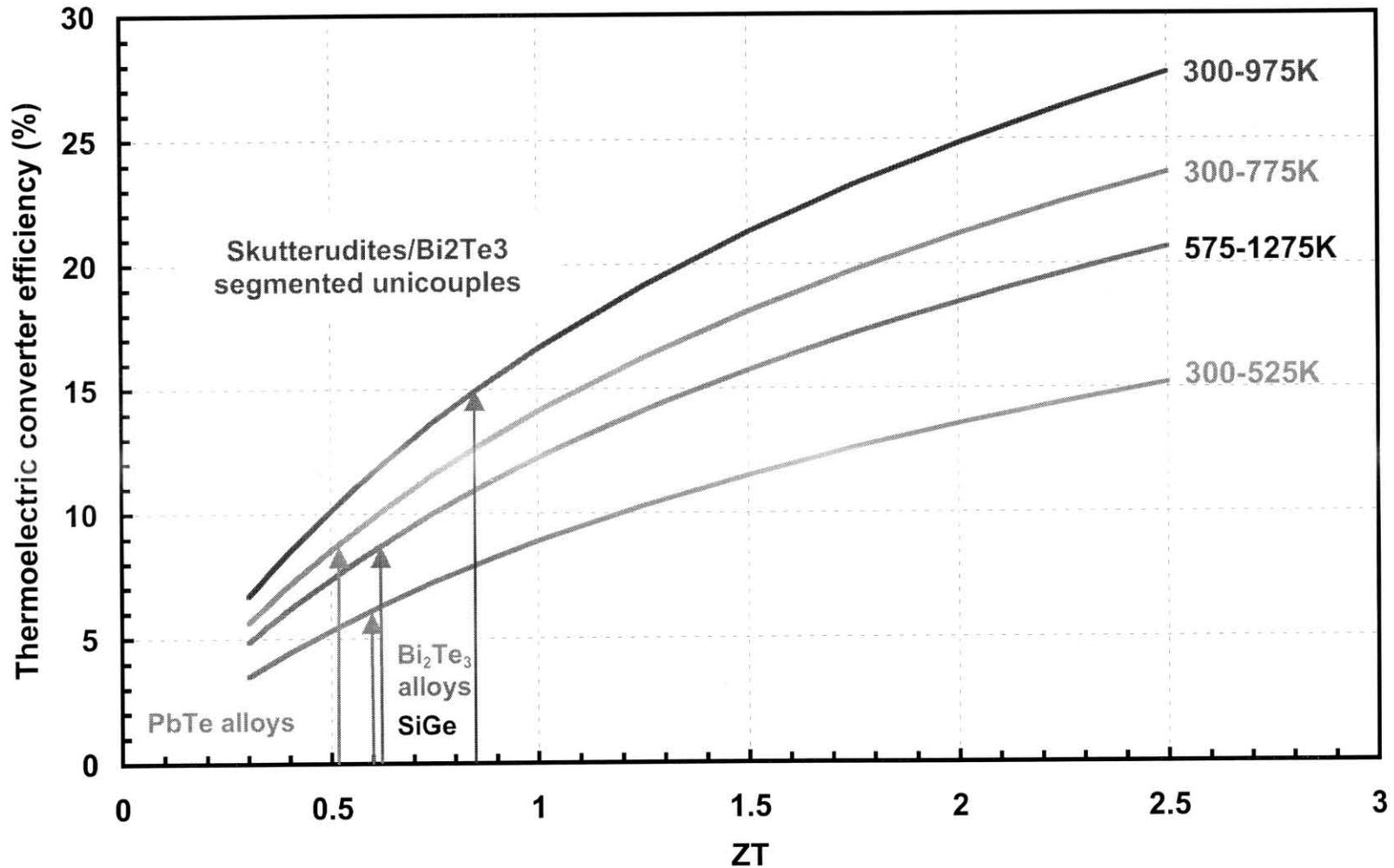


## Key technology challenges

- TE materials processing and segmented leg fabrication
- Low electrical contact resistance between segments and between segments and cold- and hot-shoes
- Unicouple mechanical integrity
- Lifetime
  - Sublimation control
  - Stable thermoelectric properties
  - Life time prediction model
- Demonstrate unicouple performance
  - Testing and modeling



# Converter efficiency : state-of-the-art vs. segmented thermoelectric technology



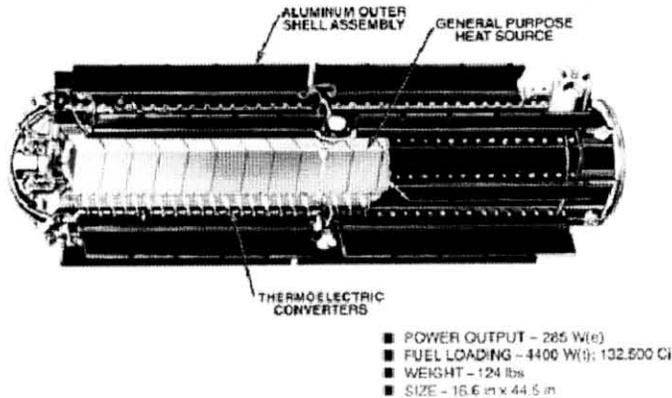
A 2x increase in efficiency over SOA thermoelectrics has been demonstrated for the STE technology



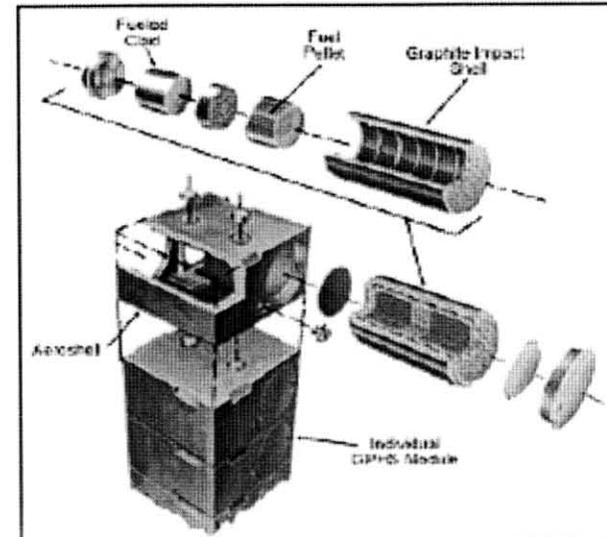
# General Purpose Heat Source RTG



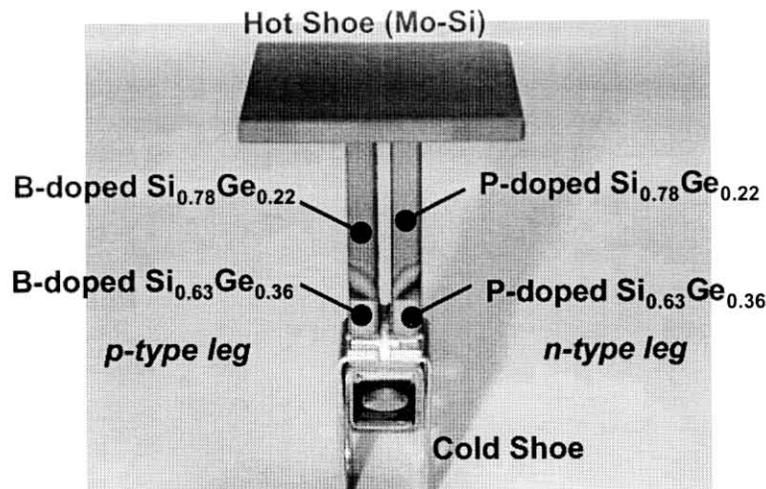
## General Purpose Heat Source (GPHS) Radioisotope Thermoelectric Generator (RTG)



The three Radioisotope Thermoelectric Generators (RTGs) provide electrical power for Cassini's instruments and computers. They are being provided by the U.S. Department of Energy.



General Purpose Heat Source Module



GPHS SiGe unicouple

### GPHS-RTG Performance Data

Power output-We	290 beginning of life 250 end of life
Operational life - hrs	40,000 after launch
Weight-kg	55.5
Output voltage	28
Dimensions	42.2 diameter 114 long
Hot junction temperature-K	1270
Cold junction temperature-K	566
Fuel	PuO <sub>2</sub>
Thermoelectric material	SiGe
Numbers of unicouples	572
Mass of Pu-238-g	7,561



# STE-ARPS

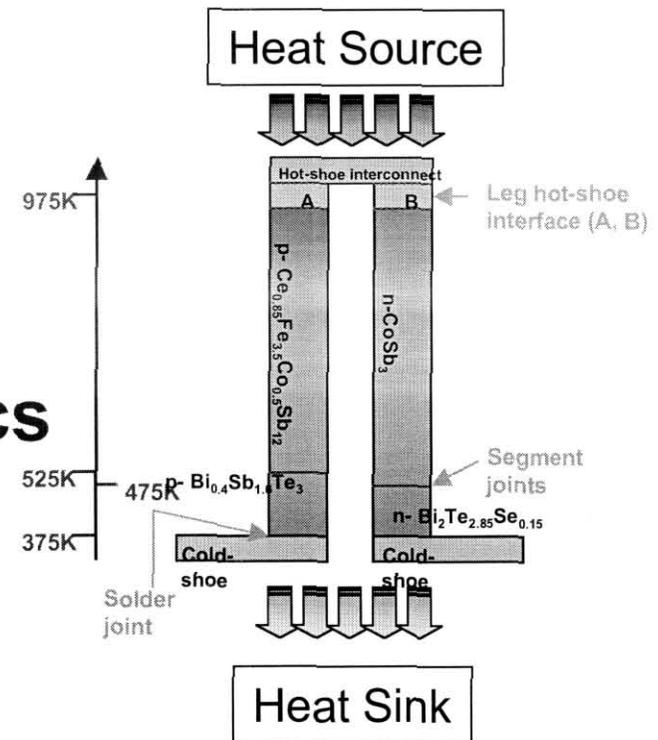


## •STE-ARPS

- Would use advanced materials segmented legs
  - 700 to 100°C operation
  - Current GPHS-RTG uncouple design would be mostly conserved
  - Modifications required to radiator fins to accommodate for lower rejection temperature
  - Shorter housing
- New segmented uncouples could “replace” uncouples almost “one for one”

## •Advantages of thermoelectrics

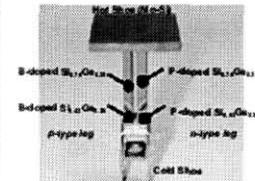
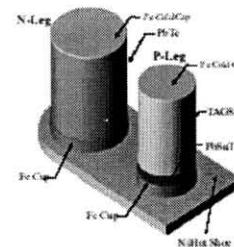
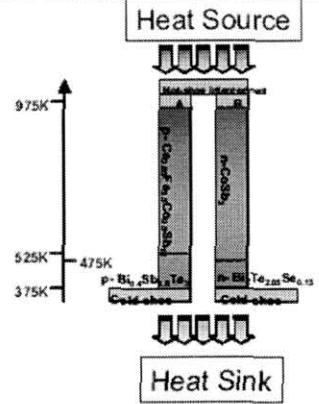
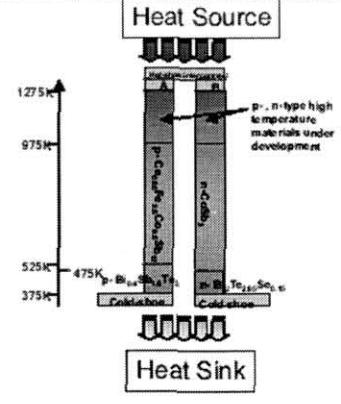
- Flight proven, long life demonstrated
- Solid state energy conversion -> reliability, no vibration, no moving parts
- Scalable
- No single point failure
- Significant system heritage





# Projected STE 100W class ARPS specifications vs. SOA

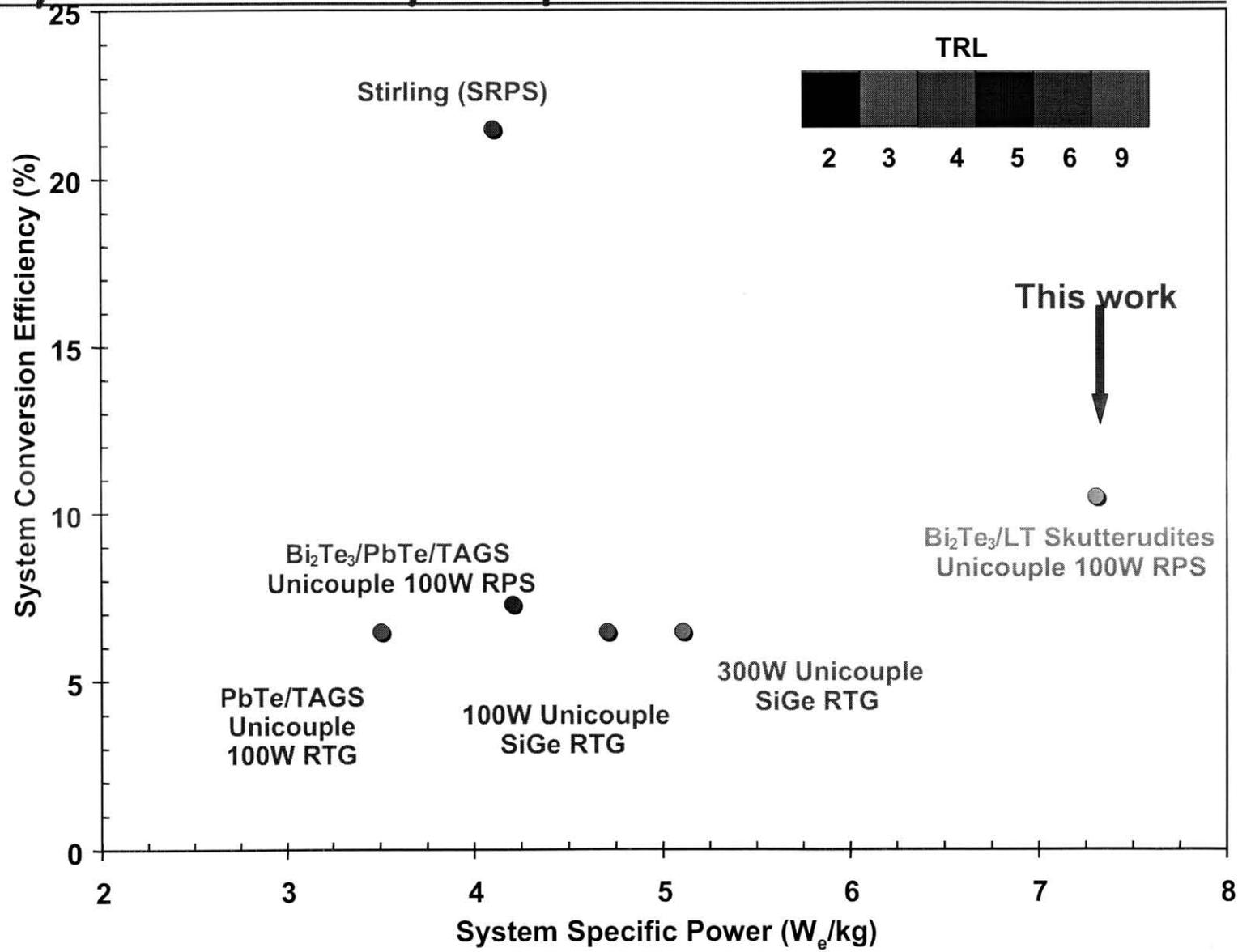


Item/Converter	SiGe-RTG	PbTe/TAGS MMRTG	Low T STE (LSTE)	High Temperature TE (HSTE)
Hot side temperature (K)	1273	823	975	1200
Cold side temperature (K)	573	453	375	375
Converter efficiency (%)	7.2	7.6	12.5	14.7
System efficiency (%)*	6.5	6.4	11.18	13.3
Thermal power (BOM)( $W_{th}$ )	2000	2000	1250	1000
Thermal efficiency (%)	85		85	85
Electrical power (BOM) ( $W_e$ )	107	110	118.8	113.0
Number of modules	8	8	5	4
Total PuO <sub>2</sub> mass (kg)	5.02	5.02	3.138	2.51
Total system mass estimate (kg)	23.24	38.1	16.3	13.1
- GPHs mass (kg)	11.54	12.83	7.215	5.77
- Housing (Kg)	3.1	4.2	1.90	1.55
- Radiator fins (kg)	0.45	3.32	1.7	1.36
- Converter (kg)	5.65	10	3.9	3.12
- Other structure (kg)	2.5	5.5	1.6	1.28
Specific power estimate ( $W_e/kg$ )	4.6	2.88	7.28	8.64
Unicouples				

\* 90% of converter efficiency



# System Efficiency & Specific Power: STE vs. SOA





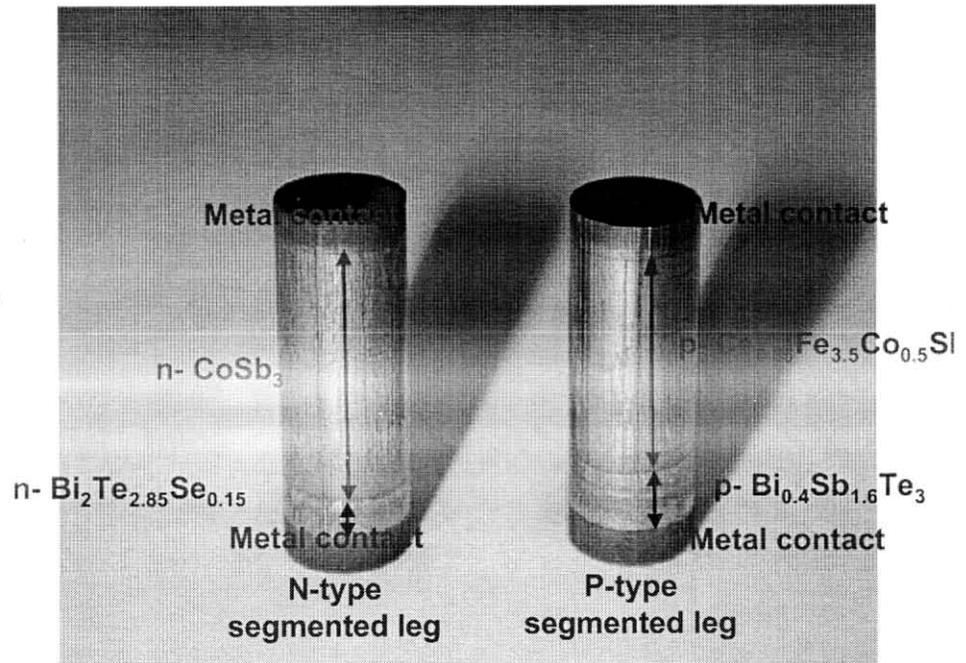
# **Segmented legs fabrication and characterization**



# Unicouples legs



- **Developed uniaxial hot-pressing technique for legs fabrication**
  - Powdered materials stacked on the top of each other
  - Temperature optimized → density close to theoretical value
  - In graphite dies and under argon atmosphere
  - With metallic diffusion barriers between the TE materials
  - **Metallic contacts at hot- and cold-side**
  - **Low electrical resistance bonds ( $<5\mu\Omega\text{cm}^2$ ) achieved → negligible impact on overall uncouple performance**

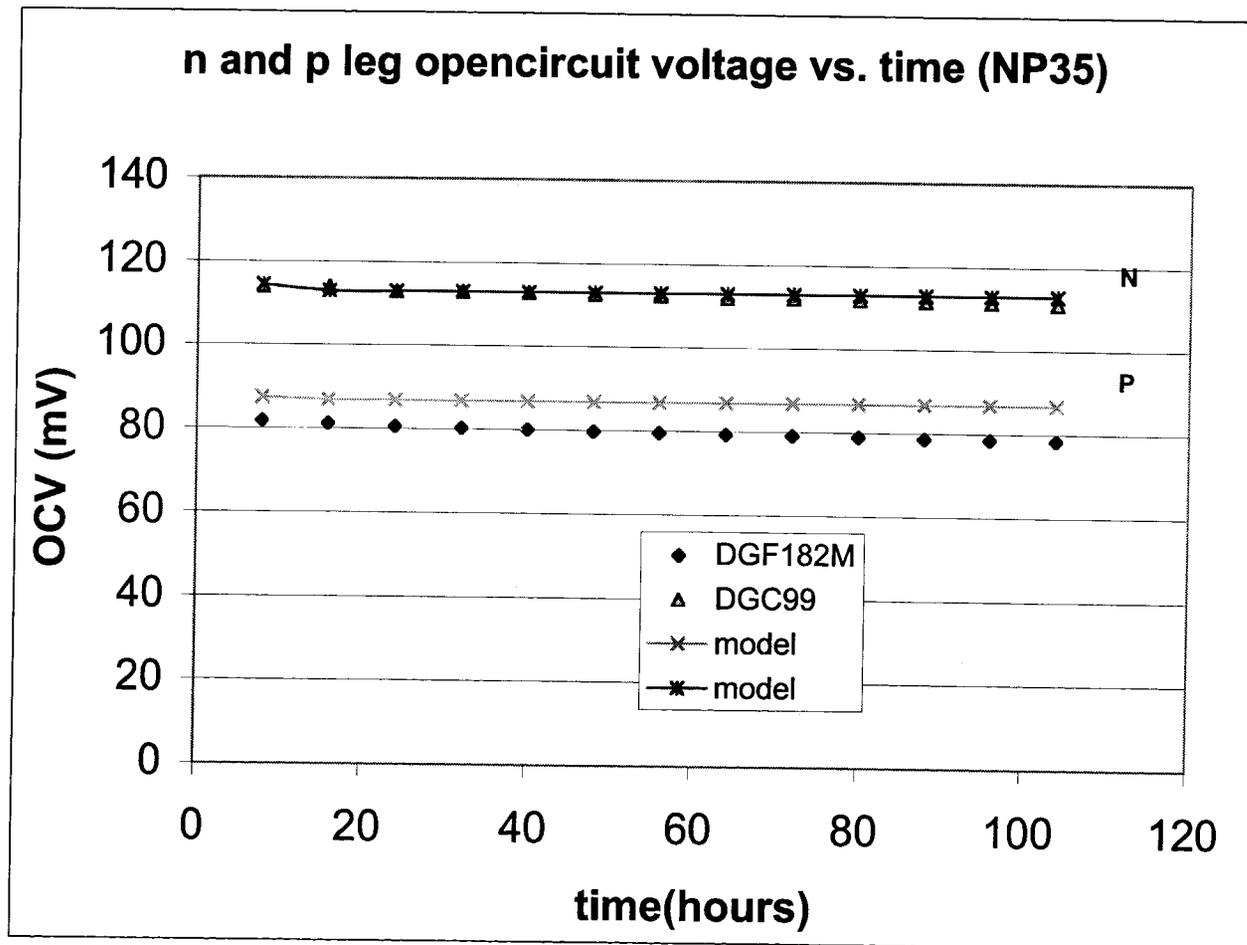




# Unicouple legs - In-gradient testing



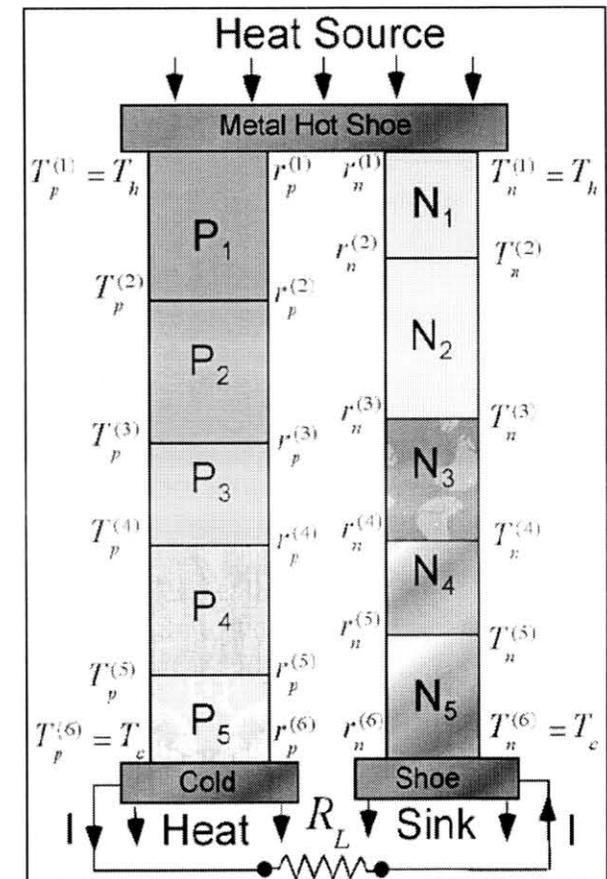
- N- and p-type in gradient (975K-350K) testing of n- and p-skutterudite legs confirm model performance prediction and show little voltage decrease after ~ 100 hours of testing





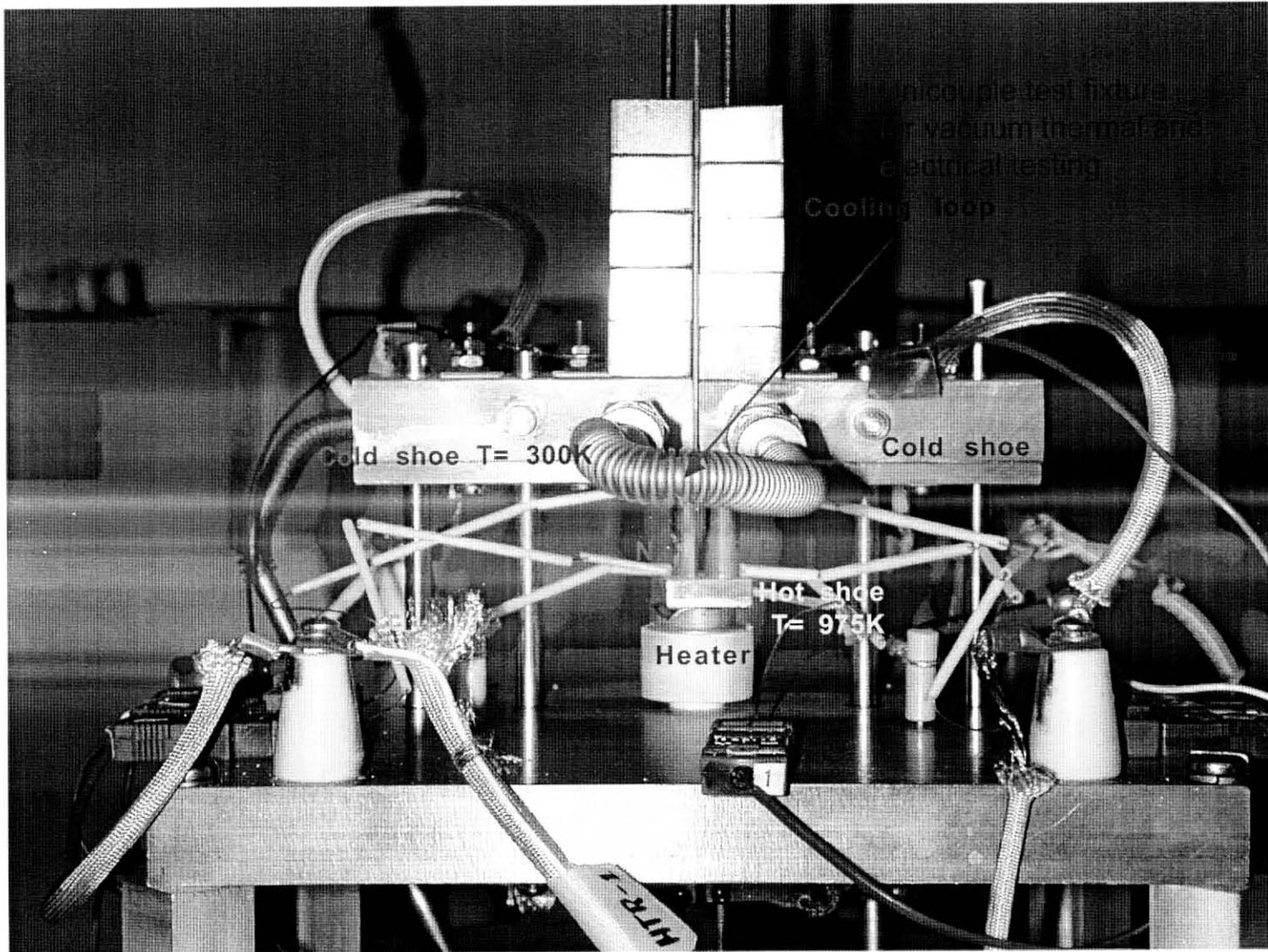
## 1-D Analytical Model of Segmented Thermoelectric Unicouples

- One-dimensional analytical model of STEs, with up to 5 segments per leg, is coupled to a *genetic algorithm* for maximizing either electrical power or efficiency
- **Input:**
  - TE materials properties
  - Total length and composition of n- and p-legs
  - Cross sectional area of the p-leg (or the n-leg)
  - Hot and cold shoe temperatures
  - Total contact resistance per leg
- **Output**
  - Number of needed segments in n- and p-legs
  - Interface temperatures between various segments
  - Lengths of various segments in n- and p-legs
  - Cross sectional area of n-leg and p-legs
  - Electrical power and conversion efficiency curves
  - Operation I-V characteristics



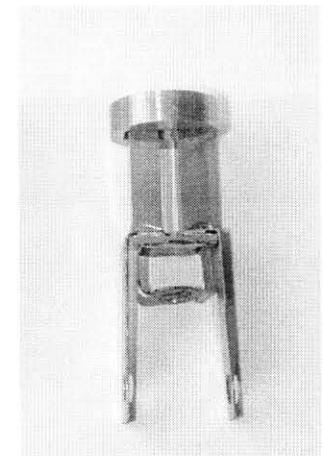
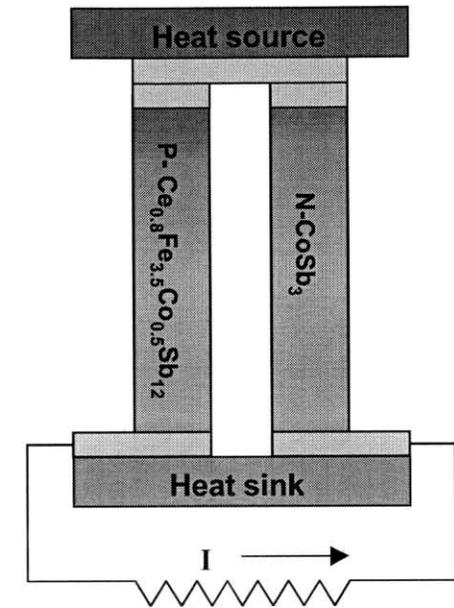
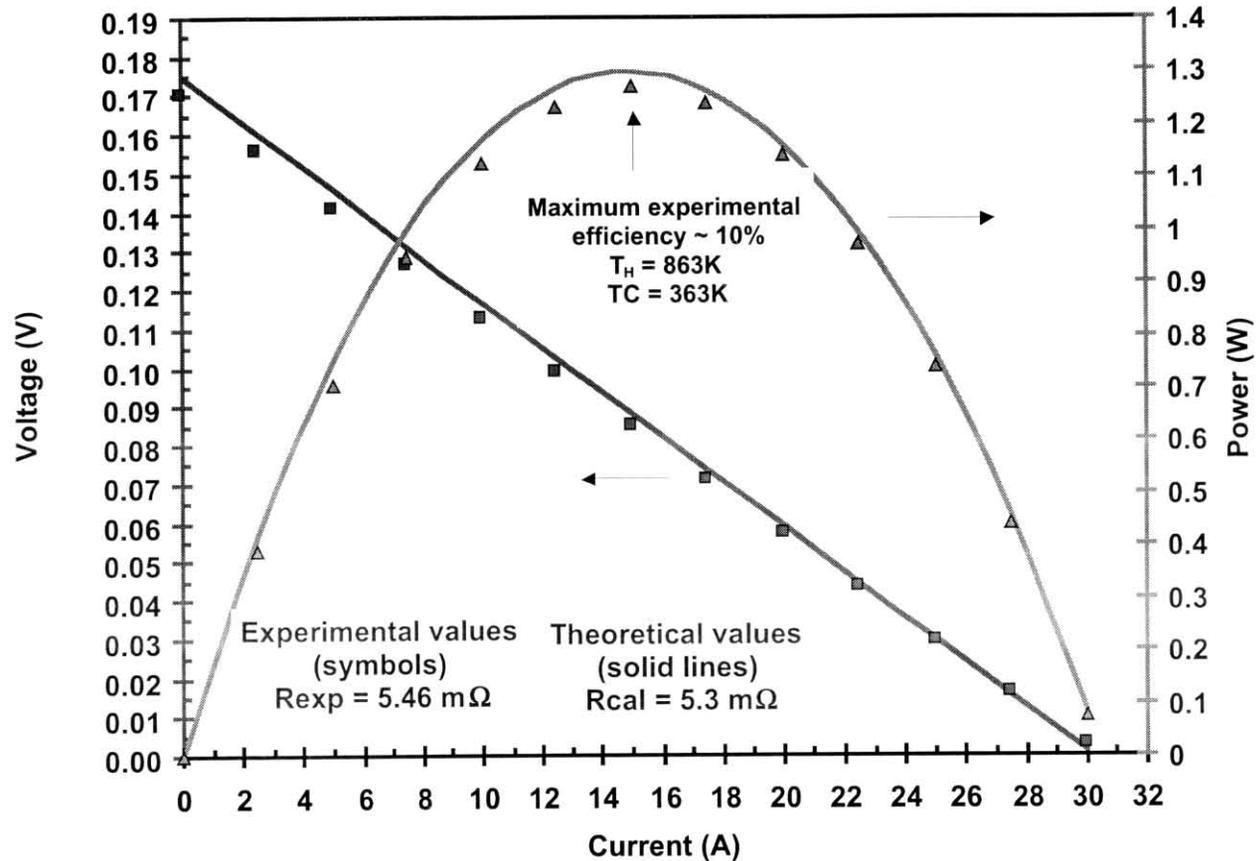


# Unicouple thermal and electrical testing





## Thermal and electrical Testing : Skutterudite only unicouple

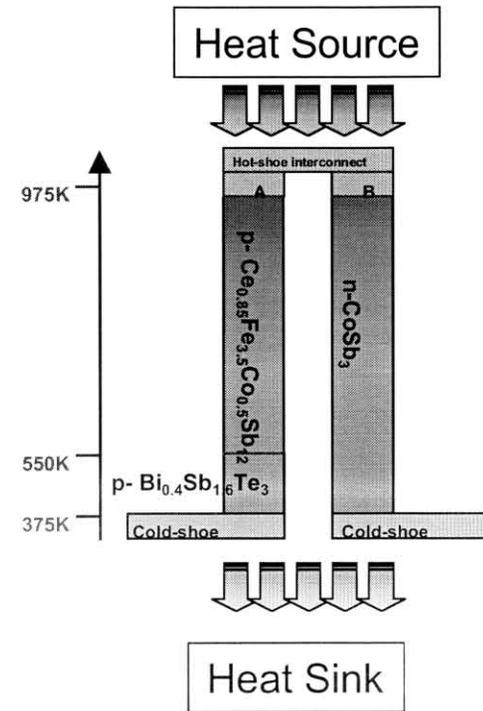
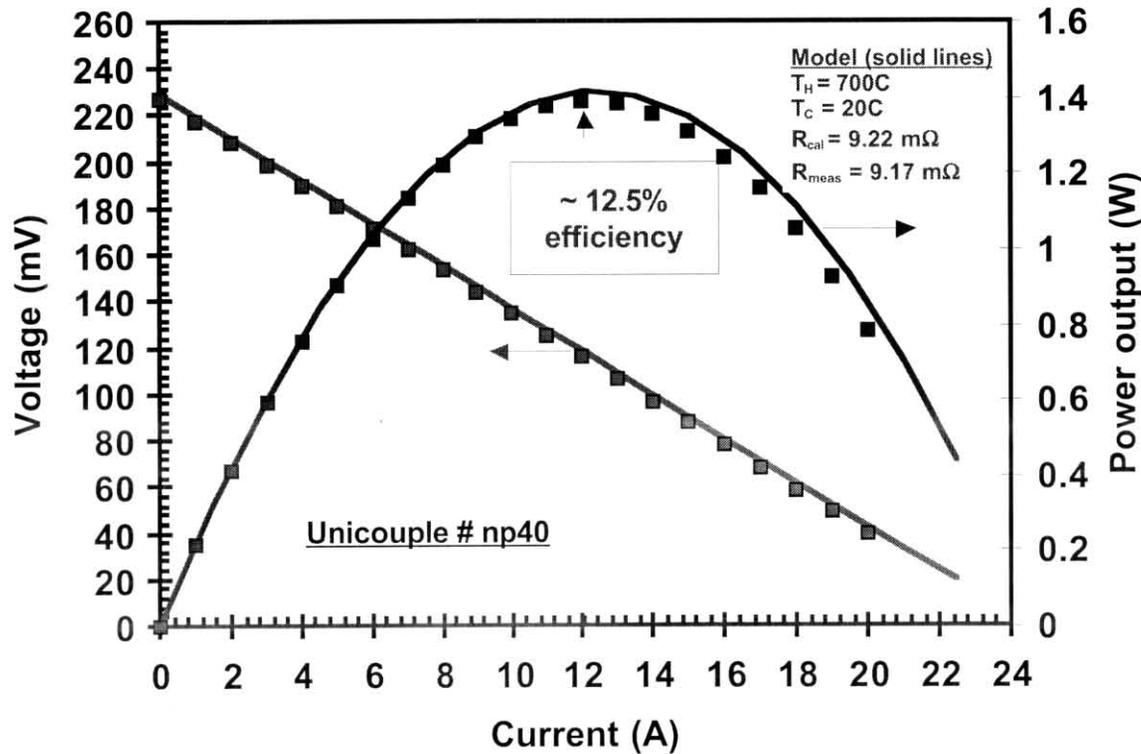


### • Unicouple performance

- Low electrical contact resistance
- Thermal to electrical efficiency : calculated  $\approx$  experimental ( ~ 10%)
- Open circuit voltage = 170 mV
- Maximum power output ~ 1.3W



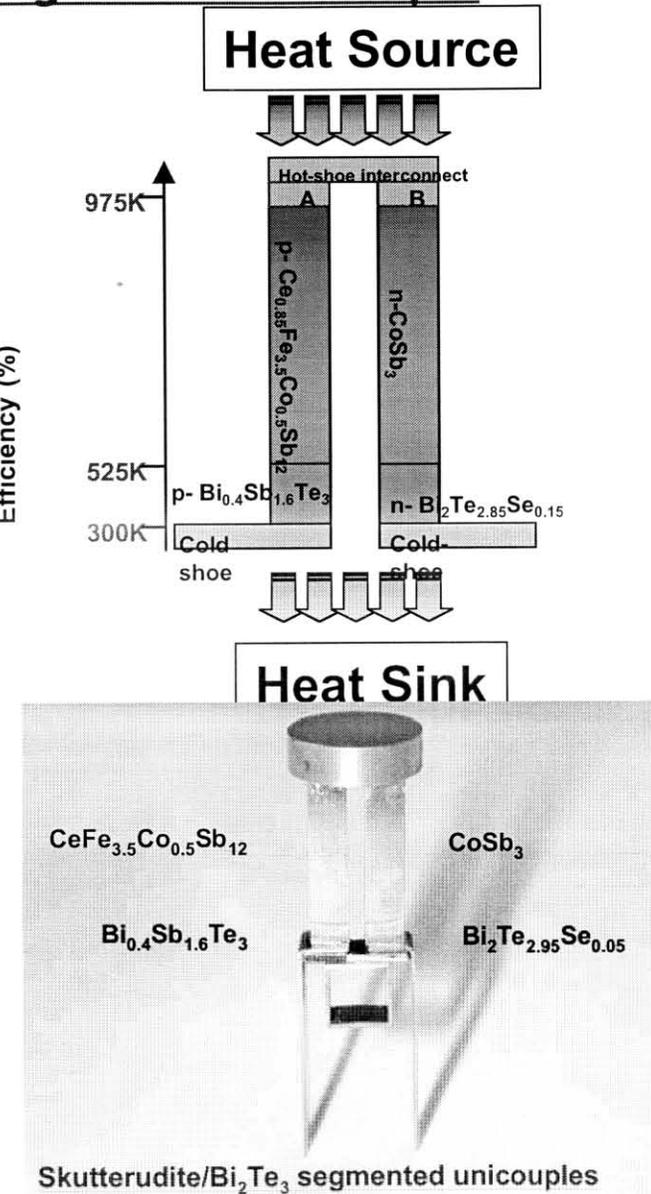
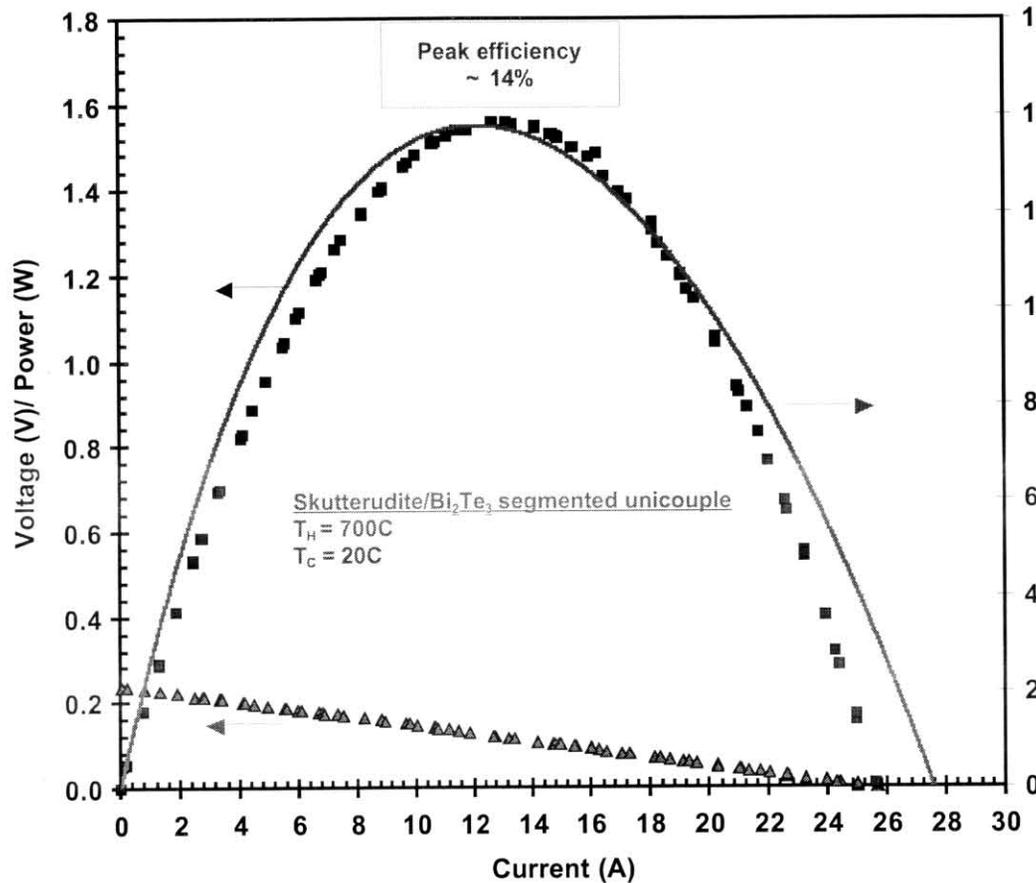
# Thermal and electrical testing - Segmented unicouple



- Achieved 12.5% efficiency for 975K-300K  $\Delta T$ 
  - With p-segmented leg and n-skutterudite leg
  - Consistent with model prediction



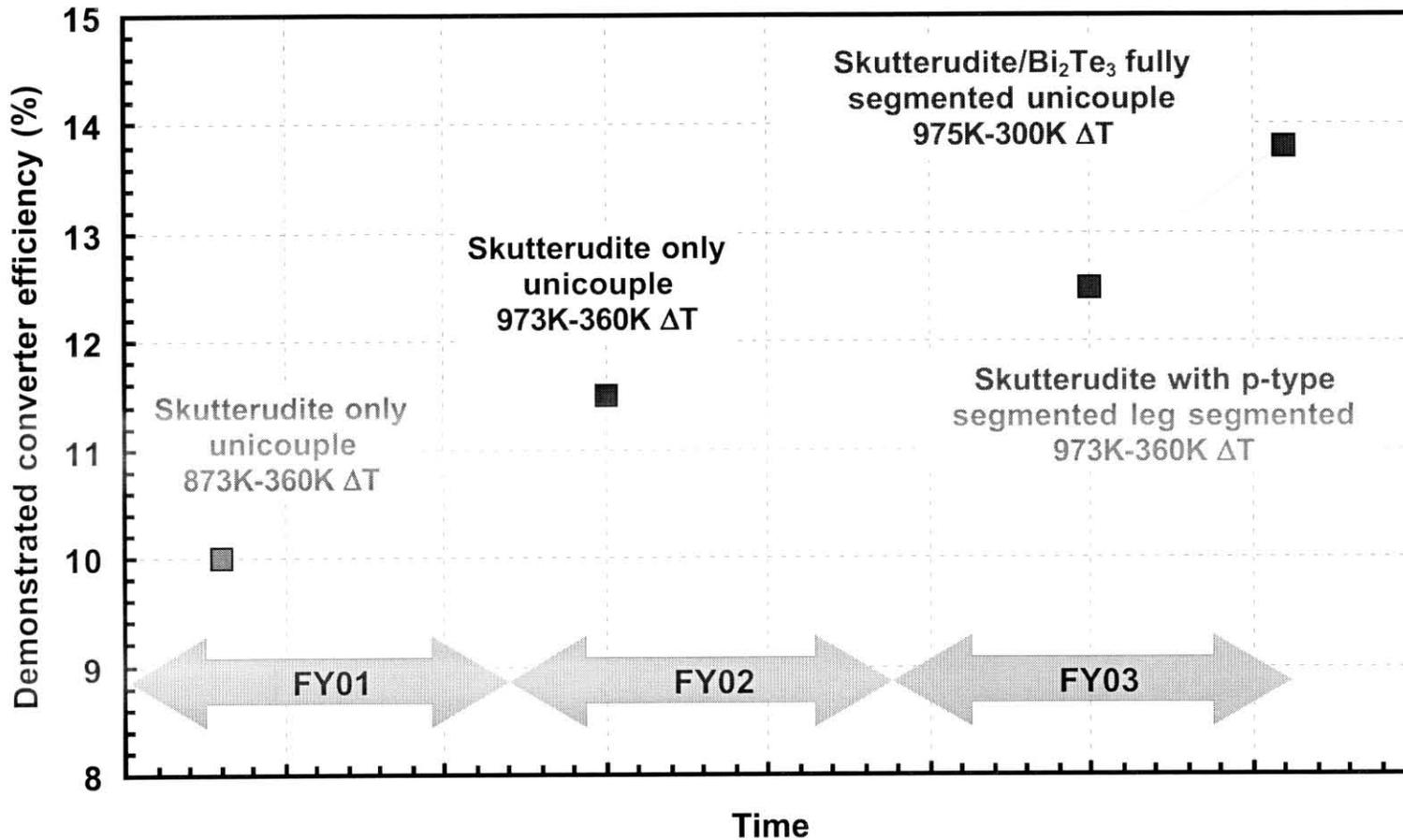
# Thermal and electrical testing - Segmented unicouple



- Achieved ~14 % efficiency for 975K-300K  $\Delta T$ 
  - For fully segmented unicouple
- ➔ Translate into 12.5% efficiency for 975K-375K  $\Delta T$
- Fully validate projected efficiency performance



## FY01-03 efficiency demonstration



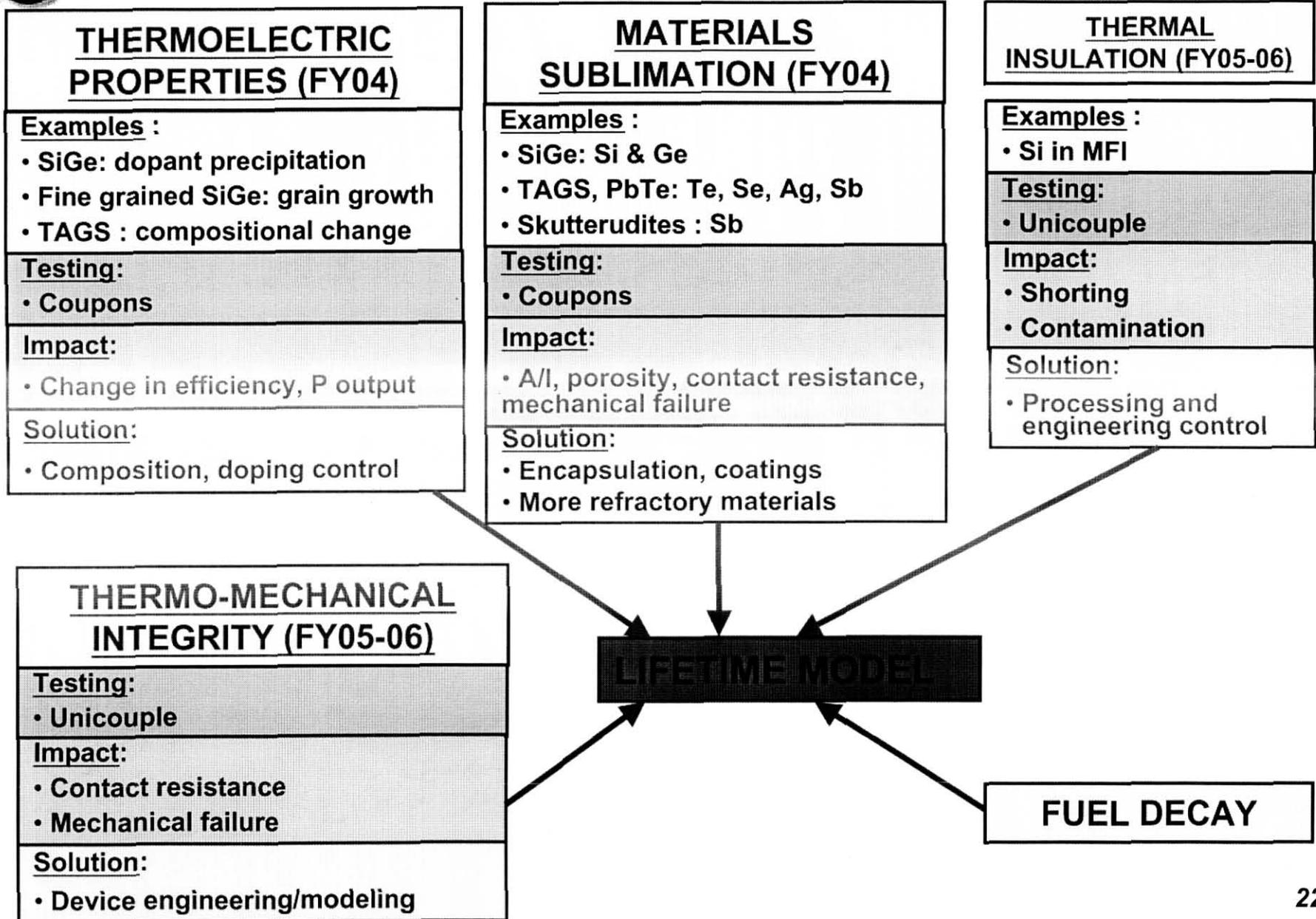
- Latest results fully validate projected performance



# **Preliminary lifetime & Sublimation studies**



# Lifetime performance testing and modeling development

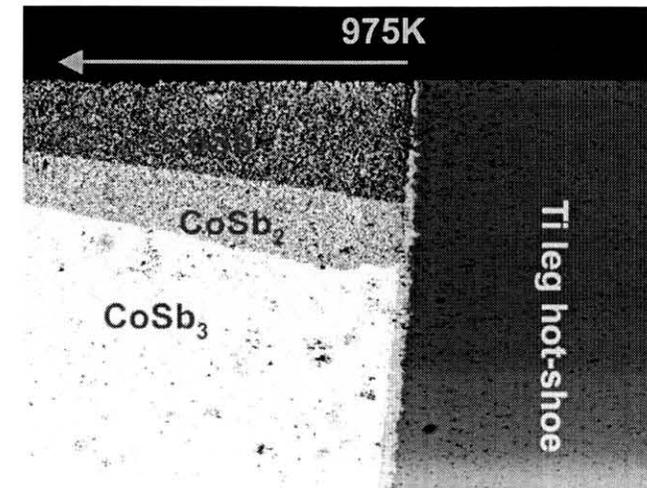




## Sublimation control experiments



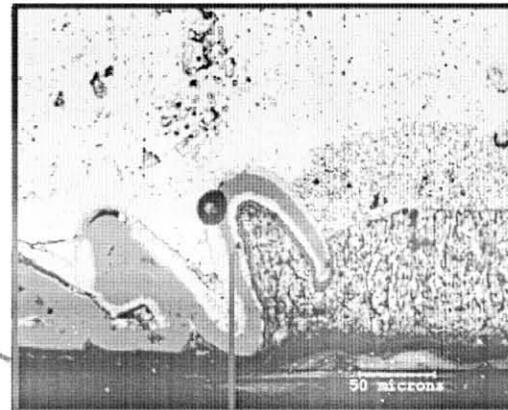
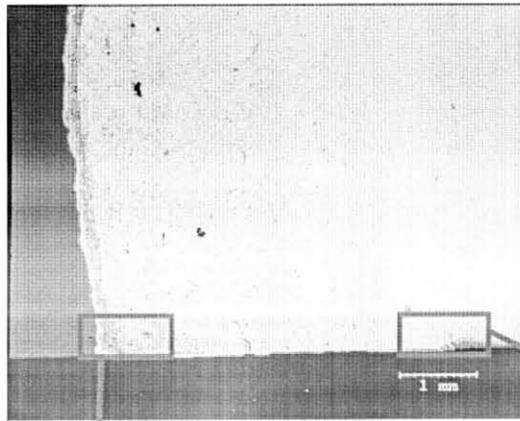
- Isothermal anneal studies
  - Confirmed that n- and p-type skutterudites are phase stable at 700°C
- Uncoated samples
  - Weight loss and temperature stability showed Sb sublimation in dynamic vacuum for T from ~ 875 to 975K for N- and p-type skutterudites
  - Decomposition into lower antimonide compounds
  - Appears to be diffusion limited
- Initial Sb sublimation control studies
  - Use of cover gas significantly suppresses Sb sublimation
  - Thin metallic film applied during hot-pressing to the sample also significantly suppresses sublimation
- Thermal/mechanical modeling performed to evaluate impact on uncouple performance



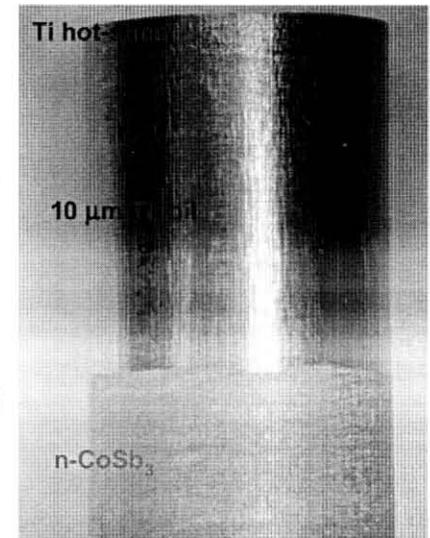
Photograph showing the decomposition of a CoSb<sub>3</sub> sample annealed in gradient for 3 months

## Coated n-type tested in-gradient for 20 days

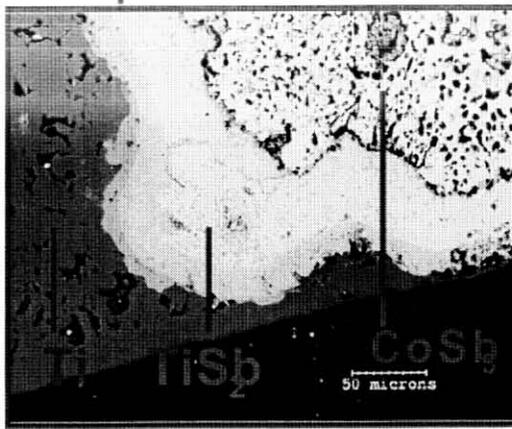
975K →



CoSb<sub>3</sub>  
CoSb<sub>2</sub>  
CoSb



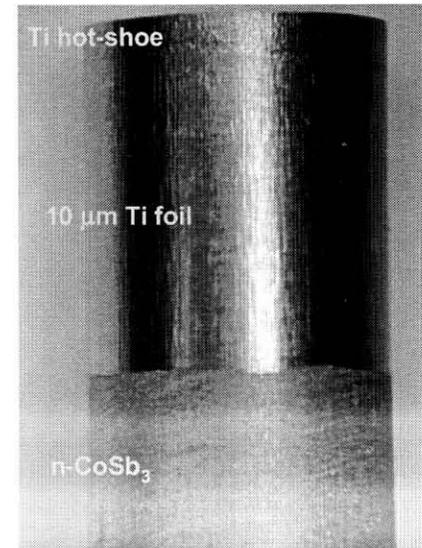
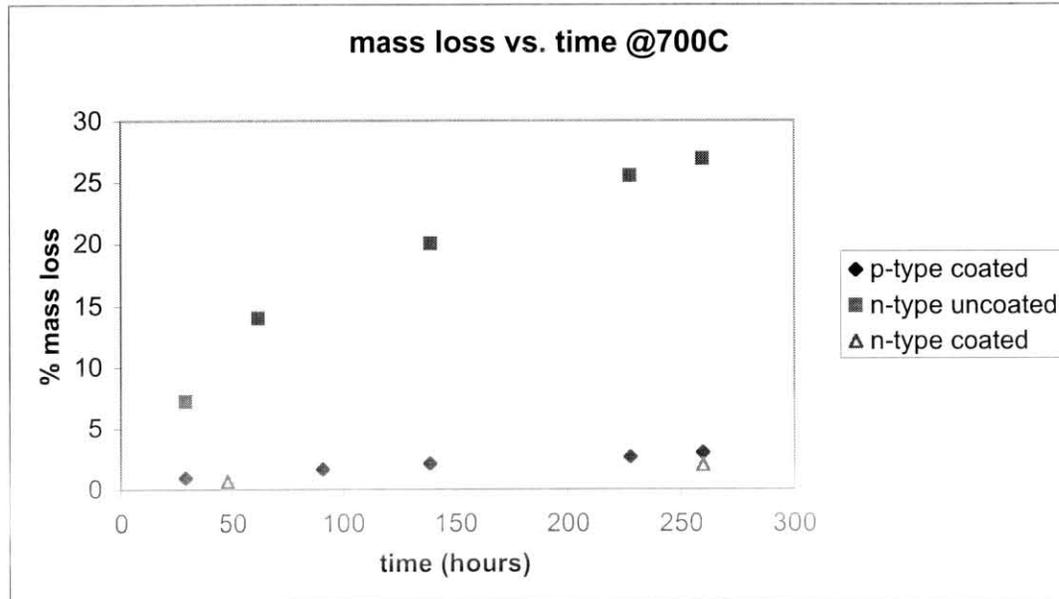
N-type Ti coated skutterudite leg



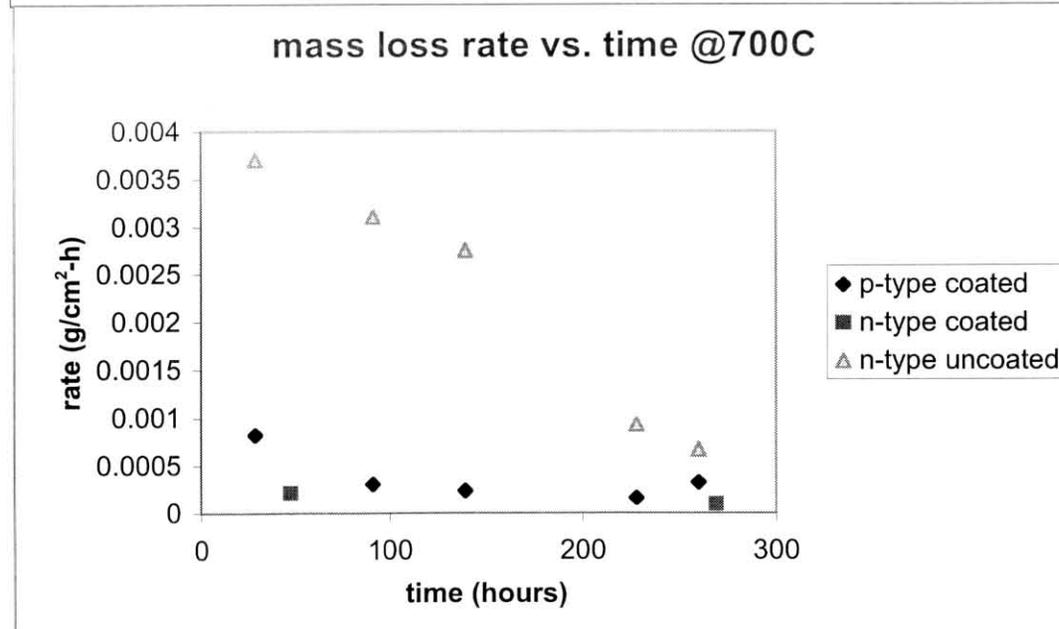
- No apparent degradation after 20 days
- Metal junction still intact
- Significant improvement over uncoated



# Mass loss experiments results



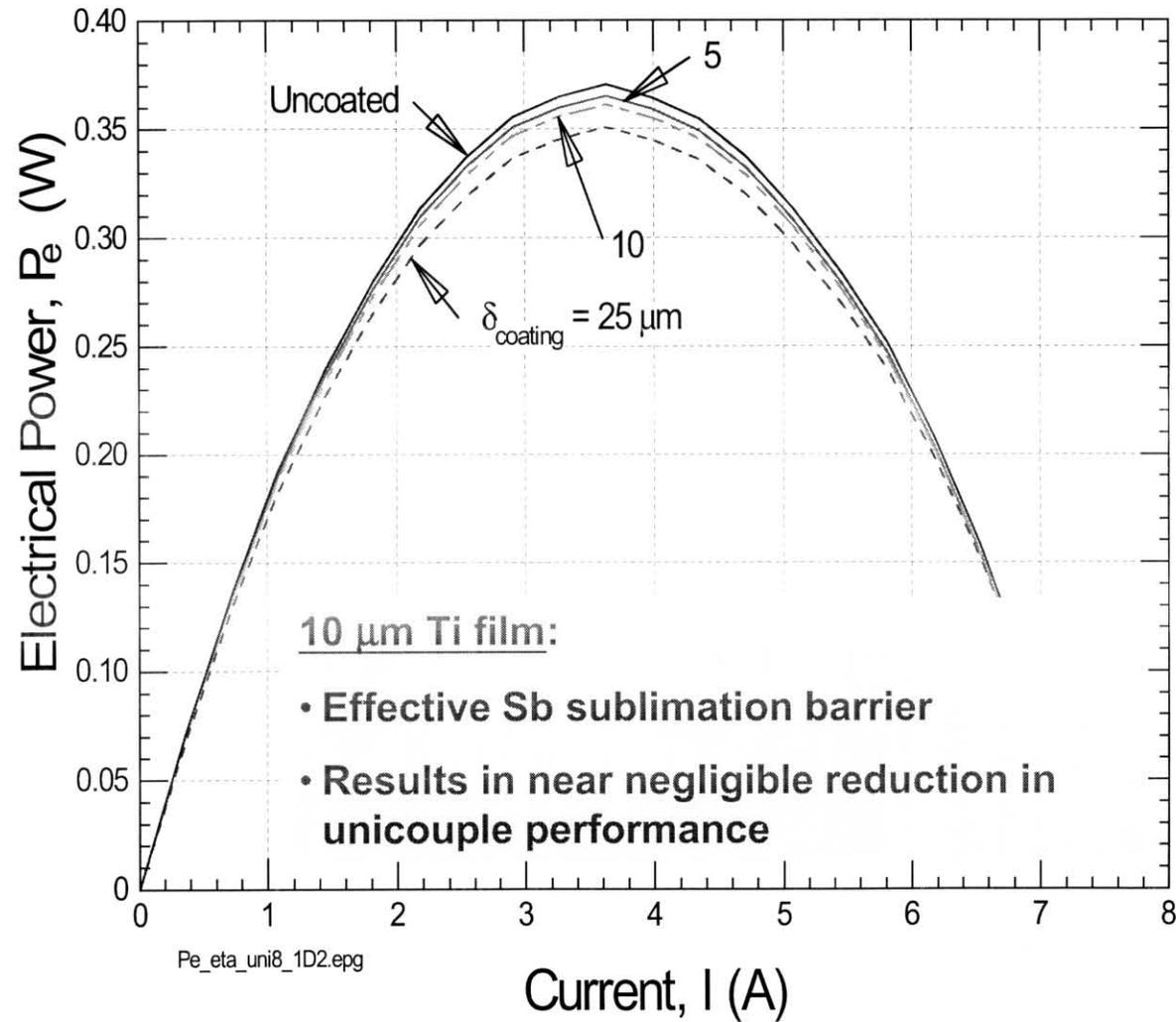
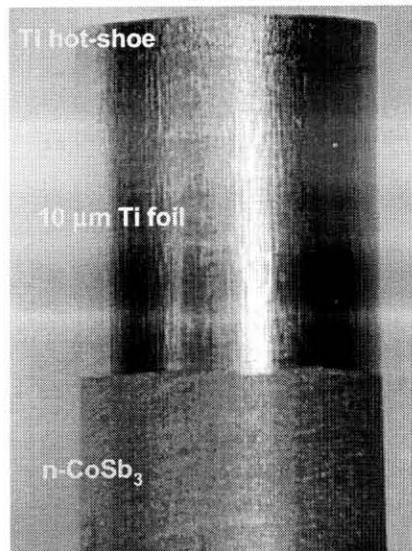
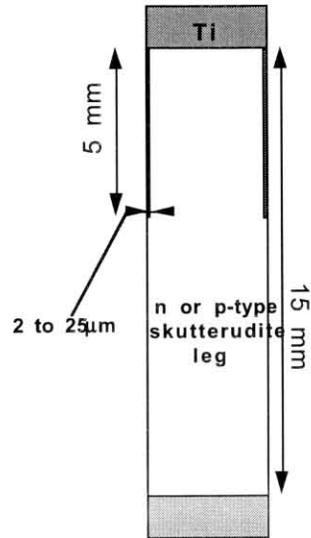
N-type Ti coated  
skutterudite leg



- Ti coating results in a significant mass loss reduction over uncoated



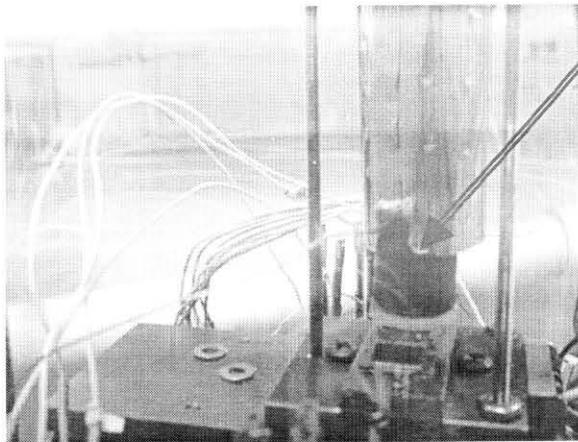
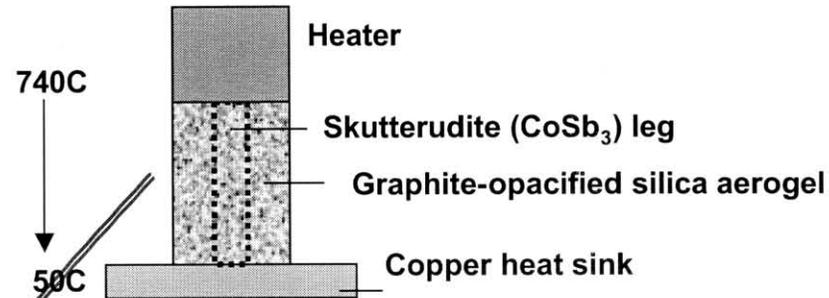
# 975K-375K Segmented TE Unicouple performance modeling (UNM)



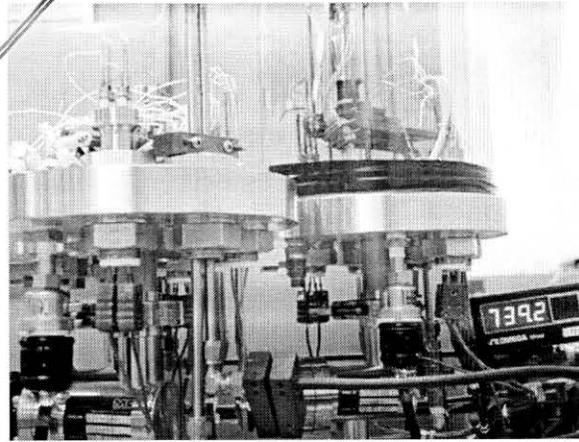
Coating Material: Ti (length 5 mm and thickness = 0-25  $\mu\text{m}$ )



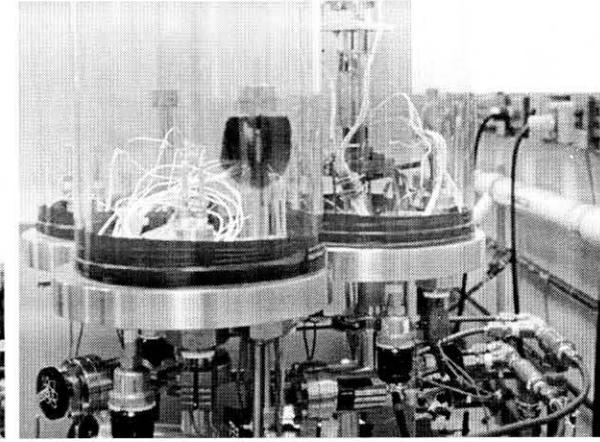
## Aerogel encapsulated skutterudite sublimation test



Skutterudite leg coated with graphite-opacified, silica aerogel. At  $10^{-6}$  torr for 6 days. The absence of condensate on the inner-wall of the bell jar indicates that sublimation is completely suppressed.



Vacuum test station used to test sublimation coatings.



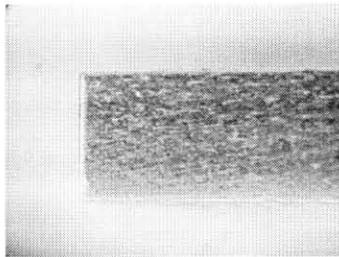
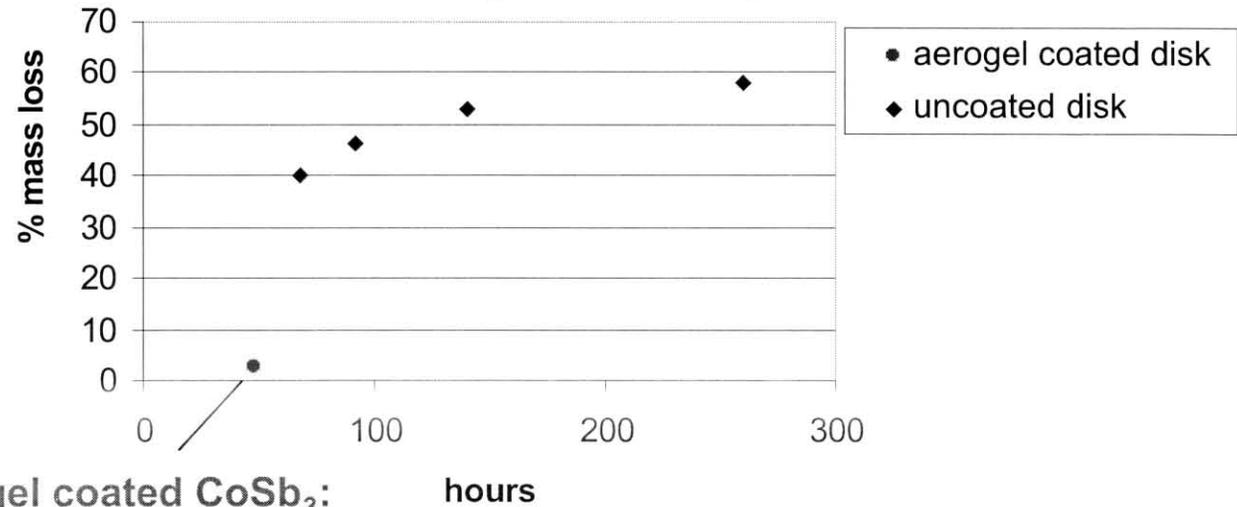
Condensation pattern of previous non-encapsulated sample sublimation test provides evidence of antimony sublimation.



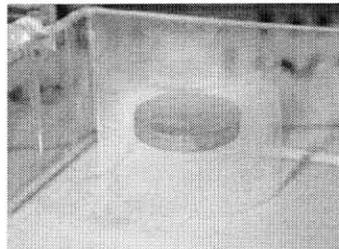
# Aerogel encapsulated samples weight loss experiments



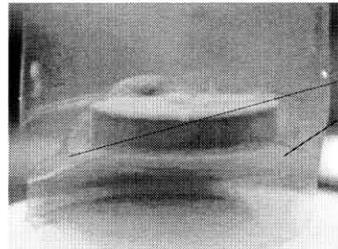
**% mass loss vs. time for CoSb<sub>3</sub> disks  
(700C 10<sup>-6</sup> torr)**



**Aerogel coated CoSb<sub>3</sub>:  
despite some cracks in  
aerogel, no depletion  
layer after 48h at 700C**



before heating



after 48h at 700C

Cracks most likely result from aerogel shrinkage around disk: need to improve thermal stability and/or strength of aerogel



# Summary



- **Demonstrated ~ 14% efficiency for STE uncouples for 975K-300K  $\Delta T$**
- **Initiated life time studies**

## FY04-06 Major Focus Areas

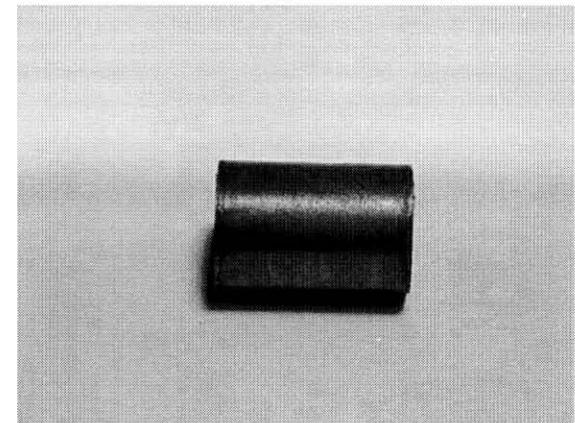
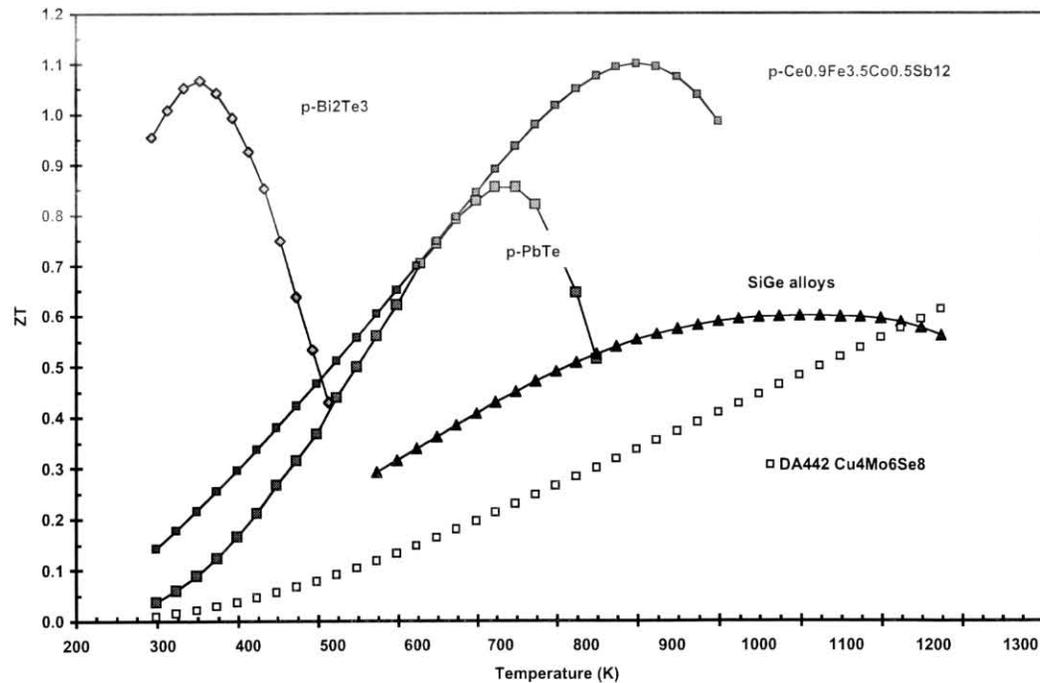
- **Optimize uncouple fabrication technique ; develop uncouple thermo-mechanical model**
- **Perform life testing of STE materials, coupons, components and uncouples**
- **Further develop sublimation control techniques/materials**
- **Develop lifetime model**



# High Temperature Materials



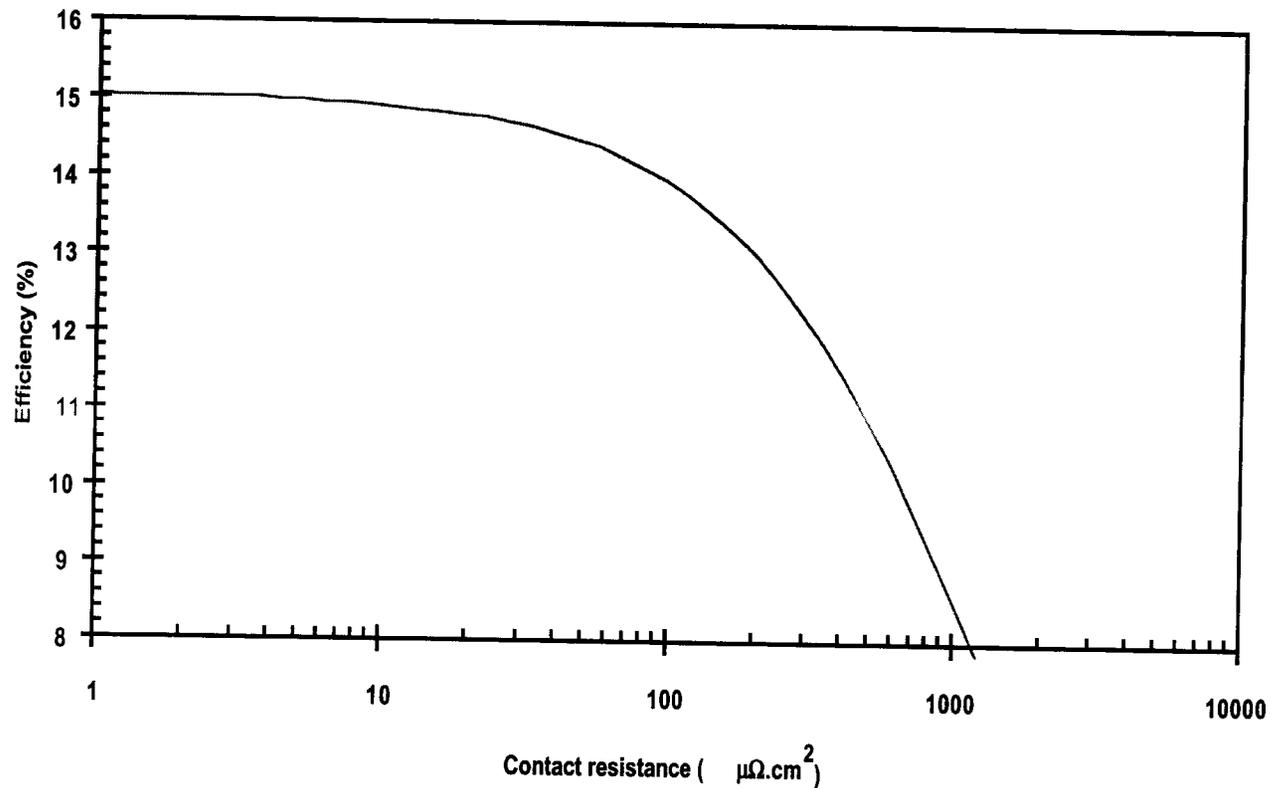
- Chevrel chalcogenides ( $\text{Mo}_6\text{Se}_8$ -based)
  - Synthesized several additional Cu and Fe filled  $\text{Mo}_6\text{Se}_8$  compositions using a powder metallurgy technique
  - Measured Seebeck coefficient, electrical resistivity, and thermal conductivity from 300K to 1275K
  - Achieved  $ZT \sim 0.6$  at 1275K for  $\text{Cu}_4\text{Mo}_6\text{Se}_8$  composition, comparable to SiGe
  - Tested  $\text{Cu}_4\text{Mo}_6\text{Se}_8$  sample under electrical load (potential Cu electromigration)
    - Sample shows no indication of electromigration after 6 days at 900°C under 5A load current



CuMo<sub>6</sub>Se<sub>8</sub> sample tested for 6 days at 900C under 5A load



## Impact of electrical contact resistance on unicouple efficiency



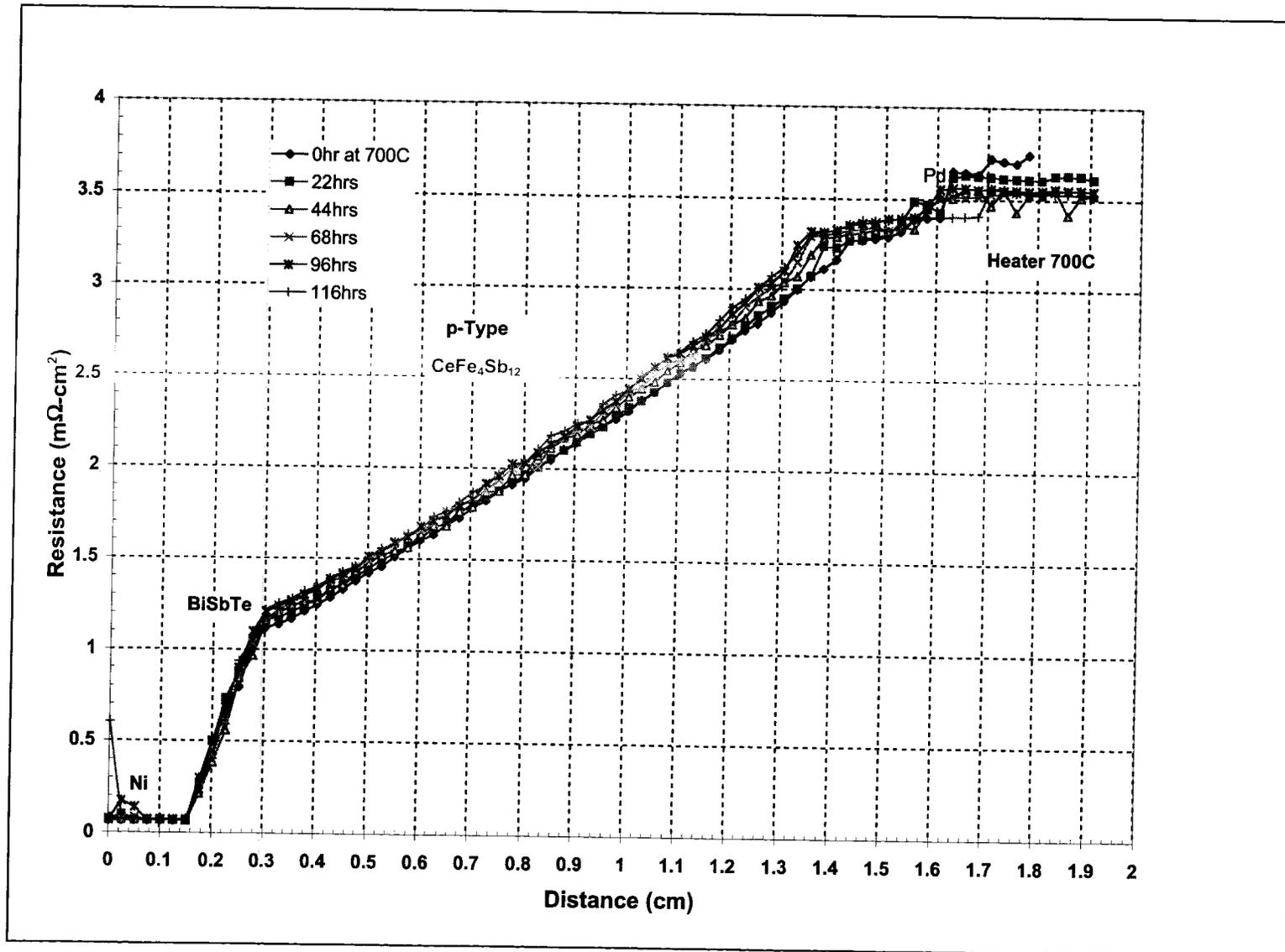
- **Electrical contact resistance needs to be  $< 5 \mu\Omega \text{cm}^2$  to prevent impact on converter efficiency**



# Electrical contact resistance measurements



- Achieved electrical contact resistance  $< 5 \mu\Omega\text{cm}^2$  at the segmented legs interfaces

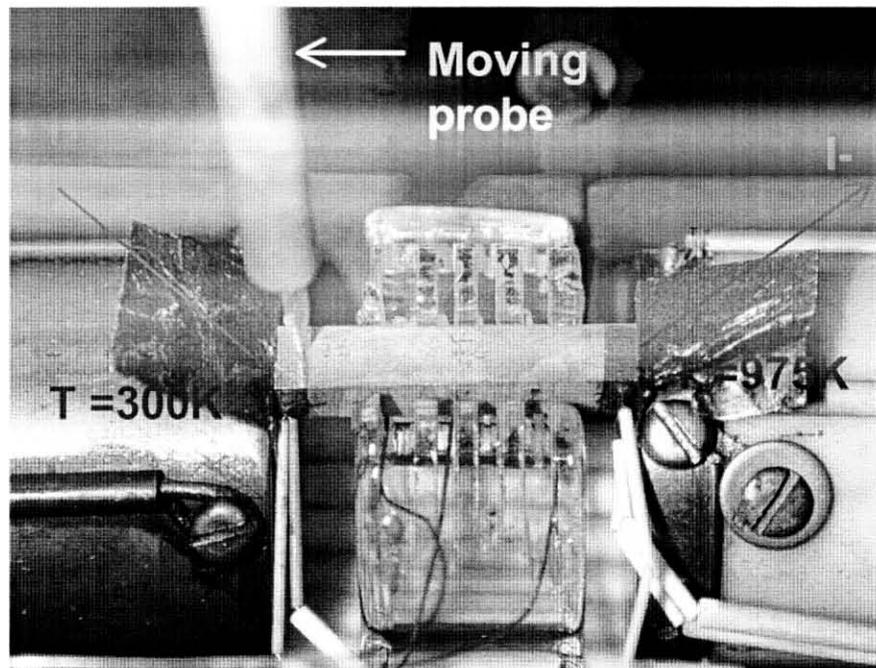




# Segmented legs electrical contact resistance measurements



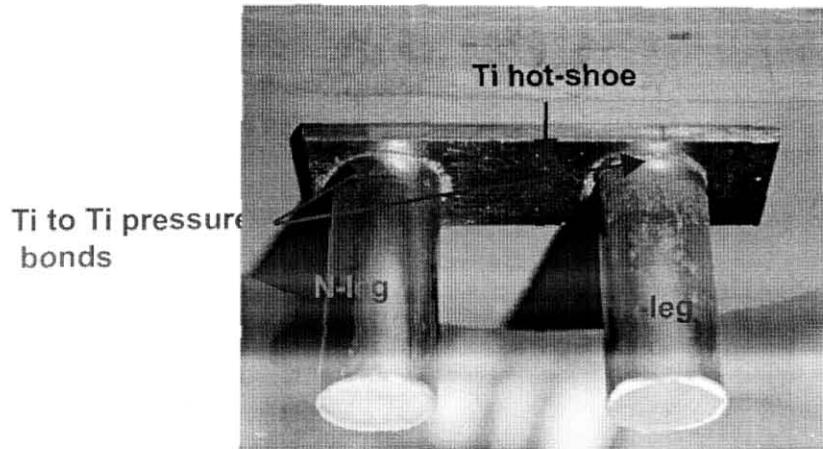
- **Bond quality**
  - Electrical contact resistance measurement
  - Microprobe analysis
    - Diffusion
    - Chemical reaction and interface layer analysis



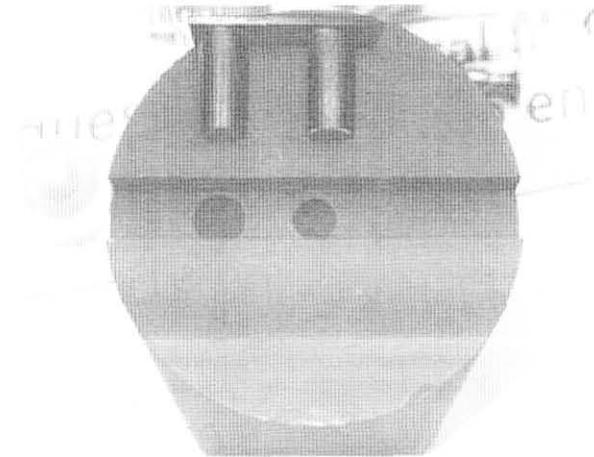
Electrical contact resistance measurements set-up



## Unicouple fabrication process developed



Unicouple fabricated by hot-pressing



Graphite die used for unicouple fabrication

- **Developed a process to fabricate unicouple by hot-pressing**
  - P- and n-leg alternatively hot-pressed onto a Ti hot-shoe
  - No measurable electrical contact resistance between TE legs and Ti hot-shoe
  - Requires further optimization but very promising
- **Process compatible with batch manufacturing**