

## Palomar Prime-Pecus Infrared Camera (PFIRCAM)

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**Abstract.** In a joint effort between engineers and scientists at the Jet Propulsion Laboratory and the California Institute of Technology, a near-infrared (0.8 - 2.6  $\mu\text{m}$ ) direct imaging system has been developed and integrated into the Caltech Palomar Observatory detector series. The camera system has been tested and operated in a science mode at the prime-focus (f/3.3) of the Hale 5-m Telescope. This paper outlines the system components and performance, including discussion of the detector linearity.

**Key words:** Instrumentation; Linearity.

### 1. PFIRCAM System Components and Performance

The system parts include a double-walled  $LN_2$  dewar containing the array, optics and filter wheels, electronic components (pre-amplifier, A/D converter, bias and timing, and high speed data transfer), and computer control (high speed receiver, array test software, cpu, etc.).

The infrared array is a matrix of 256 x 256 photodiodes formed by ion implantation into a layer of HgCdTe grown on a sapphire substrate (Rockwell's NICMOS III). The pixel size is 40 x 40,1111, corresponding to a plate scale of 0.54" x 0.54", giving a total field of view  $\sim 2.3' \times 2.3'$ . The overall camera system resolution is 11 electrons/DN with a dynamic range  $\sim 170,000$  electrons subject to a read noise  $\sim 50$  electrons. At prime focus (f/3.3) on the Hale 5-m Telescope the 10% limiting magnitudes are K  $\sim 16.7$ , H  $\sim 17.9$ , and J  $\sim 18.8$  in 60 second exposures.

### 2. PFIRCAM Linearity

The NICMOS III detector behaves nonlinearly at all flux levels, in a pixel-to-pixel dependent fashion. In order to model the detector response we obtained multiple signal images of the Hale 200" mirror cover. A typical pixel response includes a linear region followed by rollover and saturation. The linear regime may be characterized by the quadratic

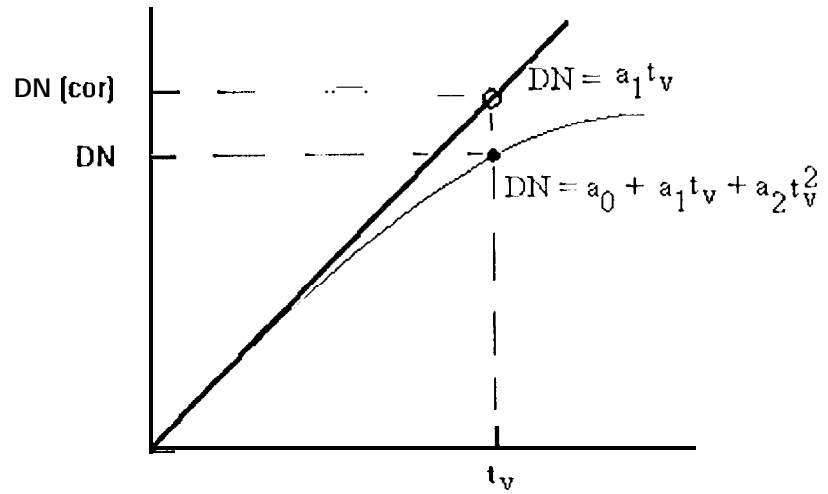
$$DN = a_0 + a_1 t + a_2 t^2; \quad DN < a_3 \quad (1)$$

where  $t$  is the integration time. In this fit the various terms are to be interpreted as:  $a_0$  the zero bias level,  $a_1$  the quantum efficiency or sensitivity,  $a_2$  the non-linearity or saturation, and  $a_3$  the dynamic range.

The fitting procedure follows four steps: (1) form  $(t, DN)$  pairs for each pixel; (2) eliminate pixels with  $DN > 95\%$  of the saturation threshold; (3) per-

form quadratic least-squares fit; (4) residuals are computed for each point; data where the residual exceeds  $2\sigma$  are eliminated and the fit is recalculated.

The basic procedure to linearly rectify PFIR-CAM science data is sketched below.



The observed DN and  $a_i$  polynomial coefficients are used to compute a “virtual” exposure time needed to match the calibration linear-sequence data. Accordingly, we must solve for  $t_v$  in the quadratic

$$DN(obs) = a_0 + a_1 t_v + a_2 t_v^2 \quad (2)$$

where the solution we seek is the smallest positive root;  $t_v$  is then multiplied by quantum efficiency  $a_1$  to give the linearized data:

$$DN(cor) = a_1 t_v. \quad (3)$$

If  $DN(obs)_{i,j} > a_3$ , then pixel  $(i,j)$  is flagged as saturated and set to some constant lower threshold.

For very large data sets it may be necessary to further optimize the computational pipeline by solving the quadratic using a series expansion. The smallest positive root has the solution

$$t_v = \frac{a_0(-a_1 + \sqrt{a_1^2 - 4a_0a_2})}{2} - \frac{a_0^2 DN}{\sqrt{a_1^2 - 4a_0a_2}} + \frac{a_0^3 DN^2}{(a_1^2 - 4a_0a_2)^{3/2}} + O(DN^3), \quad (4)$$

i.e.,

$$t_v = a_0' + a_1' DN + a_2' DN^2 + O(DN^3). \quad (5)$$