

DEVELOPMENT OF HIGH EFFICIENCY THERMOELECTRIC GENERATORS USING ADVANCED THERMOELECTRIC MATERIALS

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Abstract

Despite their relatively low **efficiency**, thermoelectric **generators** are used in a limited number of industrial applications **where** they are **preferred** to other **energy** conversion devices because of their high reliability, low maintenance and long life, in particular when considering harsh **environments**. New more **efficient** thermoelectric **materials** and devices **are** needed to expand the range of application of thermoelectric generators. Several new terrestrial applications requiring higher **efficiency** generators have been recently **described** in the literature. Heat **sources** for **these** applications range **from** low grade waste **heat** at 325-350K up to 850 to 1100K for heat **recovery** from processing plants of combustible solid waste. Commercial thermoelectric generators **are** usually built using **Bi₂Te₃**- or **PbTe**-based alloys depending on the maximum hot side temperature. A new approach consisting of using **new** high performance thermoelectric materials developed at the Jet Propulsion Laboratory (**JPL**) and operating the generator over a larger temperature **difference** is presented. By using novel segmented legs based on a combination of **state-of-the-art** thermoelectric materials and p-type **Zn_{1-x}Cd_xSb₃** alloys, p-type **CeFe₄Sb₁₂**-based alloys and n-type **CoSb₃**-based alloys, an **increase** in the thermoelectric materials conversion **efficiency** of about 60% is expected compared to **Bi₂Te₃**- and **PbTe**-based generators. The maximum thermoelectric **materials efficiency** will be about 20% for the optimum generator configuration. Various issues related to the fabrication of new segmented legs, including bonding and temperature stability tests, will be briefly discussed.

INTRODUCTION

The growing interest for thermoelectric power generation is mostly due to emerging energy saving and environmental issues. A number of new **potential** applications have been cited in the literature ranging from recovering waste heat from various industrial heat-generating processes to waste heat generated by vehicle exhaust to replace or supplement the alternator and thus **decrease fuel** consumption (**Morelli** 1997). For some of these applications, the **efficiency** as well as the cost of the thermoelectric generators are **critical**. To achieve high **efficiency**, it is desirable to operate thermoelectric generator devices over large temperature ranges and also to **maximize the** thermoelectric **performance** of the materials used to build the devices. However, no single thermoelectric **material** is suitable for use over a very wide range of temperature (-300-1000K). It is therefore necessary to use **different materials** in each **temperature** range where they possess optimum performance. This can be achieved in two ways: 1) multistage thermoelectric **generators** where each stage operates over a **fixed** temperature **difference** and is electrically insulated but thermally in contact with the other stages 2) segmented **generators** where the p- and n-legs are formed of different segments joined in series. A number of studies on segmented thermoelectric generators using **state-of-the-art** thermoelectric materials **have recently appeared** in the literature (**Schilz** et al., 1997). The materials under investigation **are** mostly **Bi₂Te₃**-based materials, **FeSi₂** and **PbTe**-based alloys. We **have** recently proposed a new version of a segmented thermoelectric generator utilizing advanced thermoelectric materials with superior thermoelectric figures of merit (**Fleurial** et al., 1997a; **Fleurial** et al., 1997b). The benefits of using these new materials are reviewed in this paper as well as the issues involved for the construction of this generator. Preliminary results for optimizing the **geometry** of the thermoelectric materials and the **efficiency** of the **generator** **are** also presented.

NEW SEGMENTED GENERATOR

The concepts of integrating new thermoelectric materials developed at the Jet Propulsion Laboratory (**JPL**) into segmented thermoelectric generators have been presented in details in earlier publications (**Fleurial** et al., 1997a, **Fleurial** et al., 1997b). The **schematic** of the first **generation** of the advanced generator is **presented** in Fig 1. The benefits of using these advanced thermoelectric materials **are** twofold: 1) the generator can be **operated** over a larger temperature drop **compared** to those using only **state-of-the-art** **Bi₂Te₃** and **PbTe**-based alloys (300-845 K versus 300-975K) 2) the **average** thermoelectric figure of merit, **ZT**, is larger. As a result, the **calculated** thermoelectric

efficiency is higher for these generators and is 15.9% for the version depicted in Figure 1. It could be as high as 19.2% for the version utilizing a second generation of improved thermoelectric materials currently being developed at JPL (Fleurial et al., 1997a). This represents a significant increase in efficiency when compared to Bi₂Te₃ and PbTe-based segmented generators with an efficiency of about 12% when operating between 300 and 845K.

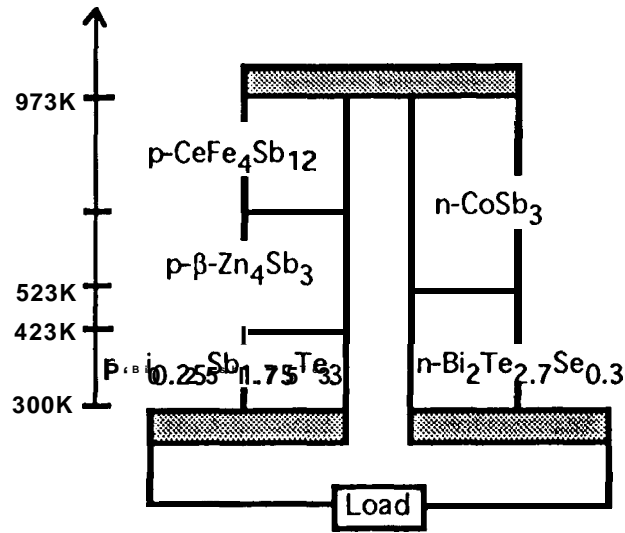


FIGURE 1. schematic of a segmented thermoelectric generator using improved thermoelectric material developed at JPL.

JPL is currently pursuing the development of the segmented generator shown in Figure 1. Ideally, the materials used in the different segments of the p- and -n legs should have similar thermophysical and mechanical properties to ensure reliable operation over a large temperature difference. In particular, they should have similar thermal conductivity and thermal expansion coefficient values. We have measured some of these properties and found that there is a reasonably good match between the properties of the different materials (Fleurial et al., 1997a). One additional requirement for the materials used in the different segments is their temperature stability. We are currently investigating the temperature stability of the thermoelectric materials used in the first version of the generator (see Figure 1). Experiments have been designed where samples are subjected to anneals over long period of time in various atmospheres and their thermoelectric properties and other physical and chemical properties such as weight and composition are monitored. In addition, the behavior of each material will be tested when subjected to a temperature gradient. The p- and n-legs are built by joining the different segments and all joints should have low electrical contact resistance as well as a good temperate stability. Joining the different segments can be achieved by directly bonding the different materials or using contacting layers which can be used to correct for any thermal expansion mismatch for example. A number of these tests are currently in progress.

OPTIMAL SEGMENT LENGTHS

A schematic segmented thermoelectric generator is shown in Figure 2 and is composed of m p-type and n n-type materials. The hot and cold junction are denoted by T_H and T_C , respectively. The optimization of the efficiency of this type of generator has been previously studied (Swanson et al., 1961). The thermal efficiency is defined as the quotient of the electrical power output (P) to the heat rate supplied at the hot junction. The optimization of the geometry of the legs involves primarily fine tuning the cross-section and length of the different segments. Given the average thermoelectric properties (Seebeck coefficient, electrical resistivity, and thermal conductivity) over the temperature range of operation for each segment of the n- and p-legs, one can calculate their optimum cross section, length as well as the optimum current and efficiency (Swanson et al., 1961). The lengths of the segments can be calculated using the following equations:

$$\frac{\lambda_{p_i} \Delta T_{p_i}}{I_{p_i}} = \frac{\lambda_{p_{i+1}} \Delta T_{p_{i+1}}}{I_{p_{i+1}}} \quad (1)$$

$$\frac{\lambda_{n_i} \Delta T'_{p_i}}{l_{n_i}} = \frac{\lambda_{n_{i+1}} \Delta T'_{n_{i+1}}}{l_{n_{i+1}}} \quad (2)$$

$$L = \sum_{i=1}^m l_{p_i} = \sum_{j=1}^o l_{n_j} \quad (3)$$

where λ is the thermal conductivity, l is the length of each segment, ΔT is the temperature drop across each segment, and L is the total length of the legs.

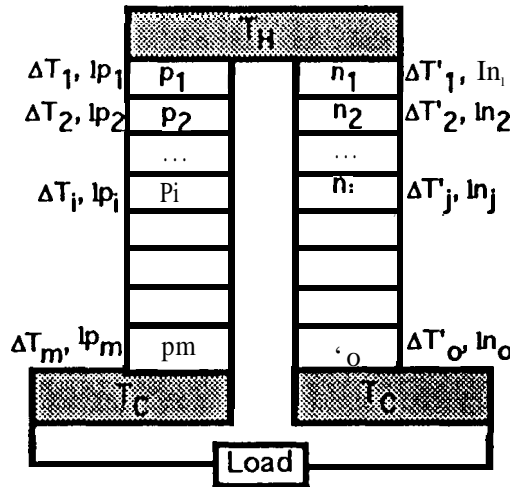


FIGURE 2. Schematic of a segmented thermoelectric generator

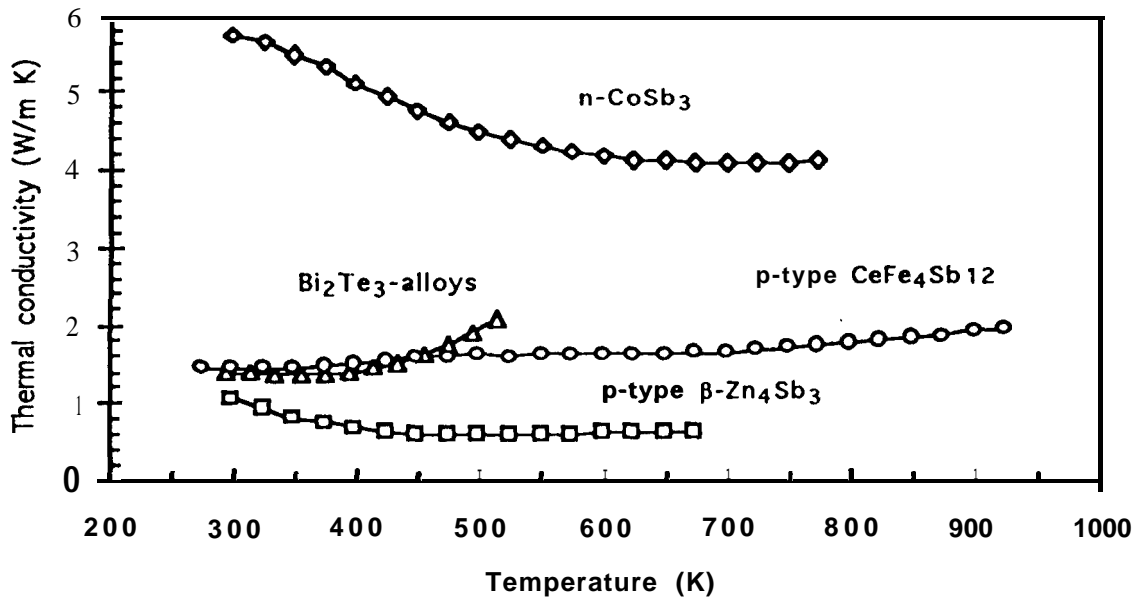


FIGURE 3. Thermal conductivity versus temperature for several state-of-the-art and advanced thermoelectric materials. N- and p-type Bi_2Te_3 based alloys have similar thermal conductivity and only the values for p-type are shown for clarity.

Equations 1,2, and 3 were used to calculate the segment lengths in the case of the segmented generator depicted in Figure 1. For the calculations, we have used the average thermal conductivity reported in Figure 3 and a value of 10 cm for L. The results are shown in Figure 4. Because of the thermal conductivity values of n-type CoSb_3 , is larger than those for the other materials used, the n-type CoSb_3 is quite long. Further estimations are in progress to calculate the optimal cress section of each leg, current and efficiency.

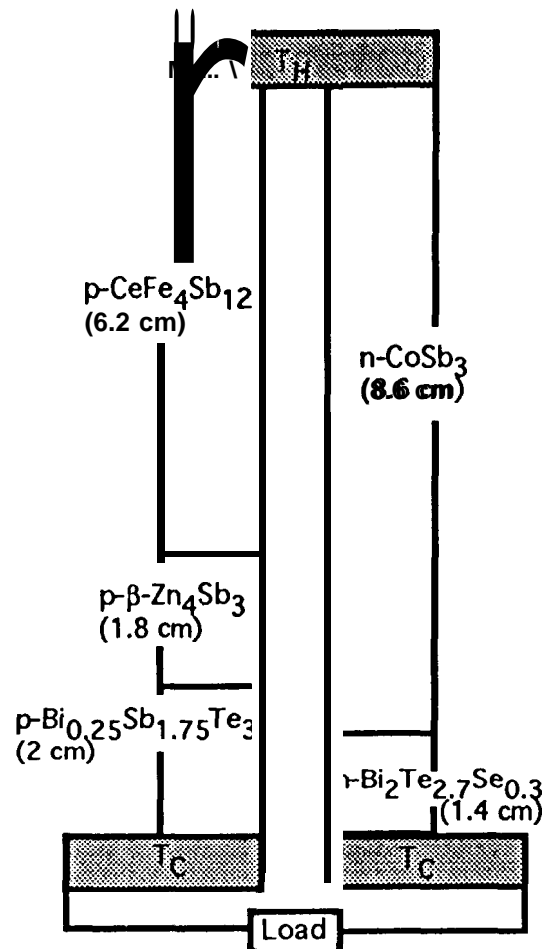


FIGURE 4. Schematic of an advanced thermoelectric generator operating between 300 and 975K illustrating the optimal segment length for each material use for the n-and p-legs.

Improved thermoelectric generators could be used in a variety of applications. Thermoelectric generators operating on natural gas, propane or diesel were built and used Bi_2Te_3 or PbTe alloys depending on the maximum hot side temperature (up to 873K) (Naughton, 1995). Despite their relatively low efficiency, these devices are used in various industrial applications because of their high reliability, low maintenance and long life, in particular when considering harsh environments. The most common applications are for cathodic protection, data acquisition and telecommunications. More recently, there has been a growing interest for waste heat recovery power generation using various heat sources such as the combustion of solid waste, geothermal energy, power plants, and other industrial heat-generating processes. There is currently an important effort in Japan to develop large scale waste heat recovery thermoelectric generators using state-of-the-art materials (Kajikawa et al., 1994). But perhaps the automobile industry is the market with the most potential (Morelli 1997). Because of the need for cleaner, more efficient cars, car manufacture worldwide are interested in using the waste heat generated by the vehicle exhaust to replace or supplement the alternator. According to some car manufacturers, the available temperature range would be from 350 to 800K, which would be match by the new segmented generators.

CONCLUSION

New highly efficient segmented thermoelectric generators using advanced thermoelectric materials are currently being developed. In the optimal version, the thermoelectric efficiency is about 20 % for a generator operating between 300 and 975K. Various issues to be resolved to build these generators including joining of the different segments, studies of the temperature stability of the thermoelectric materials, and optimal geometry were presented and are currently being investigated. These high performance thermoelectric generators could be incorporated in a variety of applications, in particular those making use of waste heat recovery.

Acknowledgments

This work was carried out at the Jet Propulsion Laboratory/California Institute of Technology, under contract with the National Aeronautics and Space Administration.

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